

## BAB V

### KESIMPULAN

#### 5.1 Kesimpulan

Dari pembahasan, pembuatan, pengujian serta hasil pengukuran yang telah dilakukan, dapat diambil kesimpulan sebagai berikut:

1. Rangkaian antarmuka jaringan telepon yang dibuat dapat berfungsi dengan baik, dimana sensor dapat mendeteksi ringing current. Demikian juga pada rangkaian lainnya, sehingga dekoder DTMF dapat berfungsi dengan baik.
2. Pada rangkaian VMS maksimum waktu perekaman yang diperoleh dengan kapasitas memory 1 Mbit kurang lebih 45 detik.
3. Di dalam perancangan ini terjadi beberapa penyimpangan dari perhitungan yang didapat, karena nilai komponen hasil perhitungan tidak ada sehingga digunakan nilai komponen yang mendekati.

Dalam perancangan mesin penjawab telepon ini selain menggunakan perhitungan juga digunakan sistem coba-coba untuk mendapatkan hasil yang maksimal.

## DAFTAR PUSTAKA

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(Suhairi)

### LM311 voltage comparator general description

The LM311 is a voltage comparator that has input currents more than a hundred times lower than devices like the LM306 or LM710C. It is also designed to operate over a wider range of supply voltages: from standard  $\pm 15V$  op amp supplies down to the single 5V supply used for IC logic. Its output is compatible with RTL, DTL and TTL as well as MOS circuits. Further, it can drive lamps or relays, switching voltages up to 40V at currents as high as 50 mA.

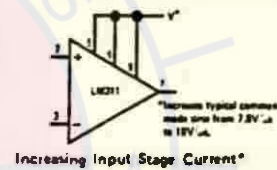
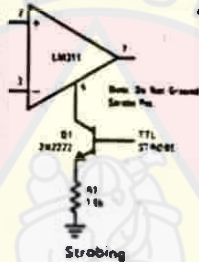
### features

- Operates from single 5V supply
- Maximum input current: 250 nA
- Maximum offset current: 50 nA

- Differential input voltage range:  $\pm 30V$
- Power consumption: 135 mW at  $\pm 15V$

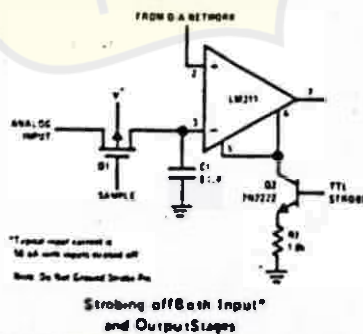
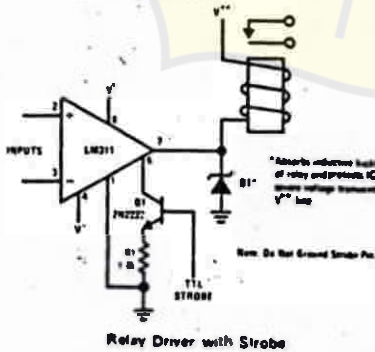
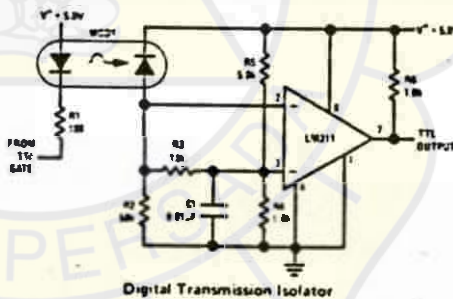
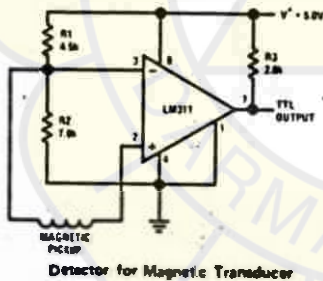
Both the input and the output of the LM311 can be isolated from system ground, and the output can drive loads referred to ground, the positive supply or the negative supply. Offset balancing and strobe capability are provided and outputs can be wire OR'ed. Although slower than the LM306 and LM710C (200 ns response time vs 40 ns) the device is also much less prone to spurious oscillations. The LM311 has the same pin configuration as the LM306 and LM710C. See the "application hints" of the LM311 for application help.

### auxiliary circuits\*



\*Note: Pin connections shown on schematic diagram and typical applications are for TO-5 package.

### typical applications\*



\*Absorb inductive kickback of relay and protect IC from reverse voltage transients on  $V^+$  line.

\*Input stage current is 100 nA with inputs excited off



## absolute maximum ratings

Total Supply Voltage ( $V_{S+}$ )	36V
Output to Negative Supply Voltage ( $V_{14}$ )	40V
Ground to Negative Supply Voltage ( $V_{14}$ )	30V
Differential Input Voltage	$\pm 30V$
Input Voltage (Note 1)	$\pm 15V$
Power Dissipation (Note 2)	500 mW
Output Short Circuit Duration	10 sec
Operating Temperature Range	0°C to 70°C
Storage Temperature Range	-65°C to 150°C
Lead Temperature (soldering, 10 sec)	300°C
Voltage at Strobe Pin	-5 V

## electrical characteristics (Note 3)

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Input Offset Voltage (Note 4)	$T_A = 25^\circ\text{C}$ , $R_B \leq 50k$		2.0	7.5	mV
Input Offset Current (Note 4)	$T_A = 25^\circ\text{C}$		6.0	50	nA
Input Bias Current	$T_A = 25^\circ\text{C}$		100	250	nA
Voltage Gain	$T_A = 25^\circ\text{C}$	40	200		V/mV
Response Time (Note 5)	$T_A = 25^\circ\text{C}$		200		ns
Saturation Voltage	$V_{IN} \leq -10\text{mV}$ , $I_{OUT} = 50\text{mA}$ $T_A = 25^\circ\text{C}$		0.75	1.5	V
Strobe ON Current	$T_A = 25^\circ\text{C}$		3.0		mA
Output Leakage Current	$V_{IN} \geq 10\text{mV}$ , $V_{OUT} = 35V$ $T_A = 25^\circ\text{C}$ , $I_{STROBE} = 3\text{mA}$		0.2	50	nA
Input Offset Voltage (Note 4)	$R_B \leq 50k$			10	mV
Input Offset Current (Note 4)				70	nA
Input Bias Current				300	nA
Input Voltage Range		-14.5	13.8, -14.7	13.0	V
Saturation Voltage	$V^+ \geq 4.5\text{V}$ , $V^- = 0$ $V_{IN} \leq -10\text{mV}$ , $I_{SINK} \leq 8\text{mA}$		0.23	0.4	V
Positive Supply Current	$T_A = 25^\circ\text{C}$		5.1	7.5	mA
Negative Supply Current	$T_A = 25^\circ\text{C}$		4.1	5.0	mA

Note 1: This rating applies for  $\pm 15V$  supplies. The positive input voltage limit is 30V above the negative supply. The negative input voltage limit is equal to the negative supply voltage or 30V below the positive supply, whichever is less.

Note 2: The maximum junction temperature of the LM311 is 110°C. For operating at elevated temperatures, devices in the TO-5 package must be derated based on a thermal resistance of 150°C/W, junction to ambient, or 45°C/W, junction to case. For the flat package, the derating is based on a thermal resistance of 185°C/W when mounted on a 1/16-inch-thick epoxy glass board with ten, 0.03-inch-wide, 2-ounce copper conductors. The thermal resistance of the dual-in-line package is 100°C/W, junction to ambient.

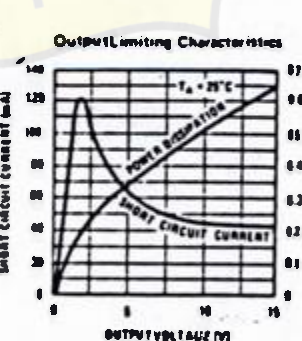
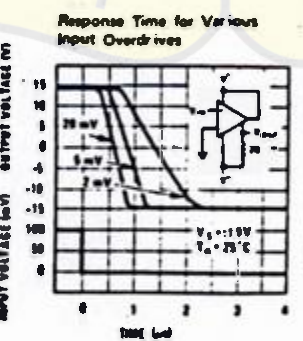
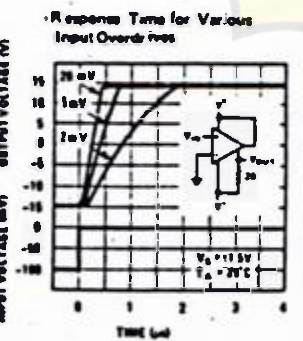
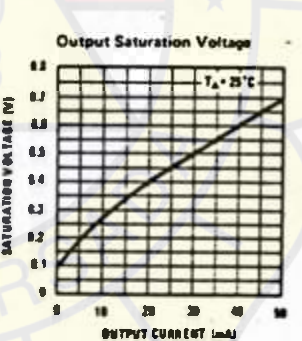
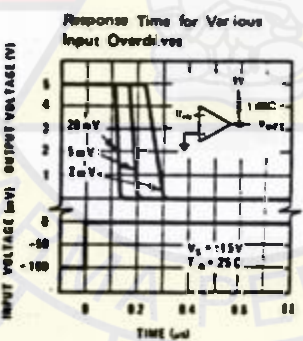
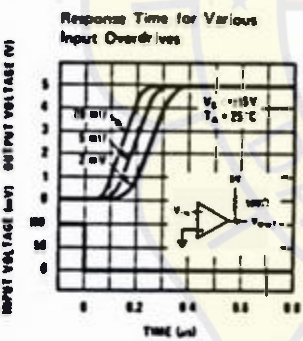
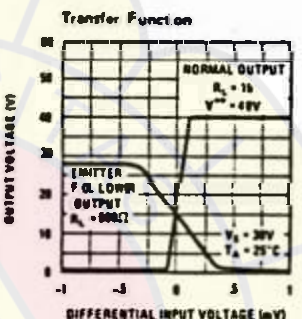
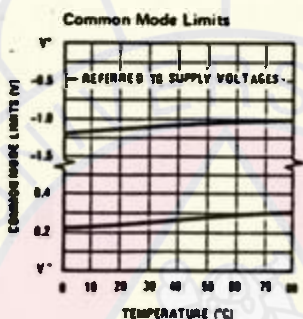
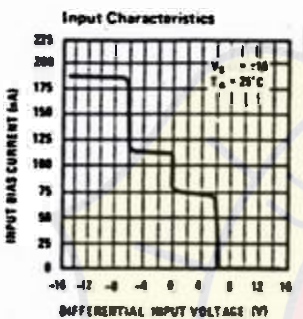
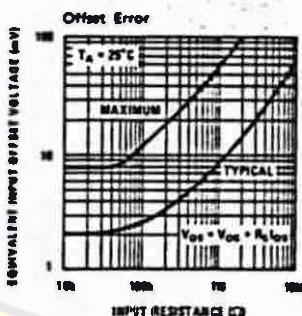
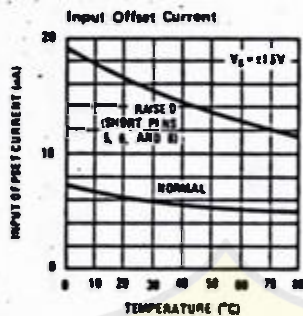
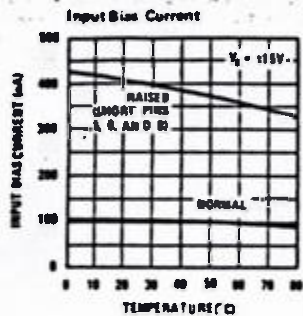
Note 3: These specifications apply for  $V_S = \pm 15V$  and the Ground pin at ground, and  $0^\circ\text{C} < T_A < +70^\circ\text{C}$ , unless otherwise specified. The offset voltage, offset current and bias current specifications apply for any supply voltage from a single 5V supply up to  $\pm 15V$  supplies.

Note 4: The offset voltages and offset currents given are the maximum values required to drive the output within one volt of either supply with 1 mA load. Thus, these parameters define an error band and take into account the worst-case effects of voltage gain and input impedance.

Note 5: The response time specified (see definitions) is for a 100 mV input step with 5 mV overdrive.

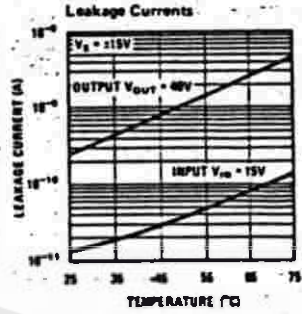
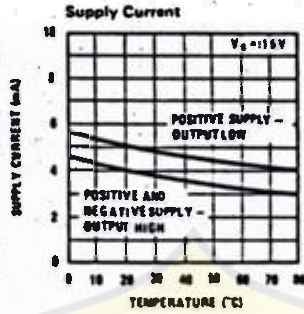
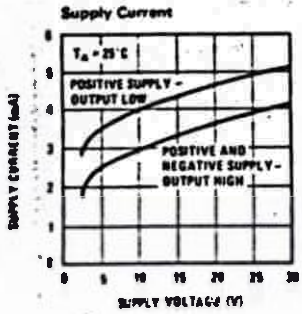
Note 6: Do not short the strobe pin to ground; it should be current driven at 3 to 5 mA.

typical performance characteristics

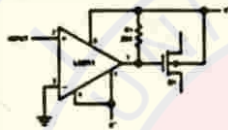




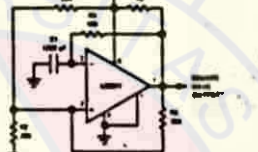
typical performance characteristics (con't)



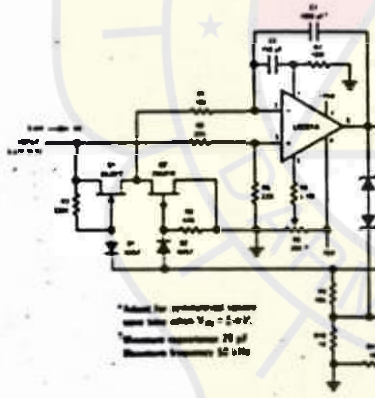
typical applications



Zero Crossing Detector Driving MOS Switch



100 kHz Free Running Multivibrator



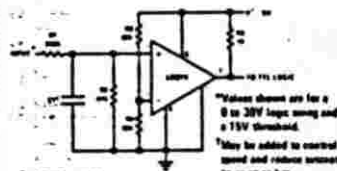
10 Hz to 10 kHz Voltage Controlled Oscillator



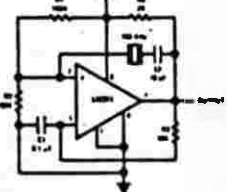
Driving Ground-Referenced Load



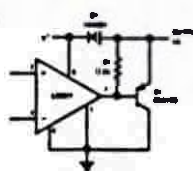
Using Clamp Diodes to Improve Response



TTL Interface with High Level Logic



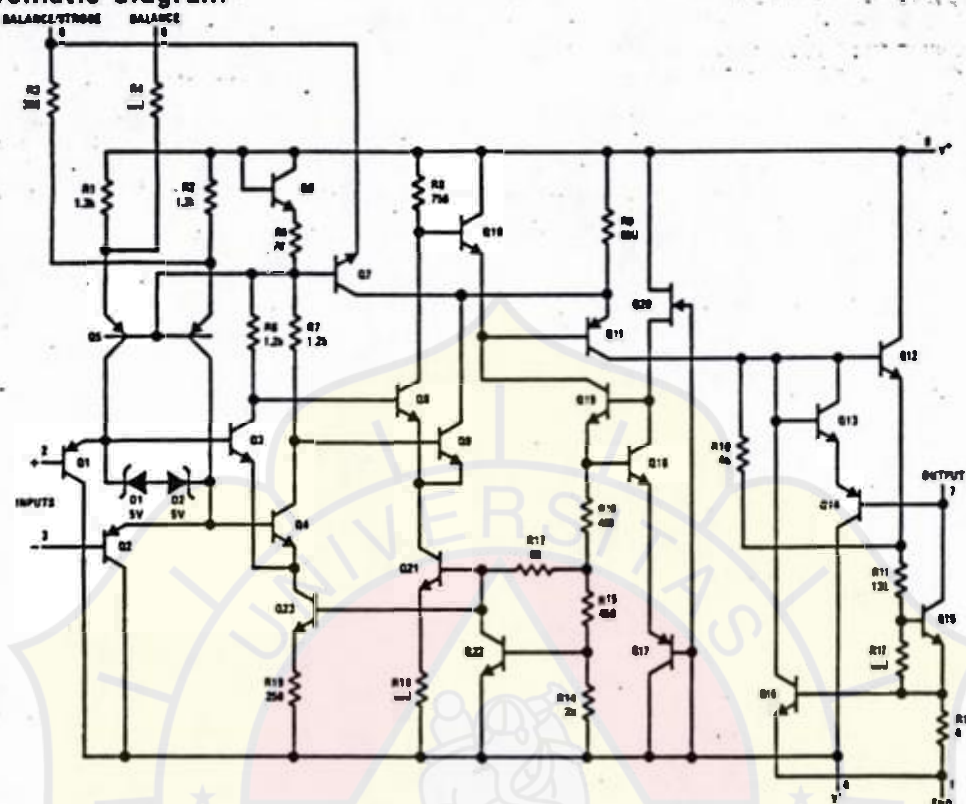
Crystal Oscillator



Comparator and Solenoid Driver

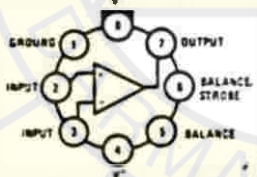


schematic diagram



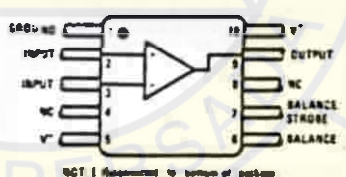
connection diagrams

Metal Can Package



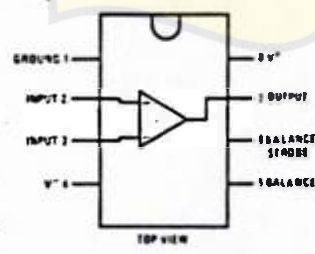
Order Number LM311M  
See NS Package HC8C

Flat Package



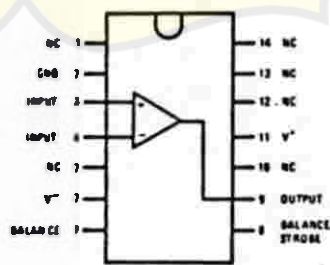
Order Number LM311F  
See NS Package F10A

Dual-In-Line Package



Order Number LM311N  
See NS Package N08B  
Order Number LM311U-8  
See NS Package J08A

Dual-In-Line Package



Order Number LM311D  
See NS Package D14E  
Order Number LM311N-14  
See NS Package N14A  
Order Number LM311J  
See NS Package J14A

\*Pin connections shown on schematic diagram and typical applications are for TO-8 package.

See Pin 8 connected to bottom of package





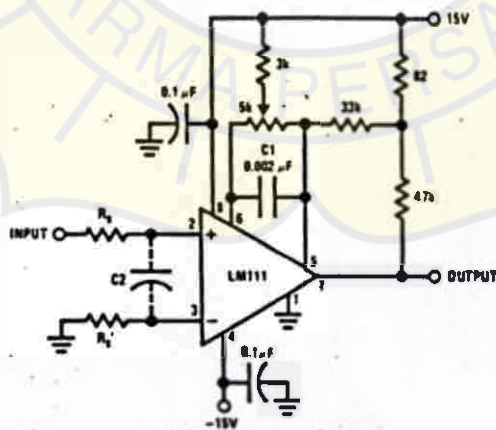
## application hints

## CIRCUIT TECHNIQUES FOR AVOIDING OSCILLATIONS IN COMPARATOR APPLICATIONS

When a high-speed comparator such as the LM111 is used with fast input signals and low source impedances, the output response will normally be fast and stable, assuming that the power supplies have been bypassed (with  $0.1 \mu\text{F}$  disc capacitors), and that the output signal is routed well away from the inputs (pins 2 and 3) and also away from pins 5 and 6.

However, when the input signal is a voltage ramp or a slow sine wave, or if the signal source impedance is high ( $1 \text{ k}\Omega$  to  $100 \text{ k}\Omega$ ), the comparator may burst into oscillation near the crossing-point. This is due to the high gain and wide bandwidth of comparators like the LM111. To avoid oscillation or instability in such a usage, several precautions are recommended, as shown in Figure 1 below.

1. The trim pins (pins 5 and 6) act as unwanted auxiliary inputs. If these pins are not connected to a trim-pot, they should be shorted together. If they are connected to a trim-pot, a  $0.01 \mu\text{A}$  capacitor C1 between pins 5 and 6 will minimize the susceptibility to AC coupling. A smaller capacitor is used if pin 5 is used for positive feedback as in Figure 1.
2. Certain sources will produce a cleaner comparator output waveform if a  $100 \text{ pF}$  to  $1000 \text{ pF}$  capacitor C2 is connected directly across the input pins.
3. When the signal source is applied through a resistive network,  $R_s$ , it is usually advantageous to choose an  $R_s$  of substantially the same value, both for DC and for dynamic (AC) considerations. Carbon, tin-oxide, and metal-film resistors have all been used successfully in comparator input circuitry. Inductive wirewound resistors are not suitable.
4. When comparator circuits use input resistors (eg. summing resistors), their value and placement are particularly important. In all cases the body of the resistor should be close to the device or socket. In other words there should be very little lead length or printed-circuit foil run between comparator and resistor to radiate or pick up signals. The same applies to capacitors, pots, etc. For example, if  $R_s = 10 \text{ k}\Omega$ , as little as 5 inches of lead between the resistors and the input pins can result in oscillations that are very hard to damp. Twisting these input leads tightly is the only (second best) alternative to placing resistors close to the comparator.
5. Since feedback to almost any pin of a comparator can result in oscillation, the printed-circuit layout should be engineered thoughtfully. Preferably there should be a groundplane under the LM111 circuitry, for example, one side of a double-layer circuit card. Ground foil (or, positive supply or negative supply foil) should extend between the output and the inputs, to act as a guard. The foil connections for the inputs should be as small and compact as possible, and should be essentially surrounded by ground foil on all sides, to guard against capacitive coupling from any high-level signals (such as the output). If pins 5 and 6 are not used, they should be shorted together. If they are connected to a trim-pot, the trim-pot should be located, at most, a few inches away from the LM111, and the  $0.01 \mu\text{F}$  capacitor should be installed. If this capacitor cannot be used, a shielding printed-circuit foil may be advisable between pins 6 and 7. The power supply bypass capacitors should be located within a couple inches of the LM111. (Some other comparators require the power-supply bypass to be located immediately adjacent to the comparator.)



Pin connections shown are for LM111 in 8-lead TO-5 hermetic package

FIGURE 1. Improved Positive Feedback

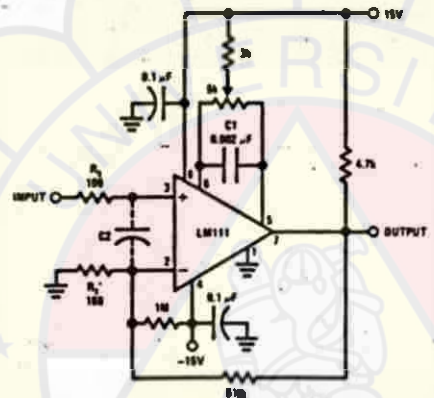
application hints (cont)

6. It is a standard procedure to use hysteresis (positive feedback) around a comparator, to prevent oscillation, and to avoid excessive noise on the output because the comparator is a good amplifier for its own noise. In the circuit of Figure 2, the feedback from the output to the positive input will cause about 3 mV of hysteresis. However, if  $R_5$  is larger than  $100\Omega$ , such as  $50\text{ k}\Omega$ , it would not be reasonable to simply increase the value of the positive feedback resistor above  $510\text{ k}\Omega$ . The circuit of Figure 3 could be used, but it is rather awkward. See the notes in paragraph 7 below.

7. When both inputs of the LM111 are connected to active signals, or if a high-impedance signal is driving the positive input of the LM111 so that positive feedback would be disruptive, the circuit of Figure 1 is

ideal. The positive feedback is to pin 5 (one of the offset adjustment pins). It is sufficient to cause 1 to 2 mV hysteresis and sharp transitions with input triangle waves from a few Hz to hundreds of kHz. The positive-feedback signal across the  $82\Omega$  resistor swings 240 mV below the positive supply. This signal is centered around the nominal voltage at pin 5, so this feedback does not add to the  $V_{OS}$  of the comparator. As much as 8 mV of  $V_{OS}$  can be trimmed out, using the  $5\text{ k}\Omega$  pot and  $3\text{ k}\Omega$  resistor as shown.

8. These application notes apply specifically to the LM111, LM211, LM311, and LF111 families of comparators, and are applicable to all high-speed comparators in general, (with the exception that not all comparators have trim pins).



Pin connections shown are for LM111H in 8-lead TO-5 hermetic package

FIGURE 2. Conventional Positive Feedback

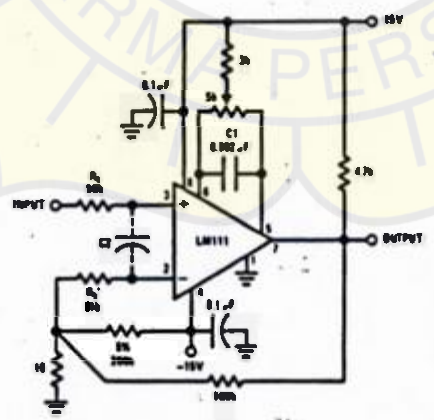


FIGURE 3. Positive Feedback With High Source Resistance



Industrial/Automotive/Functional  
Blocks/ Telecommunications

**LM555/LM555C timer**  
**general description**

The LM555 is a highly stable device for generating accurate time delays or oscillation. Additional terminals are provided for triggering or resetting if desired. In the time delay mode of operation, the time is precisely controlled by one external resistor and capacitor. For astable operation as an oscillator, the free running frequency and duty cycle are accurately controlled with two external resistors and one capacitor. The circuit may be triggered and reset on falling waveforms, and the output circuit can source or sink up to 200 mA or drive TTL circuits.

- Adjustable duty cycle
- Output can source or sink 200 mA
- Output and supply TTL compatible
- Temperature stability better than 0.005% per °C
- Normally on and normally off output

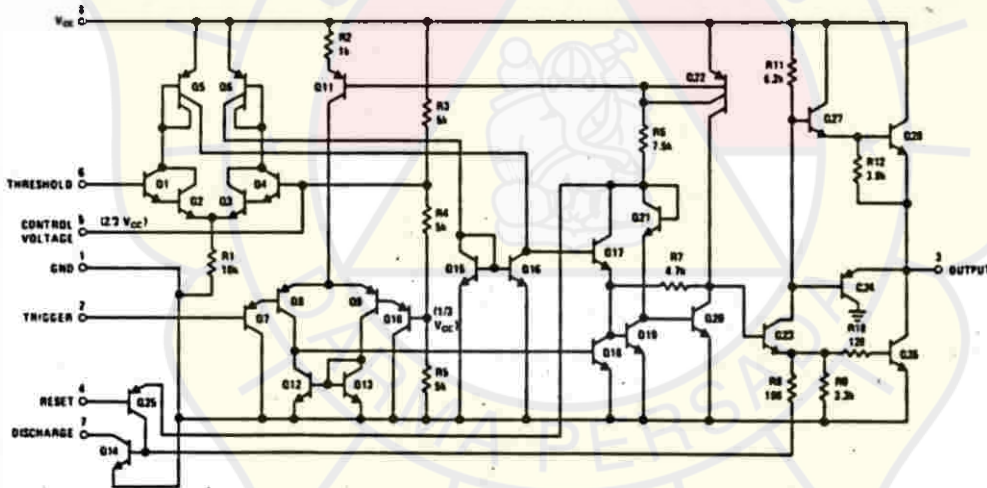
**features**

- Direct replacement for SE555/NE555
- Timing from microseconds through hours
- Operates in both astable and monostable modes

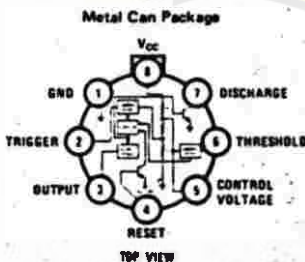
**applications**

- Precision timing
- Pulse generation
- Sequential timing
- Time delay generation
- Pulse width modulation
- Pulse position modulation
- Linear ramp generator

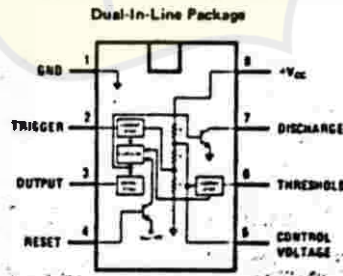
**schematic diagram**



**connection diagrams**



Order Number LM555H, LM555CH  
See NS Package HOBC



Order Number LM555CN  
See NS Package NOB B  
Order Number LM555J or LM555CJ  
See NS Package JOBA



**absolute maximum ratings**

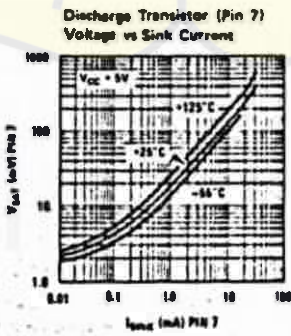
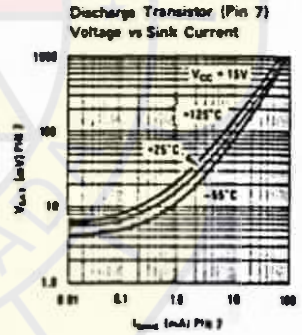
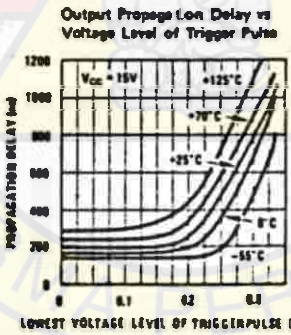
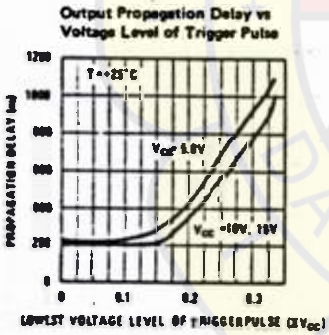
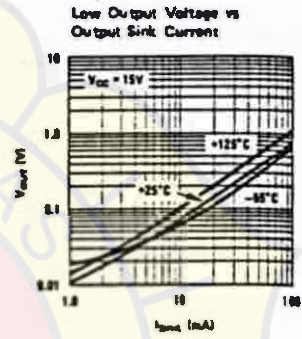
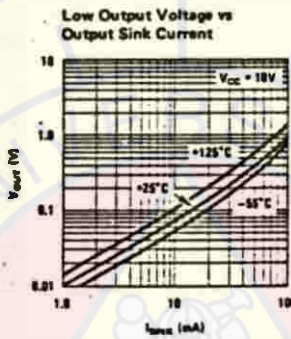
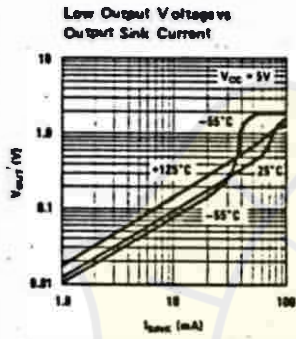
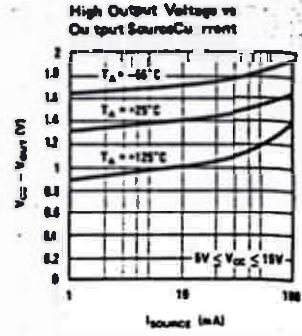
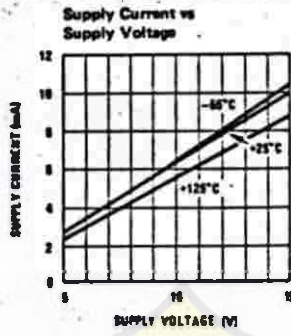
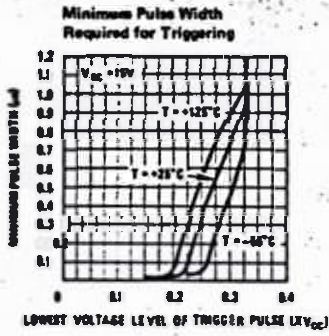
Supply Voltage  $+18\text{ V}$   
 Power Dissipation (Note 1)  $600\text{ mW}$   
 Operating Temperature Ranges  
 LM555C  $0^\circ\text{C to }+70^\circ\text{C}$   
 LM555  $-55^\circ\text{C to }+125^\circ\text{C}$   
 Storage Temperature Range  $-65^\circ\text{C to }+150^\circ\text{C}$   
 Lead Temperature (Soldering, 10 seconds)  $300^\circ\text{C}$

**electrical characteristics** ( $T_A = -25^\circ\text{C}$ ,  $V_{CC} = +5\text{V to }+15\text{V}$ , unless otherwise specified)

PARAMETER	CONDITIONS	LIMITS						UNITS
		LM555			LM555C			
		MIN	TYP	MAX	MIN	TYP	MAX	
Supply Voltage		4.5		18	4.5		18	V
Supply Current	$V_{CC} = 5\text{V}, R_L = \infty$ $V_{CC} = 15\text{V}, R_L = \infty$ (Low State) (Note 2)		3 10		5 12		3 15	mA mA
Timing Error, Monostable			0.5				1	%
Initial Accuracy			30				60	ppm/°C
Drift with Temperature	$R_A, R_B = 1\text{k to }100\text{k}$ , $C = 0.1\mu\text{F}$ , (Note 3)							%
Accuracy over Temperature			1.8				1.5	%
Drift with Supply			0.05				0.1	%/V
Timing Error, Astable			1.5				2.25	%
Initial Accuracy			90				150	ppm/°C
Drift with Temperature			25				30	%
Accuracy over Temperature			0.15				0.30	%/V
Drift with Supply							0.5	%/V
Threshold Voltage			0.667				0.667	$\times V_{CC}$
Trigger Voltage	$V_{CC} = 15\text{V}$ $V_{CC} = 5\text{V}$	4.8 1.45	6 1.67	5.2 1.8		5 1.67		V V
Trigger Current			0.01	0.5		0.5	0.9	$\mu\text{A}$
Reset Voltage		0.4	0.5	1	0.4	0.5	1	V
Reset Current			0.1	0.4		0.1	0.4	mA
Threshold Current	(Note 4)		0.1	0.25		0.1	0.25	$\mu\text{A}$
Control Voltage Level	$V_{CC} = 15\text{V}$ $V_{CC} = 5\text{V}$	9.6 2.9	10 3.33	10.4 3.8	6 1.6	10 3.33	11 4	V V
Pin 7 Leakage Output High			1	100		1	100	nA
Pin 7 Sat (Note 5)								
Output Low	$V_{CC} = 15\text{V}, I_{OL} = 15\text{ mA}$ $V_{CC} = 4.5\text{V}, I_{OL} = 4.5\text{ mA}$		150			180		mV
Output Voltage Drop (Low)	$V_{CC} = 15\text{V}$ $I_{sink} = 10\text{ mA}$ $I_{sink} = 50\text{ mA}$ $I_{sink} = 100\text{ mA}$ $I_{sink} = 200\text{ mA}$ $V_{CC} = 5\text{V}$ $I_{sink} = 8\text{ mA}$ $I_{sink} = 5\text{ mA}$		0.1 0.4 2 2.5	0.15 0.5 2.2		0.1 0.4 2 2.5	0.25 0.75 2.5	V V V V
Output Voltage Drop (High)	$I_{source} = 200\text{ mA}, V_{CC} = 15\text{V}$ $I_{source} = 100\text{ mA}, V_{CC} = 15\text{V}$ $V_{CC} = 5\text{V}$	13	12.5 3.3		12.75 2.75	12.5 3.3		V V V
Rise Time of Output			100			100		ns
Fall Time of Output			100			100		ns

Note 1: For operating at elevated temperatures the device must be derated based on a  $+150^\circ\text{C}$  maximum junction temperature and a thermal resistance of  $+45^\circ\text{C/W}$  junction to case for TO-5 and  $+150^\circ\text{C/W}$  junction to ambient for both packages.  
 Note 2: Supply current when output high typically 1 mA less at  $V_{CC} = 5\text{V}$ .  
 Note 3: Tested at  $V_{CC} = 5\text{V}$  and  $V_{CC} = 15\text{V}$ .  
 Note 4: This will determine the maximum value of  $R_A$  or  $R_B$  for 15V operation. The maximum total ( $R_A + R_B$ ) is 20 M $\Omega$ .  
 Note 5: No protection against excessive pin 7 current is necessary provided the package dissipation rating will not be exceeded.

typical performance characteristics





**applications information**

**MONOSTABLE OPERATION**

In this mode of operation, the timer functions as a one-shot (Figure 1). The external capacitor is initially held discharged by a transistor inside the timer. Upon application of a negative trigger pulse of less than  $1/3V_{CC}$  to pin 2, the flip-flop is set which both releases the short circuit across the capacitor and drives the output high.

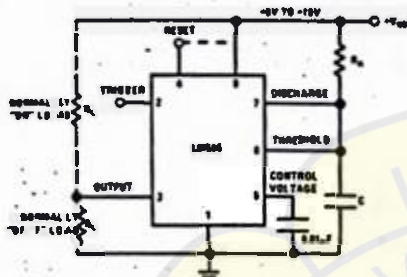


FIGURE 1. Monostable

The voltage across the capacitor then increases exponentially for a period of  $t = 1.1 R_A C$ , at the end of which time the voltage equals  $2/3 V_{CC}$ . The comparator then resets the flip-flop which in turn discharges the capacitor and drives the output to its low state. Figure 2 shows the waveforms generated in this mode of operation. Since the charge and the threshold level of the comparator are both directly proportional to supply voltage, the timing interval is independent of supply.



FIGURE 2. Monostable Waveforms

During the timing cycle when the output is high, the further application of a trigger pulse will not effect the circuit. However the circuit can be reset during this time by the application of a negative pulse to the reset terminal (pin 4). The output will then remain in the low state until a trigger pulse is again applied.

When the reset function is not in use, it is recommended that it be connected to  $V_{CC}$  to avoid any possibility of false triggering.

Figure 3 is nomograph for easy determination of R, C values for various time delays.

**ASTABLE OPERATION**

If the circuit is connected as shown in Figure 4 (pins 2 and 6 connected) it will trigger itself and free run as a

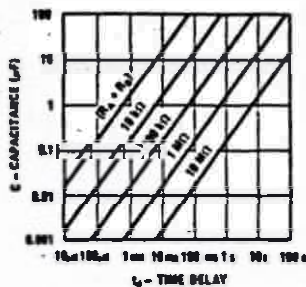


FIGURE 3. Time Delay

multivibrator. The external capacitor charges through  $R_A + R_B$  and discharges through  $R_B$ . Thus the duty cycle may be precisely set by the ratio of these two resistors.

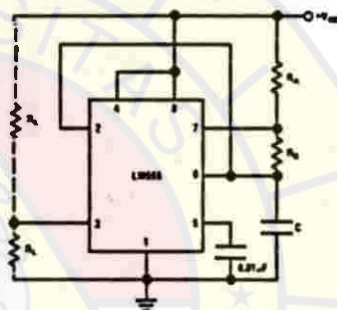


FIGURE 4. Astable

In this mode of operation, the capacitor charges and discharges between  $1/3 V_{CC}$  and  $2/3 V_{CC}$ . As in the triggered mode, the charge and discharge times, and therefore the frequency are independent of the supply voltage.

Figure 5 shows the waveforms generated in this mode of operation.

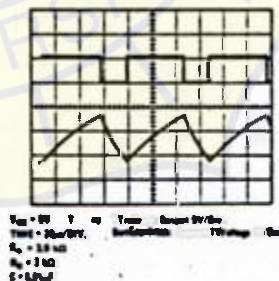


FIGURE 5. Astable Waveforms

The charge time (output high) is given by:  
 $t_1 = 0.693(R_A + R_B)C$

And the discharge time (output low) by:  
 $t_2 = 0.693(R_B)C$

Thus the total period is:  
 $T = t_1 + t_2 = 0.693(R_A + 2R_B)C$

applications information (con't)

The frequency of oscillation is:

$$f = \frac{1}{T} = \frac{1.44}{(R_A + 2R_B)C}$$

Figure 6 may be used for quick determination of these RC values.

The duty cycle is: 
$$D = \frac{R_B}{R_A + 2R_B}$$

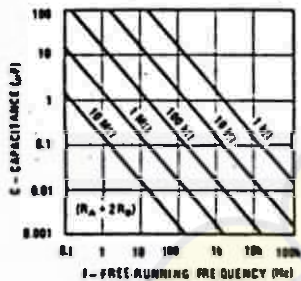


FIGURE 6. Free Running Frequency

FREQUENCY DIVIDER

The monostable circuit of Figure 1 can be used as a frequency divider by adjusting the length of the timing cycle. Figure 7 shows the waveforms generated in a divide by three circuit.

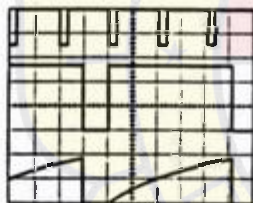


FIGURE 7. Frequency Divider

PULSE WIDTH MODULATOR

When the timer is connected in the monostable mode and triggered with a continuous pulse train, the output pulse width can be modulated by a signal applied to pin 5. Figure 8 shows the circuit, and in Figure 9 are some waveform examples.

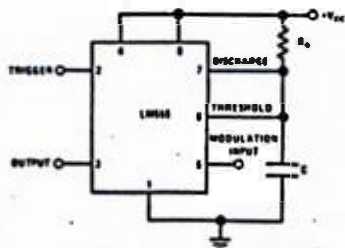


FIGURE 8. Pulse Width Modulator

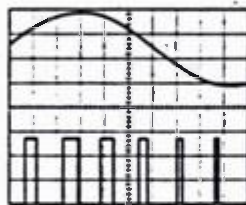


FIGURE 9. Pulse Width Modulator

PULSE POSITION MODULATOR

This application uses the timer connected for astable operation, as in Figure 10, with a modulating signal again applied to the control voltage terminal. The pulse position varies with the modulating signal, since the threshold voltage and hence the time delay is varied. Figure 11 shows the waveforms generated for a triangle wave modulation signal.

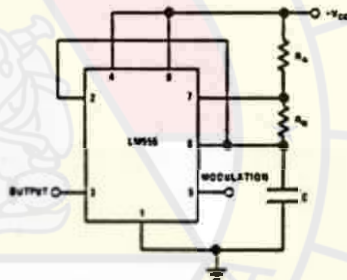


FIGURE 10. Pulse Position Modulator



FIGURE 11. Pulse Position Modulator

LINEAR RAMP

When the pullup resistor, RA, in the monostable circuit is replaced by a constant current source, a linear ramp is

## applications information (con't)

generated. Figure 12 shows a circuit configuration that will perform this function.

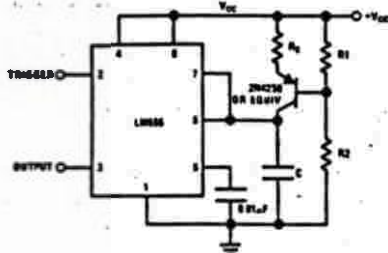


FIGURE 12.

Figure 13 shows waveforms generated by the linear ramp.

The time interval is given by:

$$T = \frac{2/3 V_{CC} R_E (R_1 + R_2) C}{R_1 V_{CC} - V_{BE} (R_1 + R_2)}$$

$$V_{BE} = 0.6V$$



$V_{CC} = 9V$   
 $T_{RMS} = 20\mu s/div$   
 $R_1 = 0.1 M\Omega$   
 $R_2 = 100 k\Omega$   
 $R_E = 0.7 M\Omega$   
 $C = 0.01\mu F$

Top Trace: Input 2V/div.  
 Middle Trace: Output 1V/div.  
 Bottom Trace: Capacitor Voltage 1V/div.

FIGURE 13. Linear Ramp

### 50% DUTY CYCLE OSCILLATOR

For a 50% duty cycle, the resistors  $R_A$  and  $R_B$  may be connected as in Figure 14. The time period for the out-

put high is the same as previous,  $t_1 = 0.693 R_A C$ . For the output low it is  $t_2 =$

$$[(R_A R_B) / (R_A + R_B)] \ln \left[ \frac{R_B - 2R_A}{2R_B - R_A} \right]$$

Thus the frequency of oscillation is  $f = \frac{1}{t_1 + t_2}$

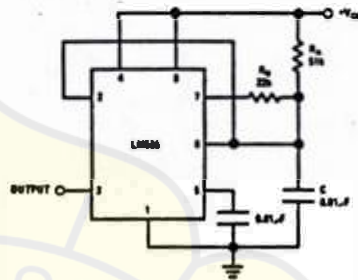


FIGURE 14. 50% Duty Cycle Oscillator

Note that this circuit will not oscillate if  $R_B$  is greater than  $1/2 R_A$  because the junction of  $R_A$  and  $R_B$  cannot bring pin 2 down to  $1/3 V_{CC}$  and trigger the lower comparator.

### ADDITIONAL INFORMATION

Adequate power supply bypassing is necessary to protect associated circuitry. Minimum recommended is  $0.1\mu F$  in parallel with  $1\mu F$  electrolytic.

Lower comparator storage time can be as long as  $10\mu s$  when pin 2 is driven fully to ground for triggering. This limits the monostable pulse width to  $10\mu s$  minimum.

Delay time reset to output is  $0.47\mu s$  typical. Minimum reset pulse width must be  $0.3\mu s$ , typical.

Pin 7 current switches within 30 ns of the output (pin 3) voltage.











