

BAB X

PENUTUP

X.1. Kesimpulan

1. Dari hasil perhitungan yang telah dilakukan untuk kapal rancangan dengan ukuran utama sebagai berikut :

- Tipe : General Cargo 700 DWT
- Dimensi :
 - a. *Length Over All* (LOA) = 62,50 m
 - b. *Length Water Line* (LWL) = 56,96 m
 - c. *Length Between Perpendicular* (LPP) = 55,42 m
 - d. *Breadth Moulded* (B mld) = 9,60 m
 - e. *Height Moulded* (H mld) = 4,90 m
 - f. *Draft Moulded* (T mld) = 3,44 m
 - g. *Coefficient Block* (Cb) = 0,72
 - h. *Coefficient Midship* (Cm) = 0,99
 - i. *Coefficient Waterline* (Cw) = 0,804
 - j. *Coefficient Prismatic* (Cp) = 0,73
 - k. *Speed* (Vs) = 11,00 Knots
- Rute Pelayaran : Surabaya – Makasar (595 mil)

Motor penggerak utama dipilih mesin diesel empat langkah dengan spesifikasi sebagai berikut :

- Merk : YANMAR
- Type : 6AYM - WET
- Jumlah silinder : 6
- Bore & Stroke : 155 x 180 (mm)
- Daya : 755 HP (555 KW)
- Putaran Mesin : 1840 Rpm
- Berat mesin : 2365 Kg
- Konsumsi bahan bakar (Sfoc) : 202 gr/kW.h
- Dimensi : 1823 × 1305 × 1431 (mm)

Marine Gear specification

- Merk : YANMAR
- Model : YXH – 240L
- Reduction Ratio : 1 : 6,95
- Berat Gear : 1240 Kg

Dan 2 unit mesin generator dengan merk:

Spesifikasi Generating set

- Merk / Tipe = YANMAR 6HAL2-WHT
- Daya motor = 144 kW/180 kVA
- RPM = 1200 rpm
- Jumlah silinder = 4
- Cylinder (bore x stroke) = 130 x 165
- Dimensi = 2574 x 1164 x 1804 mm
- Jumlah = 2 unit

Mesin – mesin pendukung kerja mesin induk antara lain :

➤ Kompresor udara

- Merk = DongHwa Pnetec
- Type = CMS-85
- Kapasitas = 21 m³/jam
- Jenis = Vertical 1 cylinder
- Putaran = 1000 RPM
- Daya = 7,5 KW
- Jumlah = 2 buah

➤ Spesifikasi Fuel Oil Transfer Pump

- Merk : TAIKO, Type NHG-4
- Kapasitas : 4 m³/jam
- Daya : 1,5 kW
- Jenis : Gear Pump
- Head : 18-31 m

➤ Spesifikasi Fuel Oil Supply Pump

Merk : TAIKO, Type NHG-4
Kapasitas : 4 m³/jam
Daya : 1,5 kW
Jenis : Gear Pump
Head : 18-31 m

➤ Spesifikasi Lubricating Oil Pump

Merk : TAIKO, Type NHG-5
Kapasitas : 5 m³/jam
Daya : 2,2 kW
Head : 17-41 m
Jenis : Gear Pump

➤ Spesifikasi Fresh Water Cooling Pump

Merk : Taiko, Type TMC-65C
Head : 22 - 30 m
Kapasitas : 10-40 m³/jam
Daya : 3,7 kW
Jenis : Centrifugal Pump

➤ Spesifikasi Sea Water Cooling Pump

Merk : Taiko, Type TMC-65C
Head : 22 - 30 m
Kapasitas : 10-40 m³/jam
Daya : 3,7 kW
Jenis : Centrifugal Pump

➤ Spesifikasi Bilge Pump

Merk : Taiko, Type TMS-65C
Head : 29-35 m
Kapasitas : 16-35 m³/jam
Daya : 7,7 kW
Jenis : Centrifugal Pump

➤ Spesifikasi Ballast Pump

Merk : Taiko, Type EHS-51B
Head : 29-45 m
Kapasitas : 8-20 m³/jam
Daya : 5,5 kW
Jenis : Centrifugal Pump

➤ Spesifikasi F.W. Sanitary Pump

Merk : Taiko, Type TMC-32
Head : 20-32 m
Kapasitas : 2-6,5 m³/jam
Daya : 1,5 kW
Jenis : Centrifugal Pump

➤ Spesifikasi S.W. Sanitary Pump

Merk : Taiko, Type TMC-32
Head : 20-32 m
Kapasitas : 2-6,5 m³/jam
Daya : 1,5 kW
Jenis : Centrifugal Pump

➤ Spesifikasi Sanitary discharge Pump

Merk : Taiko, Type TMC-32
Head : 20-32 m
Kapasitas : 2-6,5 m³/jam
Daya : 1,5 kW
Jenis : Centrifugal Pump

➤ Spesifikasi Fire Pump

Merk : Taiko, Type VS-100
Head : 15-46 m
Kapasitas : 20-60 m³/jam
Daya : 7,5 kW
Jenis : Centrifugal Pump

- Mesin Kemudi
 - Merek : Taiyo
 - Type : ITS
- Mesin Jangkar
 - Merek : Nautiservo B.V
 - Type : 722. 01E
- Mesin Capstan
 - Merek : Nautiservo B.V
 - Type : 6000 E

2. Dalam perencanaan kamar mesin tidak lepas dari asumsi-asumsi yang diberikan untuk mempermudah perhitungan dengan tidak mengabaikan tanggung jawab secara teknis, ekonomis, serta peraturan-peraturan yang ada sehingga hasil perhitungan dapat mendekati keadaan sebenarnya.
3. Tata letak mesin induk, mesin bantu, kompresor, pompa serta permesinan lainya diatur seefisien mungkin. Hal ini untuk mempermudah dalam hal perawatan dan perbaikan peralatan yang ada dikamar mesin.

X.2. Saran

Setelah melakukan perhitungan-perhitungan diatas dan dari pengalaman selama menyusun tugas perancangan mesin kapal, maka penulis dapat menyarankan sebagai berikut :

1. Mohon mahasiswa dibekali dengan pengetahuan yang lebih tentang perancangan mesin kapal serta referensi buku-buku panduan yang dapat membantu mahasiswa dalam menyelesaikan tugas perancangan ini.
2. Dalam menyelesaikan tugas merancang mesin kapal ini, pengalaman studi lapangan sangat membantu. Untuk disarankan agar lebih banyak mengadakan studi lapangan agar tugas perancangan ini dapat mudah dipahami dan diselesaikan dengan baik.
3. Mahasiswa harus mencari ilmu diluar kampus tentang dunia perkapalan agar mahasiswa mengetahui teknologi dan perkembangan industri dalam dunia perkapalan secara *up date*. Hal ini sangat berguna untuk menghadapi dunia persaingan kerja yang semakin ketat.
4. Adanya peningkatan sumber daya manusia dalam dunia perkapalan, melalui media pendidikan dan pelatihan-pelatihan sehingga diharapkan tidak menggunakan tenaga asing.
5. Pihak Jurusan mengadakan pusat informasi tentang Regulasi – regulasi terbaru khususnya tentang perencanaan kapal Cargo, maupun kapal-kapal lain pada umumnya.

DAFTAR NOTASI

Tabulasi berikut menunjukkan simbol yang digunakan pada tugas merancang kapal ini. Karena huruf terbatas, kadang kala huruf yang sama digunakan untuk menyatakan lebih dari satu konsep.

a	: Jumlah maksimum block diantara Davit Guide roller dan WinchHead.
A	: Luas pandangan samping lambung kapal (m^2), luas daun kemudi.
α	: Sudut putar daun kemudi.
a_0	: Jarak gading – gading (mm).
A_{rudder}	: Luas daun kemudi (m^2).
A_m	: Luas penampang melintang tengah kapal (m^2).
A_{wl}	: Luas bidang garis air (m^2).
b	: Lebar daun kemudi (m).
B	: Lebar kapal, lebar tangki (m).
BHP	: Brake Horse Power (HP).
B/T	: Perbandingan lebar dan sarat kapal.
B_p	: Koefisien baling-baling dengan diagram $B_p-\delta$.
c	: Lebar daun kemudi dalam (m), jumlah minimum block.
C_A	: Koefisien penambahan hambatan untuk korelasi model - kapal.
C_{AA}	: Koefisien hambatan udara.
C_{AS}	: Koefisien hambatan kemudi.
C_b	: Koefisien blok.
C_F	: Koefisien hambatan gesek.
$C_{f_{wc}}$: Kebutuhan air tawar untuk pendinginan motor induk.
$C_{f_{wd}}$: Kebutuhan air tawar untuk makan dan minum.
$C_{f_{ww}}$: Kebutuhan air tawar untuk cuci dan mandi.
C_m	: Koefisien tengah kapal.
C_p	: Koefisien prismatik memanjang.
C_R	: Koefisien hambatan sisa; Gaya pada daun kemudi.
C_T	: Koefisien hambatan total.
C_W	: Koefisien garis air kapal.
C_1	: Faktor untuk kapal.
C_2	: Faktor untuk kemudi.
C_3	: Faktor untuk profile kemudi.
C_4	: Faktor untuk perencanaan kemudi.



d	: Diameter poros dalam (m), diameter rantai (inch).
D	: Displasemen kapal (ton), volume rata-rata pemakaian air, diameter silinder mesin.
d_b	: Diameter pipa ballast.
D_{cl}	: Diameter efektif cable lifter (mm).
D_{BT}	: Diameter Bow Trushter.
D_h	: Diameter pipa utama (mm), diameter winch head.
D_o	: Diameter optimum baling-baling (m).
D_{prop}	: Diameter baling-baling (m).
D_t	: Diameter tongkat kemudi (mm).
D_T	: Diameter Tentativ.
d_w	: Diameter tali tambat (mm).
D_{we}	: Diameter penggerak tali.
d_z	: Diameter pipa cabang (mm).
Δ	: Displasemen kapal (ton).
Δ_p	: Head perbedaan tekanan (bar).
δ_K	: Koreksi Advance Coefficient
EHP	: Efektif Horse Power (HP).
η_a	: Efisiensi mekanis dengan spin gear.
η_{bw}	: Efisiensi boat winch.
η_{cl}	: Efisiensi cable lifter.
η_f	: Efisiensi alat penurunan sekoci.
η_g	: Efisiensi generator.
η_H	: Efisiensi badan kapal $(1 - t) / (1 - w)$.
η_o	: Efisiensi baling-baling dari percobaan model.
η_p	: Efisiensi baling-baling.
η_r	: Efisiensi untuk davit guide roller.
η_{rr}	: Efisiensi rotary relatif.
η_s	: Efisiensi untuk snatch block.
η_{sg}	: Efisiensi untuk electric steering gear.
η_w	: Efisiensi dari sistem transmisi.
ϵ	: Koefisien yang tergantung pada perbandingan diameter block dengan diameter penjatuh tackle.

F	: Faktor untuk instalasi propulsi (Disk Area of Screw).
F_{disk}	: Area of the screw (m^2), letak lambung timbul untuk fresh water, loadline.
F_a	: Developed blade area (m^2).
F_a/F	: Blade area ratio propeller.
F_n	: Angka froude
F_p	: Fore perpendicular (garis tegak haluan).
F_p	: Projected area of the blades (m^2).
g	: Gaya gravitasi $9,81 m/dt^2$.
G_a	: Berat jangkar (kg).
γ	: Berat jenis air laut $1,025 t/m^3$.
γ_{fo}	: Berat jenis bahan bakar $0,9 ton/m^3$.
H	: Jarak ordinat ($L_{pp}/station$), tinggi bangunan atas, tinggi centre girder, tinggi efektif diukur dari garis muat sampai puncak teratas rumah geladak dalam (m), deck load (beban geladak) kN/m^2 .
H	: Tinggi kapal (m).
H_a	: Head statis total (m).
H_{lf}	: Head loss karena pipa hisap (m).
H_{li}	: Head loss karena peralatan pipa hisap (m).
H_{rudder}	: Tinggi daun kemudi (m).
H_t	: Head total.
H_o/D	: Pitch ratio baling-baling.
i_a	: Ratio mekanisme gigi.
i_{bw}	: Perbandingan putaran motor dan putaran winch head.
J	: Kapasitas total bejana (dm^3).
k	: Faktor tipe dari poros.
k_r	: Faktor bahan tergantung dari kekuatan tarik.
k_{re}	: Jumlah penggantian udara supply/exhaust.
k_t	: Koefisien tergantung daya dorong.
k_1	: Koefisien luas daun kemudi.
k_2	: Koefisien profile / model kemudi.
k_3	: Koefisien letak daun kemudi.
L	: Jarak memanjang tangki, panjang ruangan (m), berat barang bawaan (kg).



L_a	: Panjang rantai jangkar yang menggantung (m).
λ	: Koefisien gesek pipa.
LCB	: Jarak/letak titik tekan memanjang dari tengah kapal (m).
LOA	: Length over all (panjang keseluruhan) (m).
LPP	: Length between perpendicular (panjang antara garis tegak) (m).
LWL	: Length water line (panjang garis air dalam) (m).
$L/\nabla^{1/3}$: Rasio panjang - displasemen.
m	: Jumlah total block pada alat penurunan sekoci.
M_{cl}	: Momen putar pada cable lifter (kg.m).
M_m	: Momen putar pada poros motor (kg.cm), torsi pada penggulung.
M_{mb}	: Torsi pada motor listrik.
M_h	: Torsi pada poros winch head.
n	: Jumlah station, putaran baling-baling per detik (rps).
n_m	: Putaran motor untuk electric windlass.
n_h	: Putaran pada winch head.
N_k	: Koreksi Putaran baling-baling (rpm).
N_e	: Daya efektif windlass/Capstan (HP).
N_{eu}	: Daya pada sistem supply/exhaust.
N_m	: Daya motor penggerak (HP).
N_{rs}	: Putaran motor penggerak.
N_w	: Putaran poros penggulung tali (rpm).
$P_o - e$: Tekanan statik pada sumbu baling-baling (lbs/sg.ft).
P	: Berat rata-rata ABK (kg), tekanan discharge.
P_a	: Berat rantai jangkar pada saat bergerak (kg/mm).
P_B	: Brake Horse Power (HP).
P_C	: Propulsive coefisient.
P_m	: Tekanan maksimum dalam tangki (m^3 /jam).
P_{maks}	: Daya maksimum dari pemakaian beban (kW).
P_{me}	: Tekanan kerja efektif silinder (bar).
P_n	: Gaya yang bekerja pada daun kemudi (kg).
P_o	: Tekanan minimum dalam tangki (kg/m^3).
P_s	: Shaft Horse Power (HP).
P_w	: Tenaga winch yang dibutuhkan tegangan tali.
ϕ_h	: Head factor.

Q	: Kapasitas kompresor, beban tambahan akibat tenaga kinetic.
Q _b	:Berat penuh rigged boat, kapasitas pompa bilga, kapasitas pompa ballast.
Q _{displ}	: Koefisien Prismatic displacement.
Q _r	: Momen torsi motor penggerak/daun kemudi.
Q _p	: Berat total penumpang.
Q _{pk}	: Kapasitas pompa pemadam kebakaran.
Q _u	: Kapasitas udara kamar mesin.
R	: Jari-jari propeller, radius pelayaran.
R _{AA}	: Hambatan udara (kg).
R _{br}	: Tegangan putus tali (kg/m ²).
R _F	: Hambatan gesek (kg).
R _e	: Angka Reynolds (Aliran laminar).
ρ	: Massa density 104,49 kg S ² /m ³ .
ρ _u	: Massa density udara.
R _m	: Kekuatan tarik material (N/mm ²).
R _n	: Reynolds number.
R _r	: Hambatan sisa (kg).
R _T	: Hambatan total (kg).
S	: Luas permukaan basah badan kapal (m ²).
S ^l	: Permukaan basah badan dan anggota badan kapal sepanjang garis air (m ²).
SFC	: Specific fuel oil consumption (g/kW.h).
SHP	: Shaft Horse Power (HP).
σ _v	: Angka kavitasi.
σ _{0,7}	: Konstanta kavitasi (0,7 R).
T	:Sarat kapal, lambung timbul untuk tropical load line (m), gaya dorong(kg).
t	:Tebal pelat dalam (mm), faktor pengisapan Taylor, lamanya pelayaran.
τ	: koefisien gaya dorong.
T _{cl}	: Gaya tarik pada cable lifter.
T _{max}	: Tegangan maksimum dari winch head.
T _{min}	: Tegangan minimum dari winch head.
T _w	: Tegangan putus tali.

V_a	: Kecepatan maju baling-baling (knot).
V_b	: Kecepatan aliran masuk ke pompa.
V_{ca}	: Kandungan CO_2 tiap m^3 udara luar yang masuk ruangan.
$V_{do AE}$: Volume bahan bakar motor bantu (m^3).
V_{db}	: Volume total tangki ballast (m^3).
V_e	: Kecepatan air masuk ke baling – baling (m/dtk).
V_{fo}	: Volume bahan bakar motor induk (m^3).
V_h	: Volume langkah torak tiap – tiap silinder (dm^3), volume tangki Hydrophore (m^3)
V_{lo}	: Volume tangki minyak lumas (m^3).
V_o	: Volume fluida sisa (m^3).
V_r	: Kandungan maksimum CO_2 yang dihasilkan dari ruangan (lt/m^3), kecepatan penurunan sekoci.
V_{re}	: Volume CO_2 yang dihasilkan tiap – tiap m^3 dari ruangan (lt/m^3).
V_s	: Kecepatan kapal (knot, m/dt), kecepatan aliran dalam pipa.
V_{setl}	: Volume tangki settling (m^3).
V_{serv}	: Volume tangki service (m^3).
∇_{Displ}	: Volume Displacement dalam (m^3).
V_w	: Kecepatan tarik capstan (m/s).
w	: Faktor arus ikut Taylor.
W_{fo}	: Berat bahan bakar (ton).
W_{fw}	: Berat air tawar (ton).
W_{fvc}	: Berat air untuk pendinginan motor (ton).
W_{fvd}	: Berat air tawar untuk makan dan minum (ton).
W_{fww}	: Berat air tawar untuk cuci dan mandi (ton).
W_{lo}	: Berat minyak pelumas (ton).
W_{fwd}	: Kebutuhan air tawar untuk makan dan minum (ton).
Z	: Angka petunjuk untuk jangkar, jumlah daun baling-baling, jumlah silinder motor induk.
Z_c	: Jumlah ABK.

DAFTAR PUSTAKA

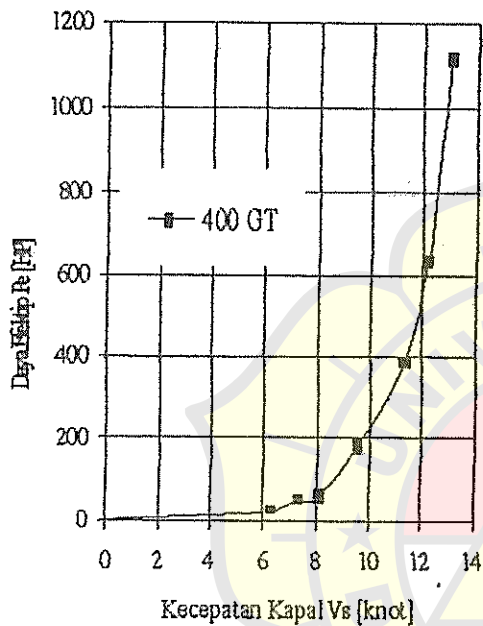
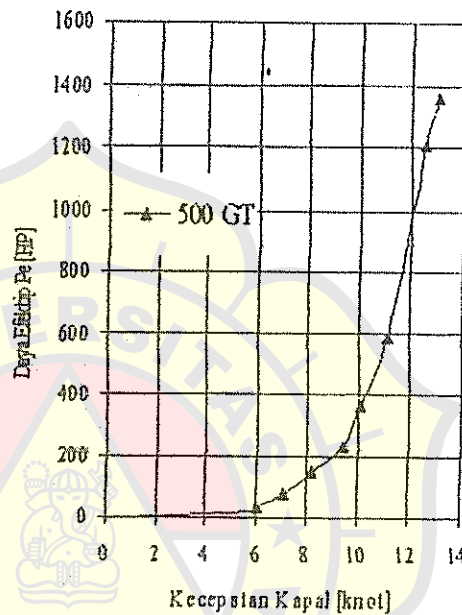
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REFERENSI BAB II



Tabel-8.4 Hasil *Resistance Test* Kapal Ferry Ro-Ro 500 GT (September 1990)⁶⁹

Run no.	v_M [m/dt]	F_r	V_s [m/dt]	V_s [knot]	R_{TM} [N]	$C_{TM} \times 10^{-3}$	$C_{TS} \times 10^{-3}$	R_{TS} [kN]	Effective Power P_E [HP]
1	0,6949	0,1554	3,1078	6,0416	1,6520	4,8690	2,6181	7,2931	30,8254
2	0,8165	0,1823	3,6514	7,0984	2,8347	6,0526	3,8944	14,9751	74,3654
3	0,9421	0,2106	4,2133	8,1907	4,4490	7,1346	5,0545	25,8780	148,2844
4	1,0781	0,2410	4,8215	9,3729	5,9271	7,2585	5,2484	35,1875	230,7311
5	1,1567	0,2586	5,1729	10,0562	8,0898	8,6065	6,6317	51,1806	360,0663
6	1,2796	0,2861	5,7225	11,1245	11,3947	9,9060	7,9804	75,3698	586,5702
7	1,4404	0,3220	6,4416	12,5225	19,5207	13,3927	11,5228	137,8955	1208,0451
8	1,4944	0,3341	6,6833	12,9923	21,0922	13,4431	11,5901	149,3042	1357,0697

Gb.8.3b Kurva $P_E - V_s$ Ferry Ro-Ro prototipe 400 GTGb.8.3c Kurva $P_E - V_s$ Ferry Ro-Ro prototipe 500 GT

Dari teori Propulsi diketahui, daya yang dibutuhkan masing-2 poros baling-2 *Shaft Horse Power SHP* [HP] atau *Shaft Power P* [kW] terkait dengan daya efektif P_E untuk suatu kecepatan kapal V_s adalah sbb.:

- kapal berbaling-baling tunggal (*single screw*): $P = P_E \cdot (P.C.)^{-1}$ ✓
- kapal berbaling-baling ganda (*twin screw*): $P = \frac{1}{2} P_E \cdot (P.C.)^{-1}$

dimana :

$P.C = \text{propulsive coefficient}$ (= *total propulsive efficiency*) dari kapal ;

Dalam praktek biasanya diberikan tambahan yakni *service allowance* atau juga disebut *load fraction* = x , sehingga formulasi menjadi sbb.:

- kapal *single screw* : $P = P_E (1+x) \cdot (P.C.)^{-1}$ ✓
- kapal *twin screw* : $P = \frac{1}{2} P_E (1+x) \cdot (P.C.)^{-1}$

Adapun daya yang diberikan kepada baling-2 yakni *Delivered Shaft Horse Power* disingkat *Delivered Horse Power DHP* [HP] atau P_D [kW], rumusnya adalah sbb.:

- kapal berbaling-baling tunggal (*single screw*): $P_D = P_E \cdot (\eta_D)^{-1}$
- kapal berbaling-baling ganda (*twin screw*) : $P_D = \frac{1}{2} P_E \cdot (\eta_D)^{-1}$

dimana :

$\eta_D = \text{propulsive efficiency}$ (= *quasi propulsive coefficient = QPC*) dari kapal ;

Adapun harga P.C didapatkan dari formulasi :

$$P.C = \eta_H \cdot \eta_O \cdot \eta_{RR} = \eta_H \cdot \eta_P$$

dimana :

- η_H = efisiensi badan kapal (*hull efficiency*) = $(1 - w) / (1 - t)$
- w = fraksi arus ikut (*wake fraction*)
- t = faktor deduksi gaya dorong (*thrust deduction factor*)
- η_P = efisiensi baling-2 pada kondisi berada di buritan kapal (*propeller efficiency in behind condition*)
- η_O = efisiensi baling-2 yang diperoleh dari percobaan model *'open water test'* (*propeller efficiency in open condition*)
- η_{RR} = faktor koreksi η_O menjadi η_P (*relative rotative efficiency*)

Untuk keperluan praktis harga $P.C \approx \eta_D$

Dengan rumus pendekatan Taylor harga-2 w dan t dapat dihitung sbb. :

- kapal *single screw* : $w = -0,05 + 0,50 C_b$
 $t = k \cdot w$

dimana C_b = *block coefficient* dan

koeffisien $k = 0,55 \sim 0,70$, yakni : $k = 0,55$ untuk kapal dengan daun kemudi tipis ;
 $k = 0,70$ untuk kapal dengan daun kemudi tebal.

- kapal *twin screw* : $w = -0,20 + 0,55 C_b$
 $t \approx w$

Bila harga-2 w dan t telah didapatkan dengan rumus diatas, maka besarnya η_H dapat dihitung. Sedangkan harga η_O *propeller efficiency in open condition* η_D dapat diasumsikan $0,50 \sim 0,65$, sedangkan *relative rotative efficiency* η_{RR} dapat dipakai harga rata-2⁽³⁴⁾ :

- kapal *single screw* : $\eta_{RR} = 1,00 \sim 1,07 \approx \pm 1,02$
- kapal *twin screw* : $\eta_{RR} < 1,00 \approx \pm 0,985$

sehingga harga P.C dari kapal ybs. dapat kapal dihitung.

Formulasi pendekatan *propulsive efficiency* η_D (= QPC) bila diketahui besarnya rpm poros baling-2 = N (untuk baling-2 berdaun 4) dan panjang L_{pp} kapal sbb. (37) :

$$\eta_D = 0,885 - 0,00012 \cdot N \cdot \sqrt{L_{pp}}$$

Sebagai gambaran, kapal LPG contoh didepan : $L_{pp} = 208$ m dan $N = 120$ rpm

$$\eta_D = 0,885 - 0,00012 \cdot 120 \cdot \sqrt{208} = 0,68$$

$$P.C \approx \eta_D = 0,68 = 68\%$$

Karena harga P_E untuk kecepatan yang diminta V_s dapat dibaca dari kurva P_E vs V_s hasil *Resistance Test* (lihat Gb.8.3a-3.c), maka harga daya yang diperlukan oleh masing-2 poros baling-2 P dapat dihitung.

Dalam praktek pembuatan estimasi daya yang diperlukan mesin induk yang digunakan sebagai penggerak kapal (*propelling engine*) P_{ME} , biasanya diambil ketentuan kerugian daya karena adanya gesekan-2 poros dengan bantalan-2 sebesar 3% untuk kapal dengan kamar mesin terletak di belakang dan 5% untuk kamar mesin berada di tengah kapal. Sedangkan kerugian daya karena adanya gigi reduksi (*gear box*) adalah 0% bila mesin induk kapal tidak memakai *gear box* dan bila ada gigi reduksi dengan *gear ratio* tinggi maka kerugian daya dapat mencapai 3%.

Selain hal-2 tersebut diperlukan tambahan yakni sebagai *service allowance* atau biasa disebut *sea margin* sebesar 10% ~ 20% tergantung dari daerah pelayarannya.

Dengan demikian besarnya P_{ME} dapat diestimasi sbb. :

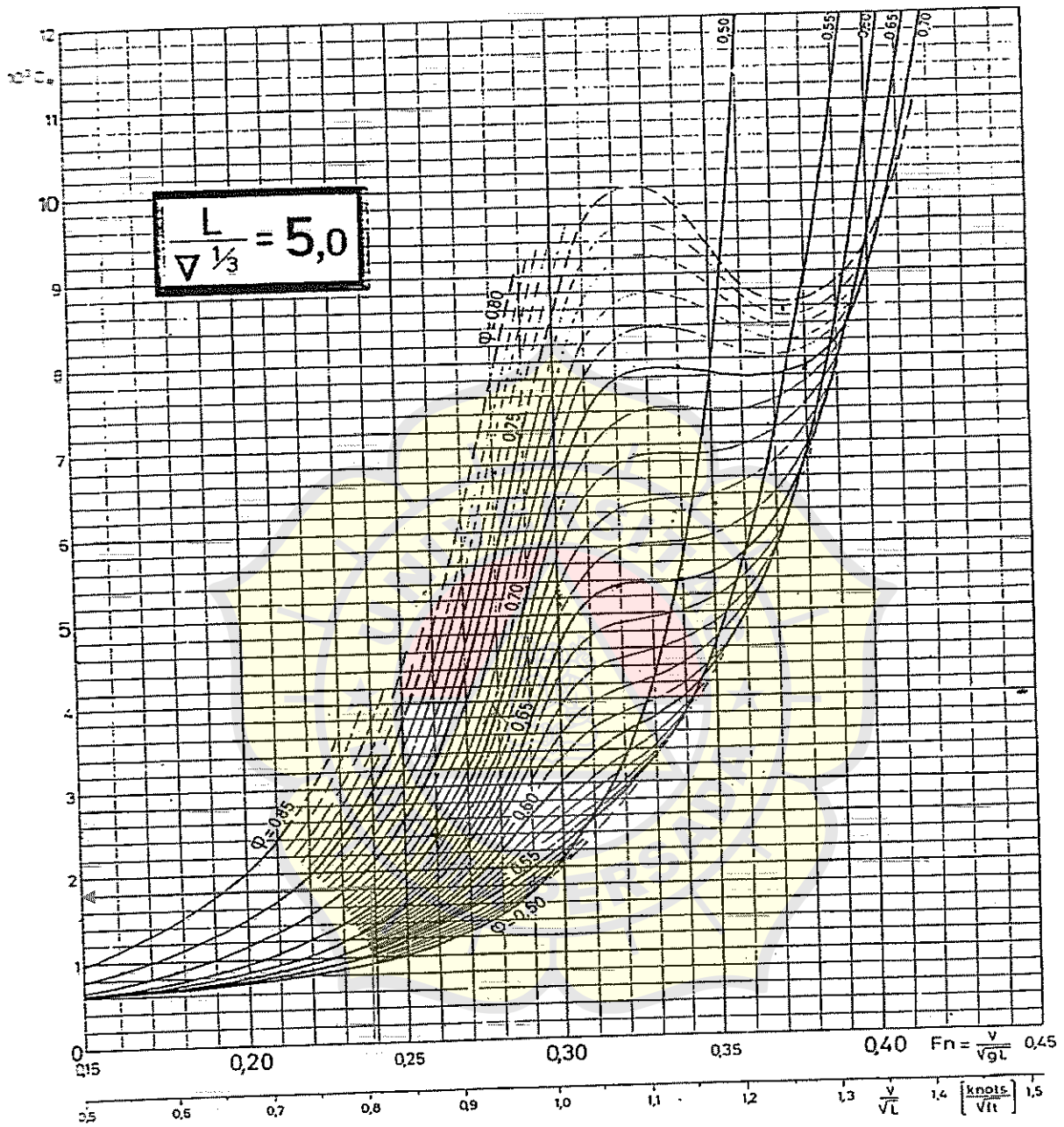
$$P_{ME} = \{ 100\% + (0\% \sim 3\%) + (3\% \sim 5\%) + (10\% \sim 20\%) \} P$$

\uparrow \uparrow \uparrow
 (gear box) (lokasi Km. Mesin) (sea margin)

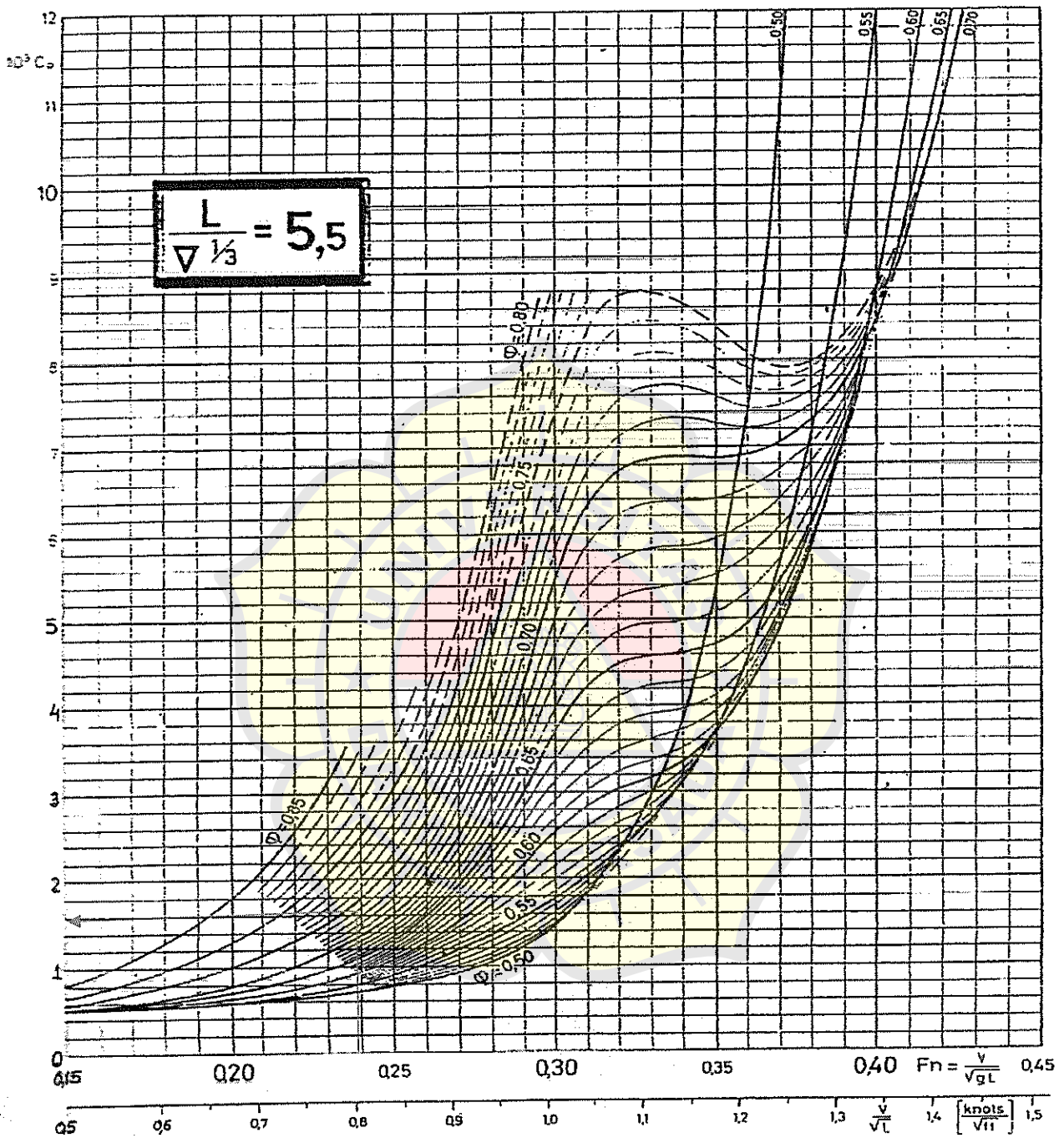
RESULT OF HYDROSTATIC CALCULATION

MULTIPLIER = $\frac{2}{3} \times \alpha = 2.533$		WATER PLANE				MIDSHIP SECTION			
Water line	Function of Water Line (F.W.L.)	Water Plane Area (W.P.A.)	Water Plane Coefficient $C_w = \frac{W.P.A.}{LWL \times B}$	TPC $= WPA \times \frac{1.025}{100}$	Midship Section Area (M.S.A.)	Midship Coeff. Cm $C_m = Am/(B \times T)$	Water line		
1.00	112.841 m	910.251 m ²	0.348	9.330 ton/Cm	9.144 m ²	0.067	1.00		
2.00	116.425 m	939.162 m ²	0.359	9.626 ton/Cm	18.744 m ²	0.137	2.00		
3.00	121.207 m	977.732 m ²	0.374	10.022 ton/Cm	28.344 m ²	0.208	3.00		
3.44	123.910 m	999.537 m ²	0.382	10.245 ton/Cm	32.568 m ²	0.239	3.44		

VERTICAL				HORIZONTAL			
Water line	KB	T.B.M.	T.K.M (KB + TBM)	LCB	LCF	L.B.M	L.K.M. (KB + LMB)
1.00	0.525 m	7.062 m	7.587 m	-0.310 m	-0.396 m	882.514 m	883.039 m
2.00	1.038 m	3.518 m	4.556 m	-0.424 m	-0.673 m	455.057 m	456.095 m
3.00	1.553 m	2.396 m	3.949 m	-0.563 m	-1.886 m	330.498 m	332.051 m
3.44	1.783 m	2.125 m	3.908 m	-0.634 m	-2.698 m	303.141 m	304.924 m



Gb.9.9.3 Diagram kurva *Residual Resistance Coefficient* C_R vs Angka Froude Fr pada rentang harga *Prismatic Coefficient* $\phi (= C_p) = 0,50 \sim 0,80$ untuk *Volumetric Coefficient* $C_\Delta (= L / \Delta^{1/3}) = 5,0$ ⁽⁸⁾



Gb.9.9.4 Diagram kurva *Residual Resistance Coefficient* C_R vs Angka Froude Fr pada rentang harga *Prismatic Coefficient* $\phi (= C_p) = 0,50 \sim 0,80$ untuk *Volumetric Coefficient* $C_V (= L / \Delta^{1/3}) = 5,5$ ⁽⁸⁾

For Harmonious Living with Global Environment



IMO Tier II Compliant

Lower fuel consumption
Lower NOx emissions

Doing Our Bit for the World!

Lower fuel consumption and emissions. At the Same Time

Normally, when NOx emissions are reduced, the fuel consumption and smoke generation will increase, adversely affecting both the environment and management. As a solution to this, YANMAR has developed "Eco Diesel" which is designed so as to comply with marine environmental protection. It improves the fuel consumption and smoke generation in addition to reducing NOx emissions.

Powerful and Friendly to People and Environment!

Techniques for Complying with IMO Tier II Emission Standards: Exhaust Gas Recirculation (EGR)

What is Exhaust Gas Recirculation (EGR)?

Nitrogen oxide (NOx) is generated during the combustion of a fuel and air mixture. However, if the temperature during combustion is lowered, the emission amount can be reduced. One such technique for reducing emissions is exhaust gas recirculation (EGR). In this technique, the combustion temperature is restricted by recirculating the exhaust gas back to the cylinders to lower the oxygen concentration. There are two EGR systems: external EGR and internal EGR. In external EGR, the line of the engine and supercharger must be equipped with devices such as EGR solenoid valves and coolers, and control must be performed for them. But in internal EGR, these functions can be performed by controlling the lift of the intake and exhaust valve.

Performance

823hp (610kW) at 1900rpm in the M operating mode / 755hp (555kW) at 1840 rpm H operating mode
This 160 mm long stroke 20 liter class diesel, with big breathing valves for better airflow, the high performance turbo fan, less turbo lag, and better mixing at low revs, the all-new high efficiency intercooler for cooler, more compact air charging, and the numerous other performance features deliver power in large amounts over a wide operating range, especially under high load conditions.

Good Fuel Economy together with Lower Emissions

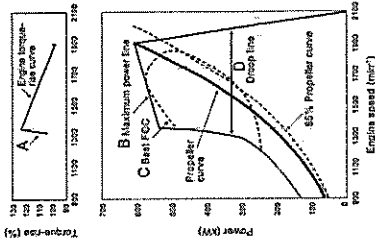
The micro-sized multiple holes in the all-new injectors produce an even finer fuel-oil mist and, combined with new perfectly matched combustion chambers and new cylinder head shapes, produce even more power. It is power delivered smoothly, due to optimum combustion conditions being maintained across a far wider operating range. And it leads directly to the bonus of lower exhaust emissions and lower fuel consumption. The boost compensator dramatically reduces black smoke under hard acceleration.

High Torque

Excellent Torque-Rise Characteristics in High Speed and High Load Range Enable Stable Performance of Job Duties even at High Load

The Engine Performance Gives Following Advantages:

1. The engine torque-rise characteristics having much in reserve, (Line A)
→ Stable cruising with least speed reduction against sudden load changes.
2. Wide Max. Power Range, (Line B)
→ A wide range propeller matching, from the passenger ship (light/medium duty) to tug boat (heavy duty), is possible.
3. Min. Fuel Consumption Range is Wide, (Line C)
→ Economical with wide min. fuel consumption range both during cruising or performing job duties.
4. Wide Medium Load Range, (Line D)
→ Produces stable engine performance even during other job duties.



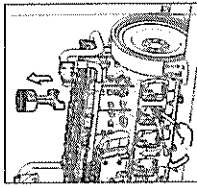
Toughness

1. Designed for marine use.
2. Type Approved by Class Societies.
3. Low, stable LOC (Lubricating Oil Consumption) and long overhaul interval.
4. Tuffride treatment cylinder liner and nitflood stainless steel rings and the finely judged clearance between piston and liner.
5. Special treatment injection nozzle.

Safety

Easier Routine Inspection, Easier Maintenance.

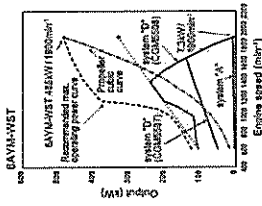
Large inspection windows on the side of the block allow in-situ replacement of pistons. Lube Oil filter is easy-to-replace cartridge type. Full mechanical engine management avoids the



chance of delicate and expensive electronics failing in hot, marine engine room conditions. Maintenance is simplified, inspection and replacement costs are lower. Reliability and durability are enhanced. Engine is user-friendly.

High capacity front PTO

It makes various applications possible, for your professional activities on the sea.



YANMAR original marine gear that can be adapted to a wide range of applications

YANMAR provides our original gearbox, which enables us to supply total marine engineering & servicing to customers!

High-Performance Marine Gear

YANMAR's original marine gear is designed to draw out best performance of YANMAR engines.

Easier Maintenance

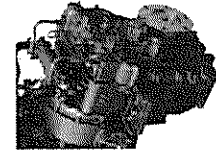
The 3-part structure of the case enables the forward shaft and reverse shaft to be disassembled and reassembled while still installed on the boat. In addition, a cartridge system is now used for the L.O. filter.

Large Capacity & Long Service Life

A fiber friction plate delivers improved trolling performance and increased clutch capacity. In addition, a finer L.O filter extends the service life of the bearings and moving parts.

Damping of Fluctuating Torque

High-performance coupling reduces the fluctuating torque that is input to the marine gear. They reduce rattling and prevent torsional vibration to protect the power transmission parts.



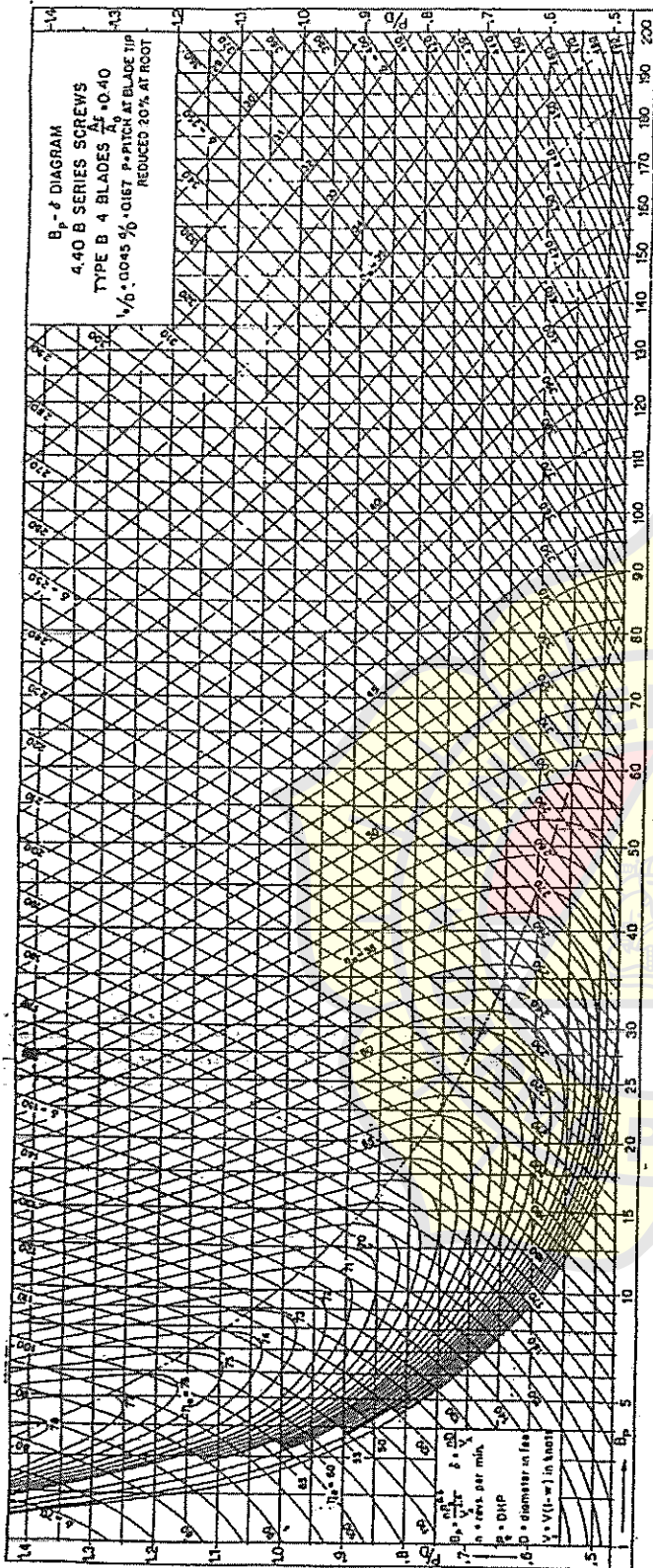


Fig. 115

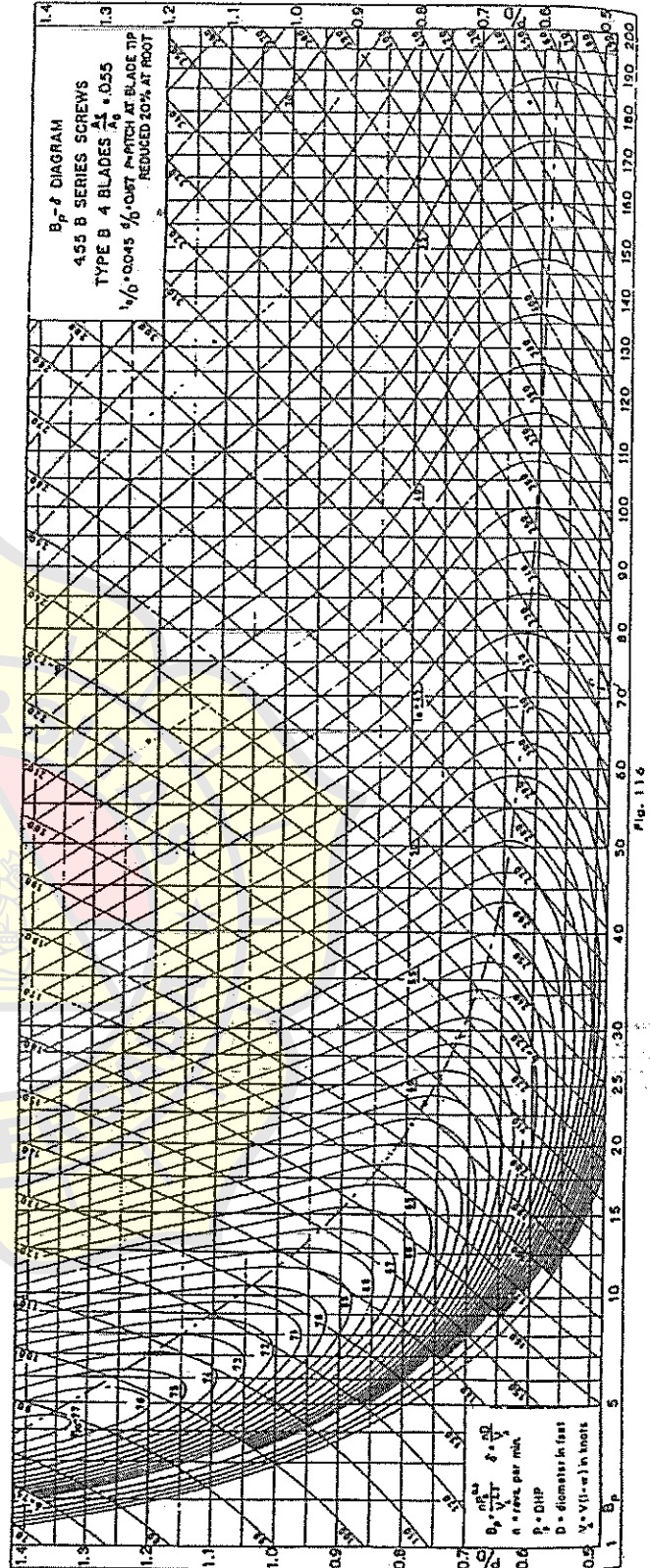


Fig. 116

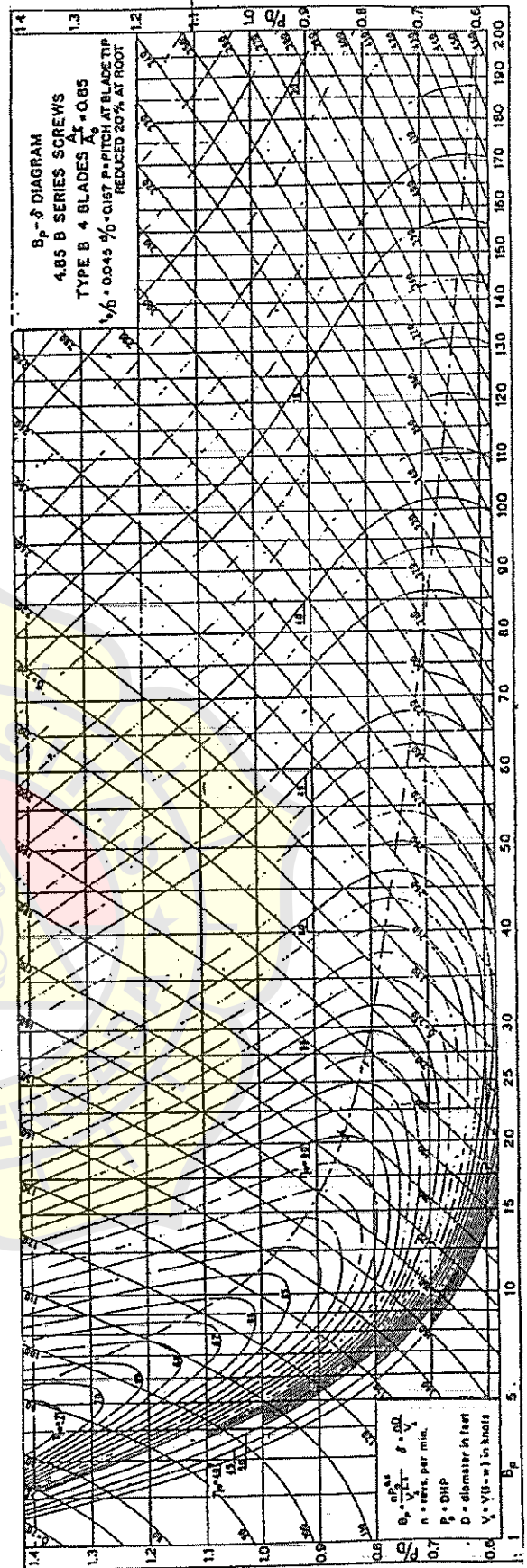
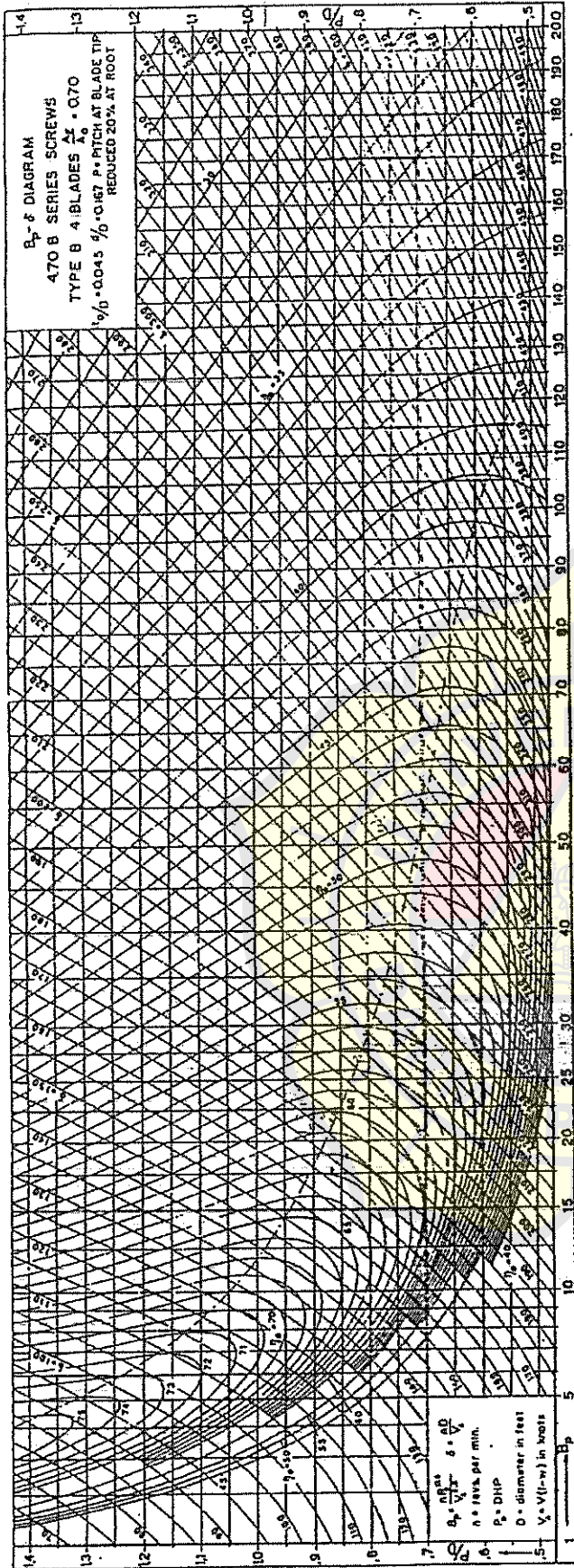


Fig. 117

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Lampiran - 1

Tabel-L1.1 Viskositas kinematis air tawar ν dalam satuan centiStokes [$\text{cST} = 10^{-6} \text{ m}^2/\text{dt}$] pada suhu dalam satuan $^{\circ}\text{C}$

$^{\circ}\text{C}$	0,0	0,1	0,2	0,3	0,4	0,5	0,6	0,7	0,8	0,9
0	1,7867	1,7806	1,7745	1,7685	1,7625	1,7565	1,7505	1,7446	1,7387	1,7329
1	1,7270	1,7212	1,7155	1,7097	1,7040	1,6984	1,6927	1,6871	1,6815	1,6759
2	1,6704	1,6649	1,6594	1,6540	1,6486	1,6432	1,6378	1,6325	1,6272	1,6219
3	1,6167	1,6114	1,6062	1,6011	1,5959	1,5908	1,5857	1,5806	1,5756	1,5706
4	1,5656	1,5606	1,5557	1,5507	1,5459	1,5410	1,5361	1,5313	1,5265	1,5217
5	1,5170	1,5123	1,5075	1,5029	1,4982	1,4936	1,4890	1,4844	1,4798	1,4752
6	1,4707	1,4662	1,4617	1,4573	1,4529	1,4484	1,4441	1,4397	1,4353	1,4310
7	1,4267	1,4224	1,4181	1,4139	1,4096	1,4054	1,4013	1,3971	1,3929	1,3888
8	1,3847	1,3806	1,3766	1,3725	1,3685	1,3645	1,3605	1,3565	1,3525	1,3486
9	1,3446	1,3407	1,3368	1,3330	1,3291	1,3253	1,3215	1,3177	1,3139	1,3102
10	1,3064	1,3027	1,2990	1,2953	1,2916	1,2879	1,2843	1,2807	1,2771	1,2735
11	1,2699	1,2663	1,2628	1,2592	1,2557	1,2522	1,2487	1,2453	1,2418	1,2384
12	1,2350	1,2315	1,2282	1,2248	1,2214	1,2181	1,2148	1,2115	1,2082	1,2049
13	1,2016	1,1983	1,1951	1,1918	1,1886	1,1854	1,1823	1,1791	1,1759	1,1728
14	1,1696	1,1665	1,1634	1,1603	1,1572	1,1541	1,1511	1,1481	1,1450	1,1420
15	1,1390	1,1360	1,1330	1,1301	1,1271	1,1242	1,1212	1,1183	1,1154	1,1125
16	1,1097	1,1068	1,1040	1,1011	1,0983	1,0955	1,0927	1,0899	1,0871	1,0843
17	1,0816	1,0788	1,0761	1,0733	1,0706	1,0679	1,0652	1,0625	1,0599	1,0572
18	1,0546	1,0519	1,0493	1,0467	1,0441	1,0415	1,0389	1,0363	1,0338	1,0312
19	1,0287	1,0261	1,0236	1,0211	1,0186	1,0161	1,0136	1,0111	1,0086	1,0062
20	1,0037	1,0013	0,9989	0,9965	0,9941	0,9917	0,9893	0,9869	0,9845	0,9822
21	0,9798	0,9775	0,9752	0,9729	0,9705	0,9682	0,9659	0,9636	0,9614	0,9591
22	0,9568	0,9546	0,9523	0,9501	0,9479	0,9457	0,9435	0,9413	0,9391	0,9369
23	0,9347	0,9326	0,9304	0,9283	0,9261	0,9240	0,9218	0,9197	0,9176	0,9155
24	0,9134	0,9113	0,9092	0,9072	0,9051	0,9031	0,9010	0,8990	0,8960	0,8949
25	0,8929	0,8909	0,8889	0,8869	0,8849	0,8829	0,8809	0,8790	0,8770	0,8751
26	0,8731	0,8712	0,8693	0,8673	0,8654	0,8635	0,8616	0,8597	0,8578	0,8560
27	0,8541	0,8522	0,8504	0,8485	0,8467	0,8448	0,8430	0,8412	0,8393	0,8375
28	0,8357	0,8339	0,8321	0,8303	0,8285	0,8268	0,8250	0,8232	0,8215	0,8197
29	0,8180	0,8163	0,8145	0,8128	0,8111	0,8094	0,8077	0,8060	0,8043	0,8026
30	0,8009	0,7992	0,7976	0,7959	0,7942	0,7926	0,7909	0,7892	0,7876	0,7859

Contoh :

Air di tangki percobaan Laboratorium Hidrodinamika ITS pada saat *resistance test* tgl.1 Juni 1994 dilaksanakan : suhu $27,0^{\circ}\text{C}$, sehingga :

$$\nu_{\text{air tawar}} = 0,8541 \text{ cST } (= 0,8451 \cdot 10^{-6} \text{ m}^2/\text{dt}.)$$

Tabel-L1.2 Viskositas kinematis air laut (air dengan kadar garam 3,5%) [cST][10^{-6} m²/dt.] pada suhu dalam satuan °C

°C	0,0	0,1	0,2	0,3	0,4	0,5	0,6	0,7	0,8	0,9
0	1,3284	1,8224	1,8163	1,8103	1,8044	1,7984	1,7925	1,7866	1,7808	1,7749
1	1,7692	1,7634	1,7577	1,7520	1,7463	1,7407	1,7351	1,7296	1,7240	1,7185
2	1,7131	1,7076	1,7022	1,6968	1,6915	1,6861	1,6808	1,6755	1,6703	1,6651
3	1,6599	1,6547	1,6496	1,6445	1,6394	1,6343	1,6293	1,6243	1,6193	1,6143
4	1,6094	1,6045	1,5996	1,5948	1,5899	1,5851	1,5803	1,5756	1,5708	1,5661
5	1,5614	1,5568	1,5521	1,5475	1,5429	1,5384	1,5338	1,5293	1,5248	1,5203
6	1,5158	1,5114	1,5070	1,5026	1,4982	1,4939	1,4896	1,4853	1,4810	1,4767
7	1,4724	1,4681	1,4640	1,4598	1,4556	1,4515	1,4474	1,4433	1,4392	1,4351
8	1,4310	1,4270	1,4230	1,4190	1,4150	1,4110	1,4071	1,4032	1,3993	1,3954
9	1,3915	1,3877	1,3839	1,3800	1,3762	1,3725	1,3687	1,33650	1,3612	1,3575
10	1,3538	1,3501	1,3465	1,3428	1,3392	1,3356	1,3320	1,3284	1,3248	1,3213
11	1,3177	1,3142	1,3107	1,3072	1,3038	1,3003	1,2969	1,2934	1,2900	1,2866
12	1,2832	1,2799	1,2765	1,2732	1,2699	1,2666	1,2633	1,2600	1,2568	1,2535
13	1,2503	1,2471	1,2438	1,2406	1,2375	1,2343	1,2311	1,2280	1,2248	1,2217
14	1,2186	1,2155	1,2124	1,2094	1,2063	1,2033	1,2003	1,1973	1,1943	1,1913
15	1,1883	1,1853	1,1824	1,1794	1,1765	1,1736	1,1707	1,1678	1,1649	1,1620
16	1,1592	1,1563	1,1535	1,1507	1,1479	1,1451	1,1423	1,1395	1,1367	1,1340
17	1,1313	1,1285	1,1258	1,1231	1,1204	1,1177	1,1150	1,1123	1,1097	1,1070
18	1,1044	1,1018	1,0991	1,0965	1,0939	1,0914	1,0888	1,0862	1,0836	1,0811
19	1,0785	1,0760	1,0735	1,0710	1,0685	1,0660	1,0635	1,0611	1,0586	1,0562
20	1,0537	1,0513	1,0489	1,0465	1,0441	1,0417	1,0393	1,0369	1,0345	1,0322
21	1,0298	1,0275	1,0251	1,0228	1,0205	1,0182	1,0159	1,0136	1,0113	1,0090
22	1,0068	1,0045	1,0023	1,00003	0,9978	0,9956	0,9934	0,9912	0,9890	0,9868
23	0,9846	0,9824	0,9802	0,9781	0,9759	0,9738	0,9716	0,9695	0,9674	0,9653
24	0,9632	0,9611	0,9590	0,9569	0,9550	0,9527	0,9507	0,9486	0,9466	0,9446
25	0,9425	0,9405	0,9385	0,9365	0,9345	0,9325	0,9305	0,9285	0,9265	0,9245
26	0,9226	0,9206	0,9187	0,9167	0,9148	0,9129	0,9109	0,9090	0,9071	0,9052
27	0,9333	0,9014	0,8995	0,8977	0,8958	0,8939	0,8921	0,8902	0,8884	0,8865
28	0,8847	0,8829	0,8811	0,8792	0,8774	0,8756	0,8738	0,8721	0,8703	0,8685
29	0,8667	0,8649	0,8632	0,8614	0,8597	0,8579	0,8562	0,8545	0,8527	0,8510
30	0,84931	0,8476	0,8459	0,8442	0,8425	0,8408	0,8391	0,8374	0,8357	0,8340

Contoh :

Tangki percobaan Laboratorium Hidrodinamika ITS saat melaksanakan *model test / resistance test* untuk kapal *tanker* 1500DWT dalam bulan Juni 1994 mengambil asumsi suhu air laut dimana kapal akan dioperasikan = 28,0° C, sehingga :

$$v'_{\text{air laut}} = 0,8847 \text{ cST } (= 0,8847 \cdot 10^{-6} \text{ m}^2/\text{dt.})$$

Tabel-L1.3 Massa jenis udara (kering)

Suhu [°C]	γ_{udara} [kg/m ³]
0	1,293
5	1,270
10	1,247
15	1,226
20	1,184
25	1,184
30	1,165

Lampiran - 2

Tabel konversi satuan menjadi S I

Kuantitas	Satuan Inggris / Amerika atau MKS	Satuan S I
Panjang	1 fathom.....	1,8288 m
	1 ft.	0,3048 m
	1 in.	25,400 mm
Luas	1 ft ²	9,2903.10 ⁻² m ²
	1 in ²	6,4516.10 ² mm ²
Volume	1 ft ³	2,8317. 10 ⁻² m ³
	1 in ³	1,6387. 10 ⁴ mm ³
	1 gallon (liquid).....	3,7854. 10 ⁻³ m ³
Massa	1 lb	0,4536 kg
	1 ton (long)	1,0160. 10 ³ kg
	1 ton (metric)	1,0000. 10 ³ kg
Gaya	1 lb	4,4482 N
	1 kg	9,8067 N
	1 ton (long)	9,9640 kN
	1 ton (metric)	9,8067 kN
Energi, Usaha	1 Btu	1,0551. 10 ⁻³ J
	1 ft.lb	1,3558 J
	1 in.lb.	1,1298.10 ⁻¹ J
	1 kcal.....	4,1868.10 ³ J
	1 kg.m	9,8067 J
Daya	1 HP (British)	7,4570.10 ² W
	= 76 kg.m/dt 1 HP (metric)..... = 75 kg.m/dt	7,3560.10 ² W
Tekanan, Tegangan	1 psi	6,8948.10 ⁻³ N/m ² (=Pa)
	1 kg/cm ²	6,8948. 10 ³ bar
	1 kg/ mm ²	9,8067.10 ⁴ N/m ² (=Pa)
Kecepatan	1 knot	0,5144 m/dt
Torsi	1 lb.in	0,11298 N.m
	1 kg.m	9,80665 N.m
Sudut (datar)	1 derajat (=degree).....	$\pi / 180$ radian

REFERENSI BAB III



Section 9

Framing System

A. Transverse Framing

1. General

1.1 Frame spacing

Forward of the collision bulkhead and aft of the after peak bulkhead, the frame spacing shall in general not exceed 600 mm.

1.2 Definitions

k = material factor according to Section 2, B.2.

$\bullet\bullet$ = unsupported span [m] according to Section 3, C., see also Fig. 9.1

$\bullet\bullet_{\min}$ = 2,0 m

$\bullet\ell_{\text{Ku}}, \bullet\ell_{\text{Ko}}$ = length of lower/upper bracket connection of main frames within the length $\bullet\bullet$ [m], see Fig. 9.1

$$m_a = 0,204 \frac{a}{\ell} \left[4 - \left(\frac{a}{\ell} \right)^2 \right], \text{ where } \frac{a}{\ell} \leq 1$$

e = spacing of web frames [m]

p = p_s or p_c as the case may be

p_s = load on ship's sides [kN/m²] according to Section 4, B.2.1

p_c = load on bow structures [kN/m²] according to Section 4, B.2.2 or stern structures according to Section 4, B.2.3 as the case may be

p_L = 'tween deck load [kN/m²] according to Section 4, C.1.

p_1, p_2 = pressure [kN/m²] according to Section 4, D.1.

H_u = depth up to the lowest deck [m]

c_r = factor for curved frames,

$$= 1,0 - 2 \frac{s}{\ell}$$

c_{\min} = 0,75

s = max. height of curve.

2. Main frames

2.1 Scantlings

2.1.1 The section modulus W_R and shear area A_R of the main frames including end attachments are not to be less than:

$$W_R = n \cdot c \cdot a \cdot \ell^2 \cdot p \cdot c_r \cdot k \quad [\text{cm}^3]$$

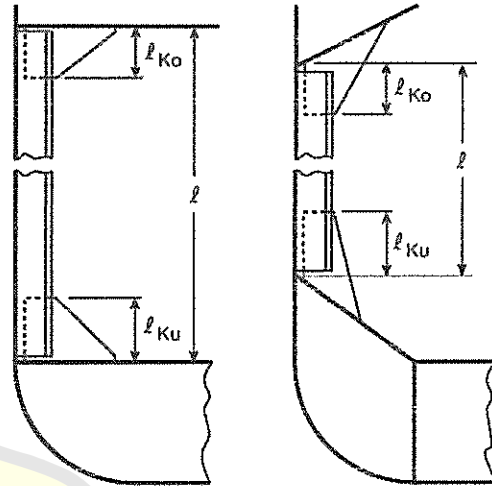


Fig. 9.1 Unsupported span of transverse frames

upper end shear area :

$$A_{RO} = (1 - 0,817 \cdot m_a) 0,04 \cdot a \cdot \ell \cdot p \cdot k \quad [\text{cm}^2]$$

lower end shear area :

$$A_{RU} = (1 - 0,817 \cdot m_a) 0,07 \cdot a \cdot \ell \cdot p \cdot k \quad [\text{cm}^2]$$

$$n = 0,9 \cdot \bullet\bullet \cdot 0,0035 \quad \text{for } L < 100 \text{ m}$$

$$= 0,55 \quad \text{for } L \geq 100 \text{ m}$$

$$c = 1,0 - \left(\frac{\ell_{Ku}}{\ell} + 0,4 \cdot \frac{\ell_{Ko}}{\ell} \right)$$

$$c_{\min} = 0,6$$

Within the lower bracket connection the section modulus is not to be less than the value obtained for $c = 1,0$.

2.1.2 In ships with more than 3 decks the main frames are to extend at least to the deck above the lowest deck.

2.1.3 The scantlings of the main frames are not to be less than those of the 'tween deck frames above.

2.1.4 Where the scantlings of the main frames are determined by strength calculations, the following permissible stresses are to be observed:

$$\text{bending stress: } \sigma_b = \frac{150}{k} \quad [\text{N/mm}^2]$$

$$\text{shear stress: } \tau = \frac{100}{k} \quad [\text{N/mm}^2]$$

Section 11

Watertight Bulkheads

A. General

1. Watertight subdivision

1.1 All ships are to have a collision bulkhead, a stern tube bulkhead and one watertight bulkhead at each end of the engine room. In ships with machinery aft, the stern tube bulkhead may substitute the aft engine room bulkhead.

1.2 For ships without longitudinal bulkheads in the cargo hold area the number of watertight transverse bulkheads should, in general, not be less than given in Table 11.1.

Table 11.1 Number of watertight transverse bulkheads

L [m]	Arrangement of machinery space	
	aft	elsewhere
$L \leq 65$	3	4
$65 < L \leq 85$	4	4
$85 < L \leq 105$	4	5
$105 < L \leq 125$	5	6
$125 < L \leq 145$	6	7
$145 < L \leq 165$	7	8
$165 < L \leq 185$	8	9
$L > 185$	to be special considered	

1.3 One or more of the watertight bulkheads required by 1.2, may be dispensed with where the transverse strength of the ship is adequate. The number of watertight bulkheads will be entered into the Register.

1.4 Number and location of transverse bulkheads fitted in addition to those specified in 1.1 are to be so selected as to ensure sufficient transverse strength of the hull.

1.5 For ships which require proof of survival capability in damaged conditions, the watertight sub-division will be determined by damage stability calculations. For oil tankers see Section 24, A.2., for passenger vessels see Section 29-I, C., for special purpose ships see Section 29-II, C., for cargo ships of more than 100 m in length see Section 36 and for supply vessels see Section 34, A.2. For liquefied gas tankers see Rules for Ships Carrying Liquefied Gases in Bulk, Volume IX, Section 2, for chemical tankers see Rules for Ships Carrying Dangerous Chemicals in Bulk, Volume X, Section 2.

2. Arrangement of watertight bulkheads-

2.1 Collision bulkhead

2.1.1 A collision bulkhead shall be located at a distance

from the forward perpendicular of not less than $0,05 L_c$ or 10 m, whichever is the less, and, except as may be permitted by the Administration, not more than $0,08 L_c$ or $0,05 L_c + 3$ m, whichever is the greater

2.1.2 Where any part of the ship below the waterline extends forward of the forward perpendicular, e.g., a bulbous bow, the distance x shall be measured from a point either:

- at the mid-length of such extension, i.e. $x = 0,5 \cdot a$
- at a distance $0,015 L_c$ forward of the forward perpendicular, i.e. $x = 0,015 \cdot L_c$, or
- at a distance 3 m forward of the forward perpendicular, i.e. $x = 3,0$ m

whichever gives the smallest measurement.

The length L_c and the distance a are to be specified in the approval documents.

2.1.3 If 2.1.2 is applicable, the required distances specified in 2.1.1 are to be measured from a reference point located at a distance x forward of the F.P.

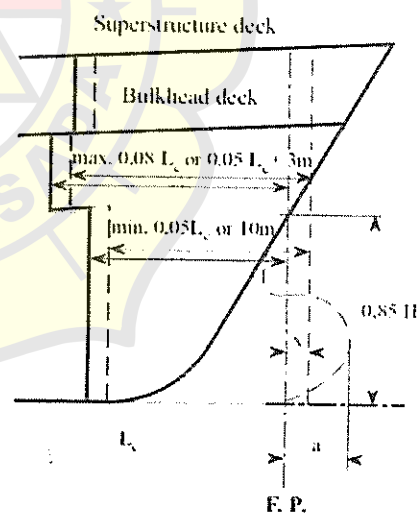


Fig.11.1 Location of collision bulkhead

2.1.4 The collision bulkhead shall extend watertight up to the bulkhead deck. The bulkhead may have steps or recesses provided they are within the limits prescribed in 2.1.1.

2.1.5 No doors, manholes, access openings, or ventilation ducts are permitted in the collision bulkhead below the bulkhead deck.

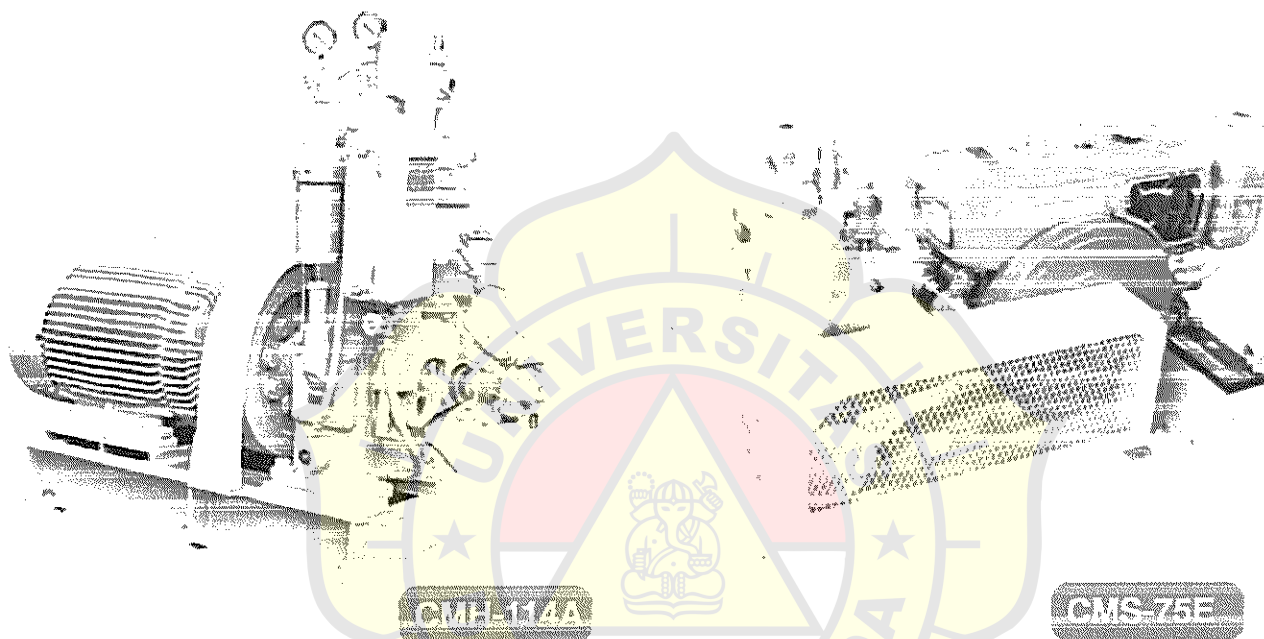
REFERENSI BAB IV DAN BAB V



CMS-54(E) / CMS-75A(E)
CMS-85 / CMS-92A
CMH-111 / CMH-114A

PRESSURE : 30 kg/cm² (2.94 MPa)
 CAPACITY : 3.7~65 m³/h
 MOTOR : 2.2~19 kW
 TYPE : 1 cylinder, vertical

- Long service life.
- Suitable for small & medium vessel (15,000 DWT below).
- Compact size and small installation area.
- Easy combine with diesel engine (emergency starting).



SPECIFICATION

MODEL	CYLINDER	SPEED (RPM)	CAPACITY F.A (m ³ /h)	PRESSURE kg/cm ² (MPa)	MOTOR or ENGINE		AIR OUTLET
					Hz	kW	
CMS-54	1 CYLINDER	1000	3.7	30 (2.94)	50	2.2	30K-15A
		1200	4.5	30 (2.94)	60		
		1500	5	30 (2.94)	-		
CMS-75A	1 CYLINDER	1000	12	30 (2.94)	50	5.5	
		1200	15	30 (2.94)	60		
		1200	15	30 (2.94)	-		
CMS-85	1 CYLINDER	1000	21	30 (2.94)	50	7.5	
		1200	26	30 (2.94)	60		
		1000	27	30 (2.94)	50		11
1200	32.5	30 (2.94)	60				
CMS-92A	1 CYLINDER	1000	44	30 (2.94)	50	15	30K-25A
		1200	53	30 (2.94)	60		
		1000	54	30 (2.94)	50		
1200	65	30 (2.94)	60				

* Mark means diesel engine driven type.
 * F.A (free air), tolerance ± 5%.

Some specifications in this catalogue may change without notice.

2.1 Spesifikasi Pompa

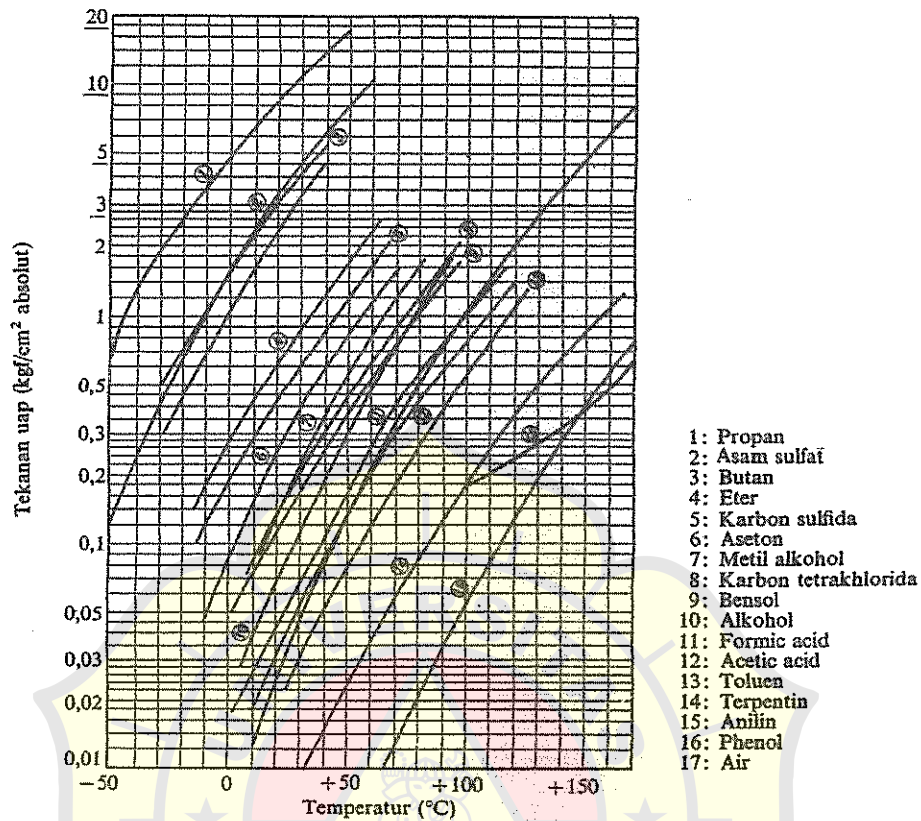
Dalam memilih suatu pompa untuk suatu maksud tertentu, terlebih dahulu harus diketahui kapasitas aliran serta head yang diperlukan untuk mengalirkan zat cair yang akan dipompa.

Selain dari pada itu, agar pompa dapat bekerja tanpa mengalami kavitasi, perlu ditaksir berapa tekanan minimum yang tersedia pada sisi masuk pompa yang terpasang pada instalasinya. Atas dasar tekanan isap ini maka putaran pompa dapat ditentukan.

Kapasitas aliran, head, dan putaran pompa dapat ditentukan seperti tersebut di atas. Tetapi apabila perubahan kondisi operasi sangat besar (khususnya perubahan kapasitas

Tabel 2.1 Data yang diperlukan untuk pemilihan pompa.

No.	Data yang diperlukan	Keterangan
1	Kapasitas	Diperlukan juga keterangan mengenai kapasitas maksimum dan minimum.
2	Kondisi isap	Tinggi isap dari permukaan air isap ke level pompa. Tinggi fluktuasi permukaan air isap. Tekanan yang bekerja pada permukaan air isap. Kondisi pipa isap.
3	Kondisi keluar	Tinggi permukaan air keluar ke level pompa. Tinggi fluktuasi permukaan air keluar. Besarnya tekanan pada permukaan air keluar. Kondisi pipa keluar.
4	Head total pompa	Harus ditentukan berdasarkan kondisi-kondisi di atas.
5	Jenis zat cair	Air tawar, air laut, minyak, zat cair khusus (zat kimia), temperatur, berat jenis, viskositas, kandungan zat padat, dll.
6	Jumlah pompa	
7	Kondisi kerja	Kerja terus-menerus, terputus-putus, jumlah jam kerja seluruhnya dalam setahun.
8	Penggerak	Motor listrik, motor bakar torak, turbin uap.
9	Poros tegak atau mendatar	Hal ini kadang-kadang ditentukan oleh pabrik pompa yang bersangkutan berdasarkan instalasinya.
10	Tempat instalasi	Pembatasan-pembatasan pada ruang instalasi, ketinggian di atas permukaan laut, di luar atau di dalam gedung, fluktuasi temperatur.
11	Lain-lain	



(b) Tekanan uap berbagai zat cair
(Catatan: $1 \text{ kg/cm}^2 = 0,1 \text{ MPa}$)

Gb. 2.1 Sifat-sifat fisik berbagai zat cair.

2.4 Head

2.4.1 Head Total Pompa

Head total pompa yang harus disediakan untuk mengalirkan jumlah air seperti direncanakan, dapat ditentukan dari kondisi instalasi yang akan dilayani oleh pompa. Seperti diperlihatkan dalam Gb. 2.2, head total pompa dapat ditulis sebagai berikut:

$$H = h_a + \Delta h_p + h_l + \frac{v_d^2}{2g} \quad (2.6)$$

di mana H : Head total pompa (m)

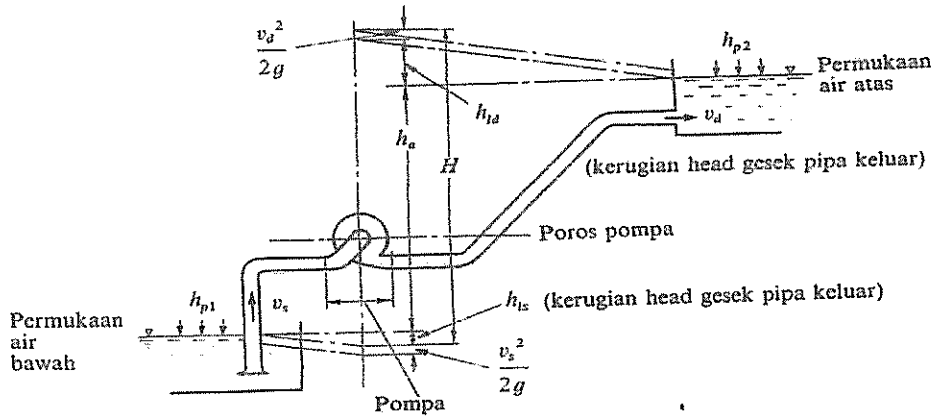
h_a : Head statis total (m)

Head ini adalah perbedaan tinggi antara muka air di sisi keluar dan di sisi isap; tanda positif (+) dipakai apabila muka air di sisi ke luar lebih tinggi dari pada sisi isap.

Δh_p : Perbedaan head tekanan yang bekerja pada kedua permukaan air (m),

$$\Delta h_p = h_{p2} - h_{p1},$$

h_l : Berbagai kerugian head di pipa, katup, belokan, sambungan, dll (m),



Gb. 2.2 Head pompa (1).

$$h_l = h_{id} + h_{is}$$

$v^2/2g$: Head kecepatan keluar (m)

g : Percepatan gravitasi (= 9,8 m/s²)

Dalam hal pompa menerima energi dari aliran yang masuk ke sisi isapnya, seperti pada pompa penguat (pompa booster), maka head total pompa dapat dihitung dengan rumus berikut:

$$H = h_a + \Delta h_p + h_l + \frac{1}{2g}(v_d^2 - v_s^2) \tag{2.7}$$

di mana h_a : Perbedaan tinggi antara titik sebarang ① di pipa keluar, dan sebarang titik ② di pipa isap (m) (Lihat Gb. 2.3).

Δh_p : Perbedaan tekanan statis antara titik ① dan titik ② (m)

h_l : Berbagai kerugian head di pipa, katup, belokan dll, antara titik ① dan titik ② (m)

v_d : Kecepatan aliran rata-rata di titik ① (m/s)

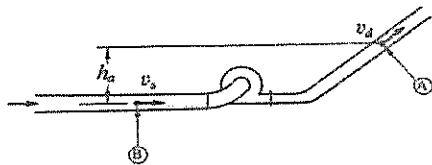
v_s : Kecepatan aliran rata-rata di titik ② (m/s)

Untuk pompa tegak yang tidak mempunyai pipa isap, $h_l = h_{id}$.

Apabila permukaan air berubah-ubah dengan perbedaan besar, head statis total harus ditentukan dengan mempertimbangkan karakteristik pompa, besarnya selisih perubahan permukaan air, dan dasar yang dipakai untuk menentukan jumlah air yang harus dipompa.

Adapun hubungan antara tekanan dan head tekanan dapat diperoleh dari rumus berikut:

$$h_p = 10 \times \frac{P}{\gamma} \tag{2.8}$$



Gb. 2.3 Head pompa (2).

di mana h_p : Head tekanan (m)

ρ : Tekanan (kgf/cm²)

γ : Berat per satuan volume zat cair yang dipompa (kgf/l)

Apabila tekanan diberikan dalam kPa, dapat dipakai rumus berikut:

$$h_p = \frac{1}{9,8} \frac{p'}{\rho} \quad (2.9)$$

di mana p' : Tekanan (Pa)

ρ : Rapat masa (kg/l)

Menurut ISO, energi spesifik Y (J/kg) kadang-kadang dipakai sebagai pengganti head H (m). Adapun hubungannya adalah sebagai berikut:

$$Y = gH \quad (2.10)$$

Sebagaimana diutarakan di atas, untuk menentukan head total yang harus disediakan pompa, perlu dihitung lebih dahulu head kerugian h_f . Di bawah ini akan diuraikan cara menghitung kerugian head tersebut.

2.4.2 Head Kerugian

Head kerugian (yaitu head untuk mengatasi kerugian-kerugian) terdiri atas head kerugian gesek di dalam pipa-pipa, dan head kerugian di dalam belokan-belokan, reduser, katup-katup, dsb. Di bawah ini akan diberikan cara menghitungnya, satu per satu.

(1) Head kerugian gesek dalam pipa

Untuk menghitung kerugian gesek di dalam pipa dapat dipakai salah satu dari dua rumus berikut ini:

$$v = CR^p S^q \quad (2.11)$$

$$h_f = \lambda \frac{L}{D} \frac{v^2}{2g} \quad (2.12)$$

di mana v : Kecepatan rata-rata aliran di dalam pipa (m/s)

C, p, q : Koefisien-koefisien

R : Jari-jari hidrolis (m)

$$R = \frac{\text{Luas penampang pipa, tegak lurus aliran (m}^2\text{)}}{\text{Ketiling pipa atau saluran yang dibasahi (m)}}$$

S : Gradien hidrolis

$$S = \frac{h_f}{L}$$

h_f : Head kerugian gesek dalam pipa (m)

λ : Koefisien kerugian gesek

g : Percepatan gravitasi (9,8 m/s²)

L : Panjang pipa (m)

D : Diameter dalam pipa (m)

Selanjutnya, untuk aliran yang laminer dan yang turbulen, terdapat rumus yang berbeda. Sebagai patokan apakah suatu aliran itu laminer atau turbulen, dipakai bilangan Reynolds:

$$Re = \frac{vD}{\nu} \quad (2.13)$$

特長

Feature

NHGシリーズは、
一般電動横形低圧・
内装軸受式歯車ポンプです。

NHG series is motor driven
horizontal low pressure internal
bearing type gear pumps.

■温度：世界にさきがけて考案された、
一点連続接触歯車“欠円ギヤ”が
標準です。



■Tooth Profile：To be the first in the world to design a
one-point-contact-gear called
"Segmental Gear" as our standard
model.

仕様

Specification

■歯形：取扱い油温は、最高80℃です。

■Temperature：Maximum handling oil temperature is 80℃.

■軸受：内装軸受式で揚液による自己潤滑方式のため、潤滑性を有する液に適します。

■Bearing：Internal bearing is self-lubricated by pumping liquid which is suitable to serve lubricant fluids.

■軸封：グランドパッキン式が標準です。
ご要望に応じて、メカニカルシール式
又はオイルシール式を製作します。

■Shaft Seal：The conventional gland packing is our standard; however, the mechanical seal type is also available.

■フランジ：吸込み、吐出し共JIS10Kです。

■Flange：Both suction and discharge are JIS10K.

■軸心：ポンプと電動機との軸継手の芯の振れの許容範囲は、回転速度2000～500min⁻¹において、軸継手側面で0.1mm以下、軸継手端面で0.1mm以下です。

■Centering：If connecting the pump with the motor, the standard allowable alignment value at the rate of 2000 to 500min⁻¹ at the shaft coupling side surface should be under 0.1mm and at the shaft coupling end surface should be under 0.1mm.

■水圧試験：計画仕様圧力の2倍が標準です。
最高1.20MPaです。

■Hydraulic Test：Twice the value of the designed specification pressure with a maximum value of 1.20MPa.

■吐出し量：吐出し量は、吐出圧力0.60MPa、
粘度25.8mm²/sにおける量です。
許容吸込圧力範囲は、ポンプ入口に
おいて、-0.05～0.20MPaです。

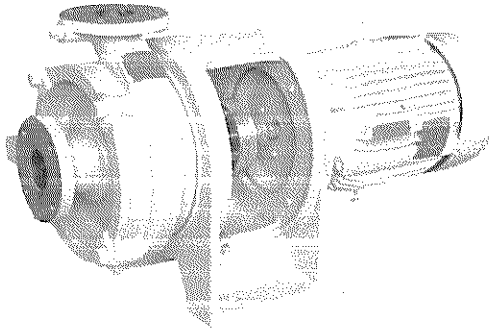
■Capacity：The following capacity shows at viscosity of 25.8mm²/s with discharge pressure of 0.60MPa. The allowable suction pressure range is -0.05 to 0.20MPa at the pump suction.

形番 Model No.	口径 Bore (mm) 吸込み×吐出し Suc.× Dis.	吐出し量 Capacity (m ³ /h)			
		60Hz		50Hz	
		1200min ⁻¹	1800min ⁻¹	1000min ⁻¹	1500min ⁻¹
NHG-0.3	32×25	0.3	0.45	0.25	0.37
NHG-0.5		0.5	0.75	0.41	0.62
NHG-1		1	1.5	0.8	1.2
NHG-1.5	40×32	1.5	2.2	1.2	1.8
NHG-2		2	3	1.6	2.5
NHG-2.5		2.5	3.7	2	3
NHG-3	50×40	3	4.5	2.5	3.7
NHG-4		4	6	3.3	5
NHG-5		5	7.5	4	6
NHG-6	65×50	6	9	5	7.5
NHG-7.5		7.5	11	6	9
NHG-10		10	15	8	12
NHG-12	80×65	12	18	10	15
NHG-15		15	22	12	18
NHG-20		20	30	16	25
NHG-25	100×80	25	—	20	30
NHG-30		30	—	25	—



CENTRIFUGAL PUMP

TMC



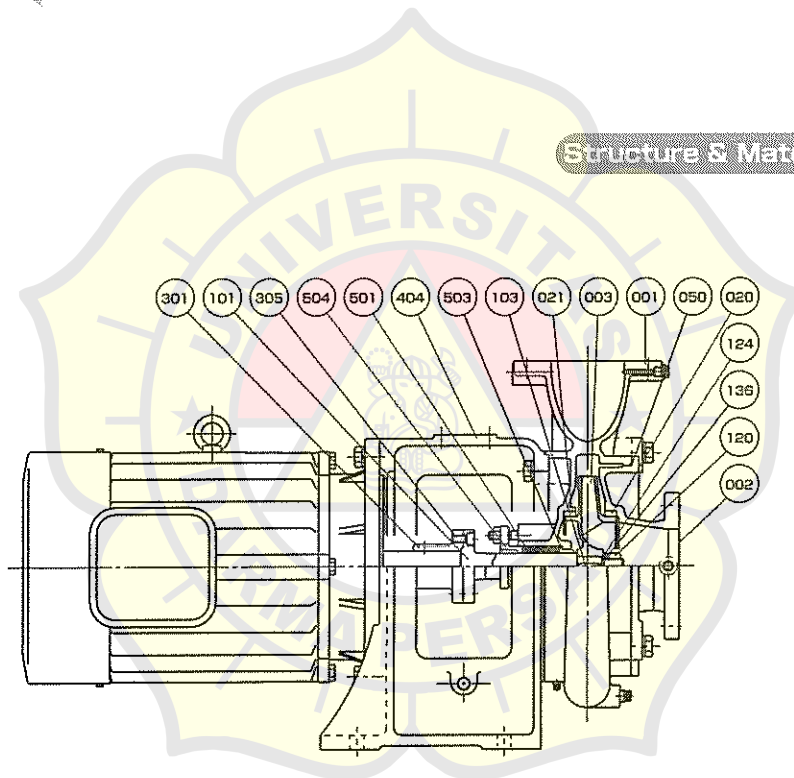
Application

Cooling Fresh Water
Cooling Sea Water
Sea Water Service

Feature

Horizontal Single-stage Single-suction
Closed Coupling Type

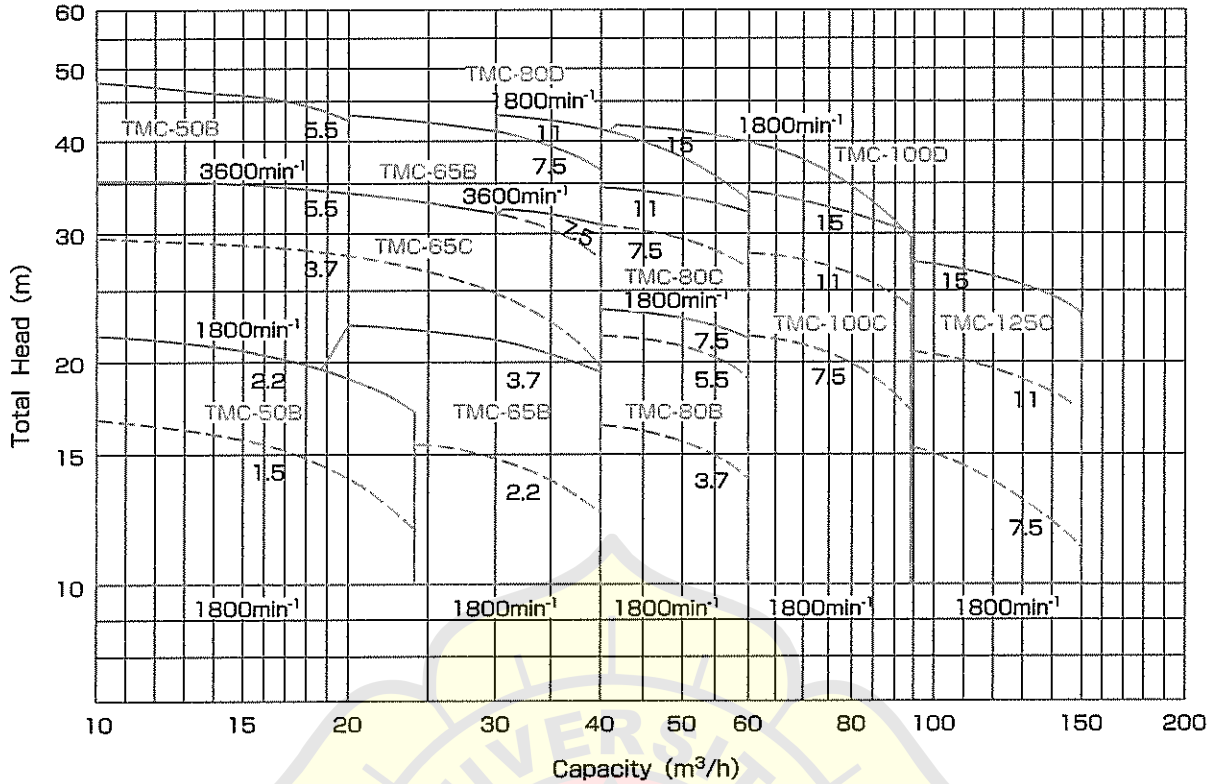
Structure & Material



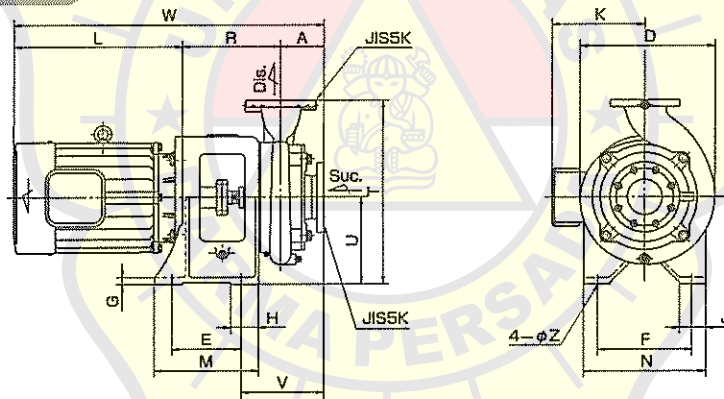
Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
001	CASING	1	BRONZE	CAC402	CAST IRON	FC200
002	CASING COVER	1	BRONZE	CAC402	CAST IRON	FC200
003	IMPELLER	1	PHOSPHOR BRONZE	CAC502A	PHOSPHOR BRONZE	CAC502A
020	CASING RING	1	BRONZE	CAC402	BRONZE	CAC402
021	CASING RING	1	BRONZE	CAC402	BRONZE	CAC402
050	O-RING	1	RUBBER	NBR	RUBBER	NBR
101	SHAFT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
103	IMPELLER KEY	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
120	IMPELLER NUT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304

Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
124	IMPELLER WASHER	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
136	SPRING WASHER	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
301	COUPLING	1	MILD STEEL	SS400	MILD STEEL	SS400
305	COUPLING BOLT	4	Cr-Mo STEEL	SCM435	Cr-Mo STEEL	SCM435
404	FRAME	1	CAST IRON	FC200	CAST IRON	FC200
501	GLAND PACKING	4	CARBONIZED FIBER	-	CARBONIZED FIBER	-
503	LANTERN RING	1	BRONZE	CAC402	BRONZE	CAC402
504	GLAND	1	BRONZE	CAC402	BRONZE	CAC402

Performance



Dimensi

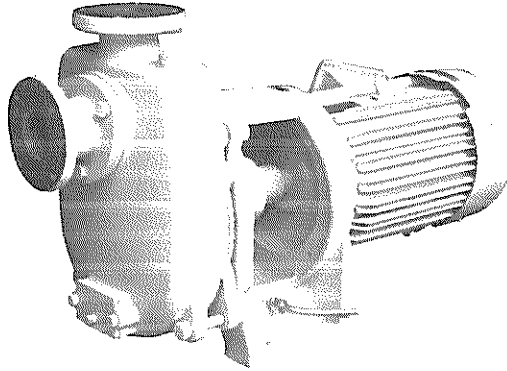


Model No.	Motor		Bore		Dimension (mm)																	
	kW	min ⁻¹	Suc.	Dis.	A	D	E	F	G	H	J	K	L	M	N	R	T	U	V	W	Z	
TMC-50B	1.5	1800	50	50	100	255	150	220	15	80	65	195	300	250	280	215	370	190	205	615	15	
	2.2	1800					180	270					205	330	280	225	245	330		210		655
	5.5	3600					200	270					265	400	300	330	245	390		210		745
TMC-65B	2.2	1800	65	65	100	285	180	220	18	80	65	205	330	280	280	227	390	190	207	657	15	
	3.7	1800					200	270					215	355	300	330	247	410		210		682
	7.5	3600					180	220					265	400	300	330	247	415		190		747
TMC-65C	3.7	1800	65	65	100	335	180	220	18	80	65	215	355	280	280	227	415	190	207	682	15	
	5.5	1800					200	270					265	400	300	330	247	435		210		747
	7.5	1800					180	220					215	355	280	280	227	415		190		682
TMC-80B	3.7	1800	80	80	100	325	180	220	18	80	65	215	355	280	280	232	415	190	212	687	15	
	5.5	1800					200	270					265	400	300	330	252	435		210		752
	7.5	1800					180	220					215	355	280	280	232	415		190		687
TMC-80C	7.5	1800	80	80	100	365	200	270	18	80	75	265	400	300	350	252	500	250	212	752	19	
	11	1800					20	270					265	485	300	350	282	500		250		857
TMC-80D	11	1800	80	80	125	405	200	270	20	80	75	285	485	300	350	290	530	250	245	900	19	
	7.5	1800					18	270					265	400	300	350	253	530		250		778
TMC-100C	11	1800	100	100	125	385	200	270	20	80	75	285	485	300	350	283	530	250	238	883	19	
	15	1800					18	270					265	400	300	350	283	530		250		933
	7.5	1800					20	270					265	485	300	350	285	530		250		805
TMC-100D	15	1800	100	100	125	405	200	270	20	80	75	285	525	300	350	290	565	250	245	940	19	
	7.5	1800					18	270					265	400	300	350	265	530		250		805
	11	1800					20	270					265	485	300	350	285	530		250		820
TMC-125C	7.5	1800	125	125	140	420	200	270	20	80	75	285	485	300	350	285	530	250	265	820	19	
	15	1800					20	270					265	485	300	350	285	530		250		880



CENTRIFUGAL PUMP

TMS



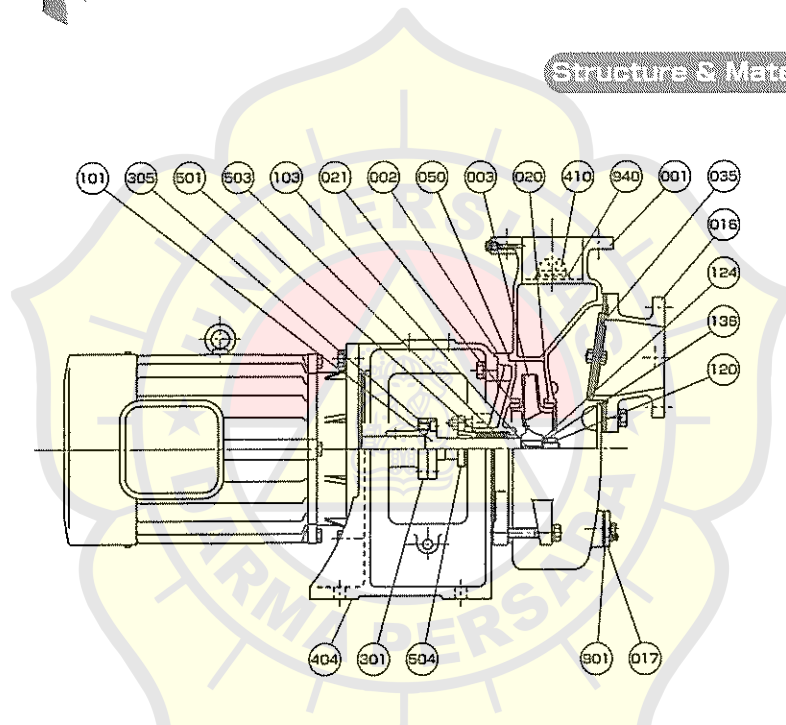
Application

Fire & G.S. Pump
Bilge & Ballast Pump

Feature

Horizontal Single-stage Single-suction
Self-priming Closed Coupling Type

Structure & Material

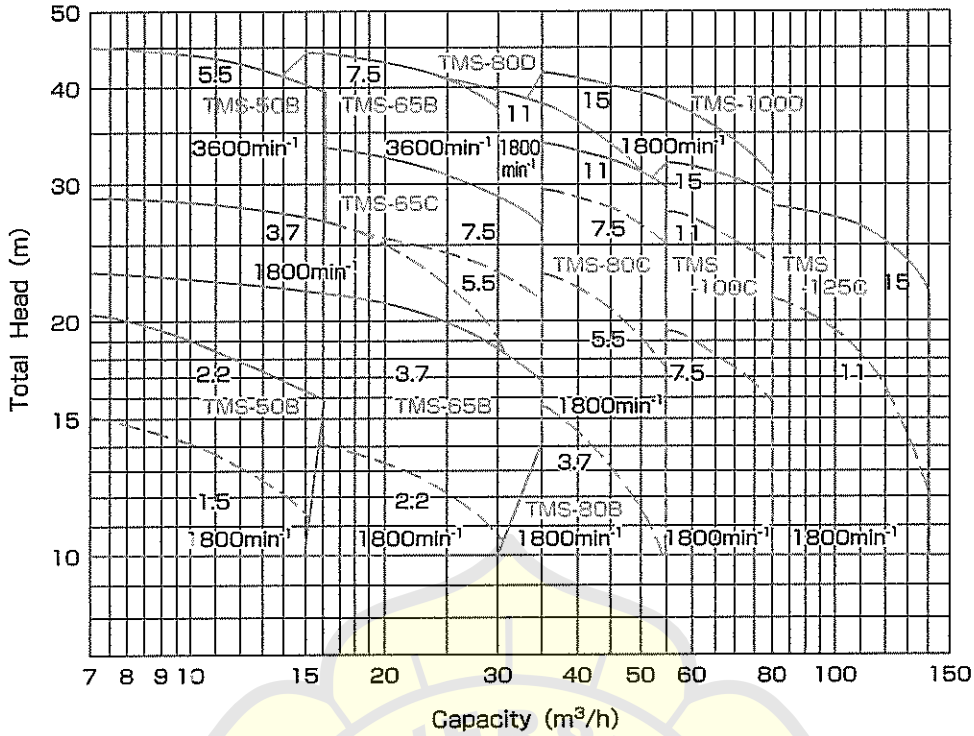


2-4

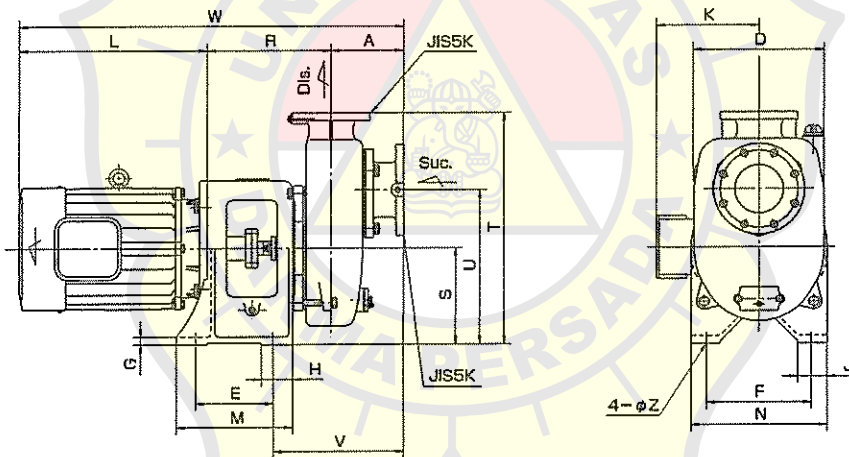
Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
001	CASING	1	BRONZE	CAC402	CAST IRON	FC200
002	CASING COVER	1	BRONZE	CAC402	CAST IRON	FC200
003	IMPELLER	1	PHOSPHOR BRONZE	CAC502A	PHOSPHOR BRONZE	CAC502A
016	SUCTION COVER	1	BRONZE	FC200	CAST IRON	FC200
017	DRAIN COVER	1	BRONZE	FC200	CAST IRON	FC200
020	CASING RING	1	BRONZE	CAC402	BRONZE	CAC402
021	CASING RING	1	BRONZE	CAC402	BRONZE	CAC402
035	CHECK VALVE	1	RUBBER / BRONZE	NBR / CAC402	RUBBER / BRONZE	NBR / CAC402
050	O-RING	1	RUBBER	NBR	RUBBER	NBR
101	SHAFT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
103	IMPELLER KEY	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
120	IMPELLER NUT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304

Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
124	IMPELLER WASHER	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
136	SPRING WASHER	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
301	COUPLING	1	MILD STEEL	SS400	MILD STEEL	SS400
305	COUPLING BOLT	4	Cr-Mo STEEL	SCM435	Cr-Mo STEEL	SCM435
404	PUMP FRAME	1	CAST IRON	FC200	CAST IRON	FC200
410	PRIMING CAP	1	BRONZE	CAC402	BRONZE	CAC402
501	GLAND PACKING	4	CARBONIZED FIBER	-	CARBONIZED FIBER	-
503	LANTERN RING	1	BRONZE	CAC402	BRONZE	CAC402
504	GLAND	1	BRONZE	CAC402	BRONZE	CAC402
901	GASKET	1	RUBBER	NBR	RUBBER	NBR
940	GASKET	1	RUBBER	NBR	RUBBER	NBR

Performance

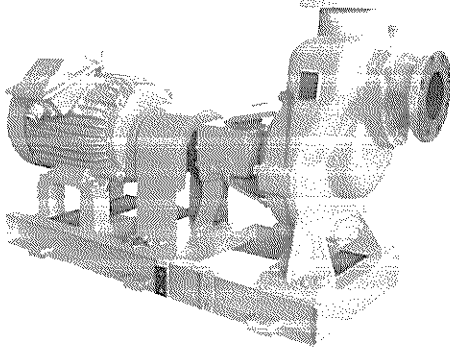


Dimension



Model No.	Motor		Bore		Dimension (mm)																							
	kW	min ⁻¹	Suc.	Dis.	A	D	E	F	G	H	J	K	L	M	N	R	S	T	U	V	W	Z						
TMS-50B	1.5	1800	50	50	150	270	150	220	18	80	65	195	300	250	280	240	180	455	315	280	690	15						
	2.2	1800					180	220				205	330	280		250					730							
	5.5	3600					200	270				265	400	300		270					210		475	335	820			
TMS-65B	2.2	1800	65	65	150	275	180	220	18	80	65	205	330	280	280	260	190	455	315	280	740	15						
	3.7	1800					200	270				215	355	280		280					210		475	335	765			
	7.5	3600					180	220				265	400	300		280					210		475	335	830			
TMS-65C	3.7	1800	65	65	150	325	200	270	18	80	65	215	355	280	280	260	190	480	330	290	765	15						
	5.5	1800					200	270				265	400	300		330					210		500	350	830			
	7.5	1800					180	220				215	355	280		280					210		480	330	830			
TMS-80B	3.7	1800	80	80	165	305	180	220	18	80	65	215	355	280	280	270	180	480	315	315	780	15						
	5.5	1800																					265	400	300	350	290	250
TMS-80C	7.5	1800	80	80	165	340	200	270	18	80	75	265	400	300	350	290	250	600	400	315	855	19						
	11	1800																					285	485	320	320	290	970
TMS-80D	11	1800	80	80	165	480	200	270	20	80	75	285	485	300	350	335	250	625	425	330	985	19						
	7.5	1800																					265	400	290	290	875	
TMS-100C	11	1800	100	100	185	340	200	270	20	80	75	285	485	300	350	320	250	600	400	335	890	19						
	15	1800																					285	485	320	320	290	1030
	5.5	1800																					265	400	290	290	875	
TMS-100D	15	1800	100	100	165	480	200	270	20	80	75	285	525	300	350	335	250	625	425	330	1025	19						
	11	1800																					265	400	290	290	875	
TMS-125C	11	1800	125	125	210	365	200	270	20	80	75	285	485	300	350	335	250	625	425	375	1030	19						
	15	1800																					265	400	290	290	875	

CENTRIFUGAL PUMP EHS



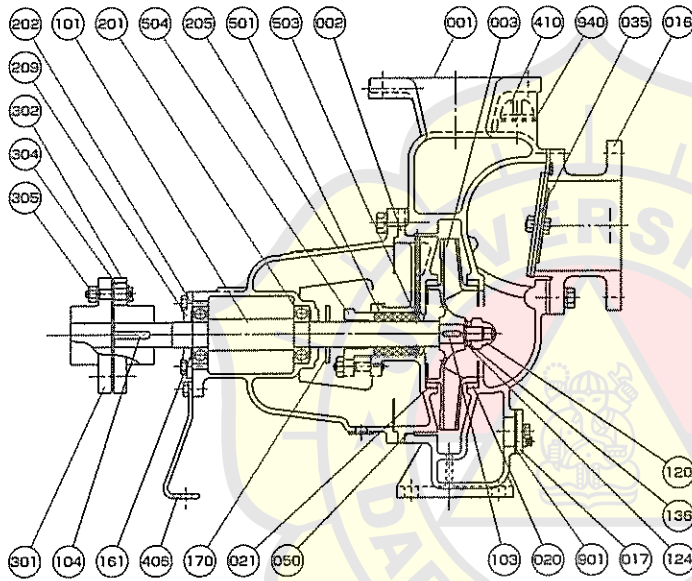
Application

Fire & G.S. Pump
Bilge & Ballast Pump

Feature

Horizontal Single-stage Single-suction
Self-priming Type

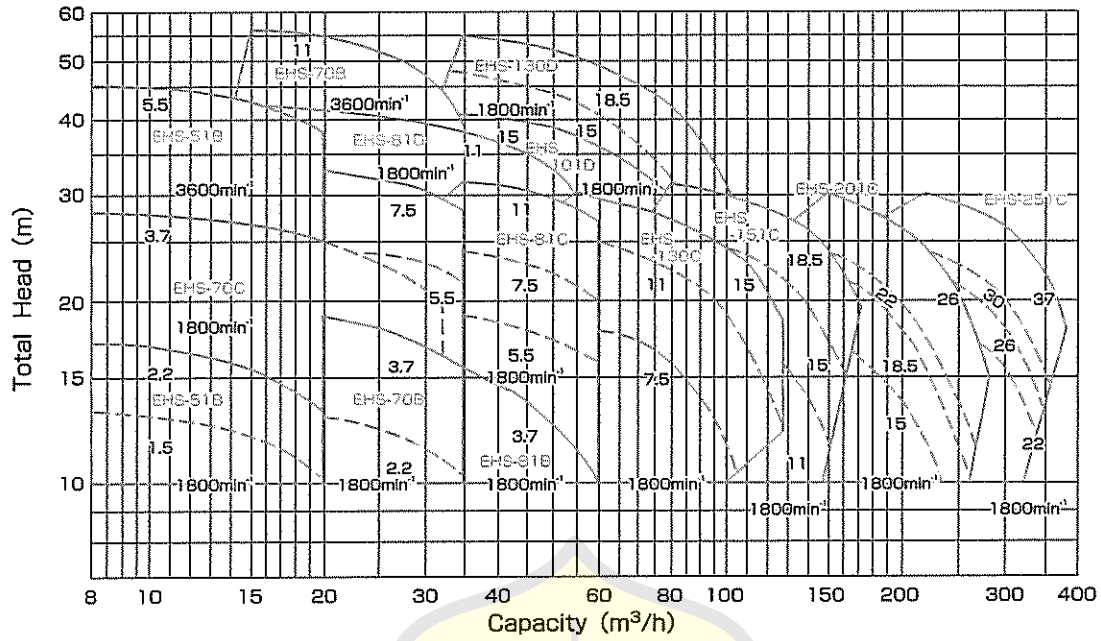
Structure & Material



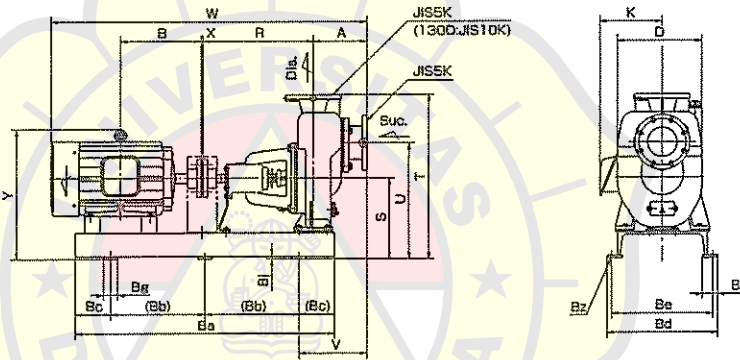
Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
001	CASING	1	BRONZE	CAC402	CAST IRON	FC200
002	CASING COVER	1	BRONZE	CAC402	CAST IRON	FC200
003	IMPELLER	1	PHOSPHOR BRONZE	CAC502A	PHOSPHOR BRONZE	CAC502A
016	SUCTION COVER	1	BRONZE	CAC402	CAST IRON	FC200
017	DRAIN COVER	1	BRONZE	CAC402	CAST IRON	FC200
020	CASING RING	1	BRONZE	CAC402	BRONZE	CAC402
021	CASING RING	1	BRONZE	CAC402	BRONZE	CAC402
035	CHECK VALVE	1	RUBBER / BRONZE	NBR / CAC402	RUBBER / BRONZE	NBR / CAC402
050	O-RING	1	RUBBER	NBR	RUBBER	NBR
101	SHAFT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
103	KEY	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
104	KEY	1	CARBON STEEL	S45C	CARBON STEEL	S45C
120	IMPELLER NUT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
124	IMPELLER WASHER	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
136	SPRING WASHER	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
161	RETAINING RING	1	SPRING STEEL	SUP6	SPRING STEEL	SUP6

Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
170	FLINGER	1	RUBBER	NBR	RUBBER	NBR
201	BALL BEARING	1	BEARING STEEL	SUJ2	BEARING STEEL	SUJ2
202	BALL BEARING	1	BEARING STEEL	SUJ2	BEARING STEEL	SUJ2
205	BEARING HOUSING	1	CAST IRON	FC200	CAST IRON	FC200
209	BEARING COVER	1	CAST IRON	FC200	CAST IRON	FC200
301	COUPLING	1	CAST IRON	FC200	CAST IRON	FC200
302	COUPLING	1	CAST IRON	FC200	CAST IRON	FC200
304	COUPLING RING	8	RUBBER	NBR	RUBBER	NBR
305	COUPLING BOLT&NUT	8	MILD STEEL	SS400	MILD STEEL	SS400
406	SUPPORT	1	MILD STEEL	SS400	MILD STEEL	SS400
410	PRIMING CAP	1	BRONZE	CAC402	BRONZE	CAC402
501	GLAND PACKING	4	CARBONIZED FIBER	-	CARBONIZED FIBER	-
503	LANTERN RING	1	BRONZE	CAC402	BRONZE	CAC402
504	GLAND	1	BRONZE	CAC402	BRONZE	CAC402
901	GASKET	1	RUBBER	NBR	RUBBER	NBR
940	GASKET	1	RUBBER	NBR	RUBBER	NBR

Performance

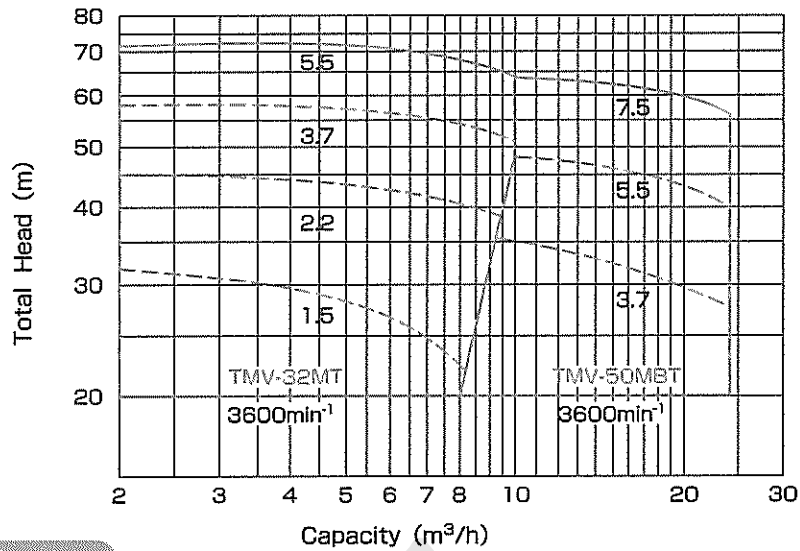


Dimension

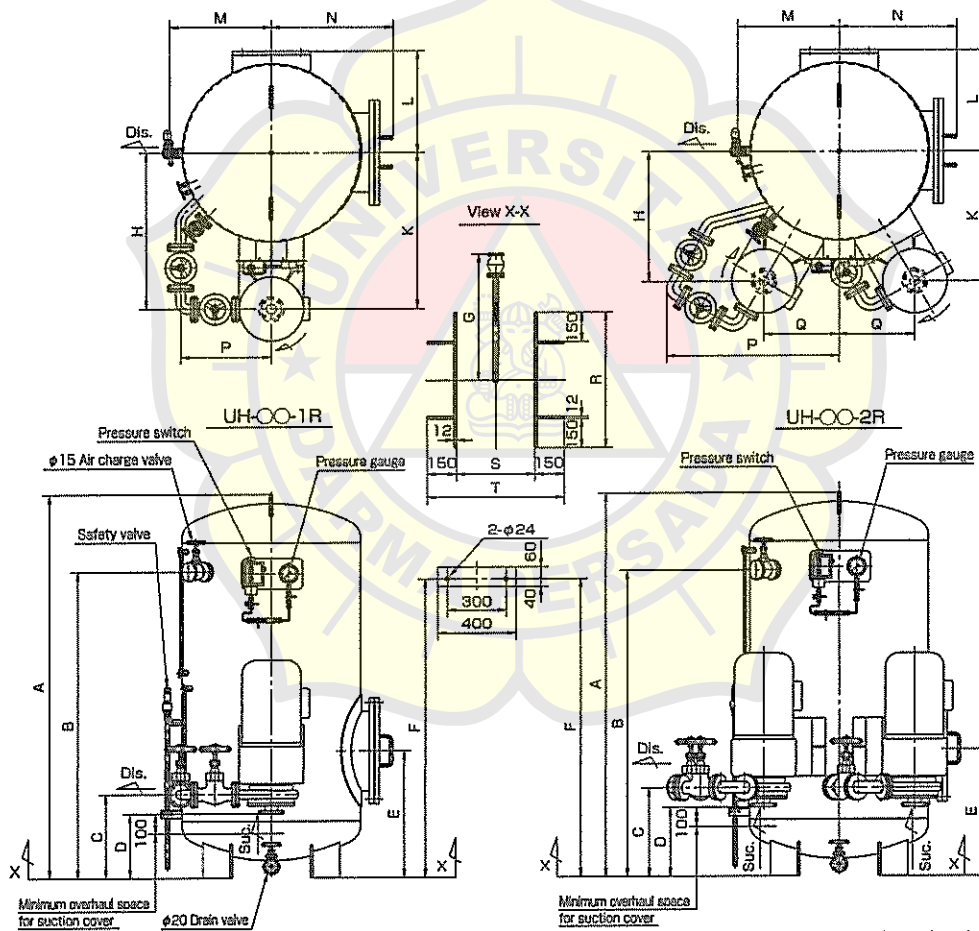


Model No.	Motor		Bore		Dimension (mm)																				
	kW	min ⁻¹	Suc.	Dis.	A	B	D	K	R	S	T	U	V	W	X	Y	Ba	Bb	Bc	Bd	Be	Bf	Bg	Bi	Bz
EHS-51B	1.5	1800	50	50	168.5	189	189	189	355	270	538	380	239	867	3	355	700	450	125	325	290	55	50	12	4-φ15
	2.2	1800			193	193	254	197	355	270	538	380	239	914	3	375	700	450	150	325	290	55	50	12	4-φ15
	6.5	3600			239	239		245	355	270	538	380	248	990	3	428	800	500	150	325	290	55	50	12	4-φ15
EHS-70B	2.2	1800	65	65	188	193	187	187	355	270	538	380	248	924	3	375	700	450	125	325	290	55	50	12	4-φ15
	3.7	1800			200	200	262	212	355	270	538	380	248	944	3	416	800	500	150	325	290	55	50	12	4-φ15
	11	3600			323	323		285	355	270	538	380	248	1154	3	500	1000	700	150	325	290	55	50	12	4-φ15
EHS-70C	3.7	1800	65	65	188	200	212	212	355	290	595	430	248	944	3	436	800	500	150	390	350	65	60	12	4-φ15
	5.5	1800			239	239	313	245	355	290	595	430	273	1039	3	436	900	550	175	390	350	65	60	12	4-φ19
	7.5	1800			258	258		245	355	290	595	430	273	1039	3	436	900	550	175	390	350	65	60	12	4-φ19
EHS-81B	3.7	1800	80	80	230	200	276	212	355	290	595	400	300	996	3	436	800	500	150	390	350	65	60	12	4-φ15
	5.5	1800			239	239		245	355	290	595	400	300	1132	3	436	800	500	150	390	350	65	60	12	4-φ15
EHS-81C	7.5	1800	80	80	205	258	337	285	470	320	670	470	285	1171	3	478	1000	350	150	470	430	65	60	12	6-φ19
	11	1800			323	323		285	470	320	670	470	285	1286	3	550	1100	400	150	470	430	65	60	12	6-φ19
EHS-81D	11	1800	80	80	215	323	394	285	470	345	720	520	275	1286	3	575	1100	400	150	470	430	65	60	12	6-φ19
	15	1800	100	100	225	345	400	285	470	370	745	545	285	1348	3	600	1100	400	150	470	430	65	60	12	6-φ19
EHS-101D	7.5	1800	100	100	225	258		245	470	370	745	545	285	1191	3	503	1000	350	150	470	430	65	60	12	6-φ19
	11	1800	125	125	225	323	358	285	470	345	700	465	285	1306	3	575	1100	400	150	470	430	65	60	12	6-φ19
	15	1800			345	345		285	470	370	745	545	285	1348	3	600	1100	400	150	470	430	65	60	12	6-φ19
EHS-130C	15	1800	125	125	225	345		285	470	370	745	545	285	1191	3	503	1000	350	150	470	430	65	60	12	6-φ19
	18.5	1800	150	150	285	345	416	285	470	370	770	545	340	1306	3	575	1100	400	150	470	430	65	60	12	6-φ19
EHS-130D	11	1800	100	100	225	323		330	470	370	745	545	340	1508	3	600	1200	450	150	470	430	65	60	12	6-φ19
	18.5	1800	125	125	225	351.5		330	470	370	745	545	340	1520	3	630	1200	450	150	470	430	65	60	12	6-φ19
EHS-151C	11	1800	150	150	285	323		285	470	345	720	520	345	1386	3	575	1100	400	150	470	430	65	60	12	6-φ19
	15	1800			345	345	353	285	470	345	720	520	345	1408	3	605	1100	400	150	470	430	65	60	12	6-φ19
	18.5	1800			351.5	351.5		285	470	345	720	520	345	1420	3	605	1100	400	150	470	430	65	60	12	6-φ19
EHS-201C	15	1800	200	200	325	345		285	470	370	810	570	385	1448	3	600	1100	400	150	470	430	65	60	12	6-φ19
	18.5	1800			351.5	351.5	400	330	470	370	810	570	385	1448	3	630	1100	400	150	470	430	65	60	12	6-φ19
	22	1800			370.5	370.5		330	470	370	810	570	385	1499	3	630	1200	450	150	470	430	65	60	12	6-φ19
EHS-251C	22	1800	250	250	335	351.5		330	530	430	960	660	365	1530	3	690	1200	450	150	550	500	65	60	25	6-φ19
	26	1800			370.5	370.5	500	330	530	430	960	660	365	1568	3	705	1300	500	150	550	500	65	60	25	6-φ19
	37	1800			425.5	425.5		345	530	430	960	660	365	1650	4	705	1300	500	150	550	500	65	60	25	6-φ19

Performance



Dimension

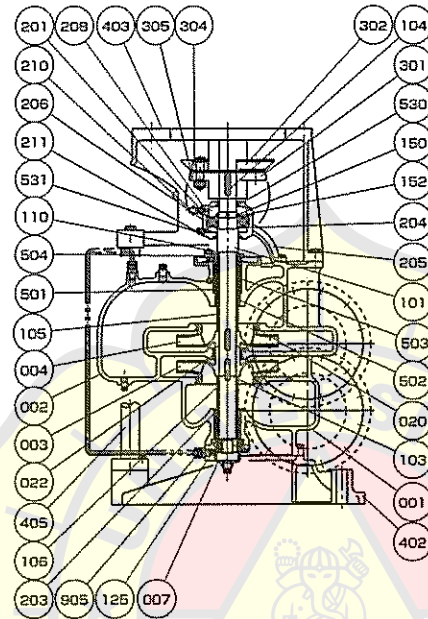
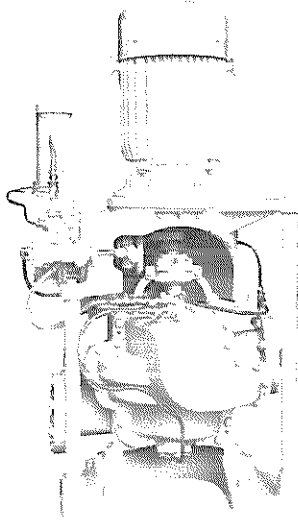


*mark is based on the bore size of attached pump.

Model No.	Bore		Tank Volume (L)	Dimension (mm)																
	Suc.	Dis.		A	B	C	D	E	F	G	H	K	L	M	N	P	Q	R	S	T
UH-0.5-1R	*	50	500	1198	805	450	350	600	795	625	680	680	495	520	595	260	-	700	400	700
UH-0.5-2R	*	50	500	1198	880	450	350	600	795	625	589	589	495	520	595	560	340	700	400	700
UH-1.0-1R	*	50	1000	1967	1570	450	350	650	1620	650	720	720	520	520	620	240	-	700	400	700
UH-1.0-2R	*	50	1000	1967	1570	450	350	650	1620	650	624	624	520	520	620	580	360	700	400	700
UH-1.5-1R	*	50	1500	1956	1530	450	350	700	1620	750	820	820	620	650	715	240	-	800	500	800
UH-1.5-2R	*	50	1500	1956	1530	450	350	700	1620	750	710	710	620	650	715	630	410	800	500	800
UH-2.0-1R	*	50	2000	2170	1700	450	350	750	1630	800	860	960	670	700	785	280	-	800	600	900
UH-2.0-2R	*	50	2000	2170	1700	450	350	750	1630	800	830	830	670	700	785	734	480	900	600	900

CENTRIFUGAL PUMP

VS



Application

Fire & G.S. Pump
Bilge & Ballast Pump

Feature

Vertical Two-stage Single-suction
Split-casing Type

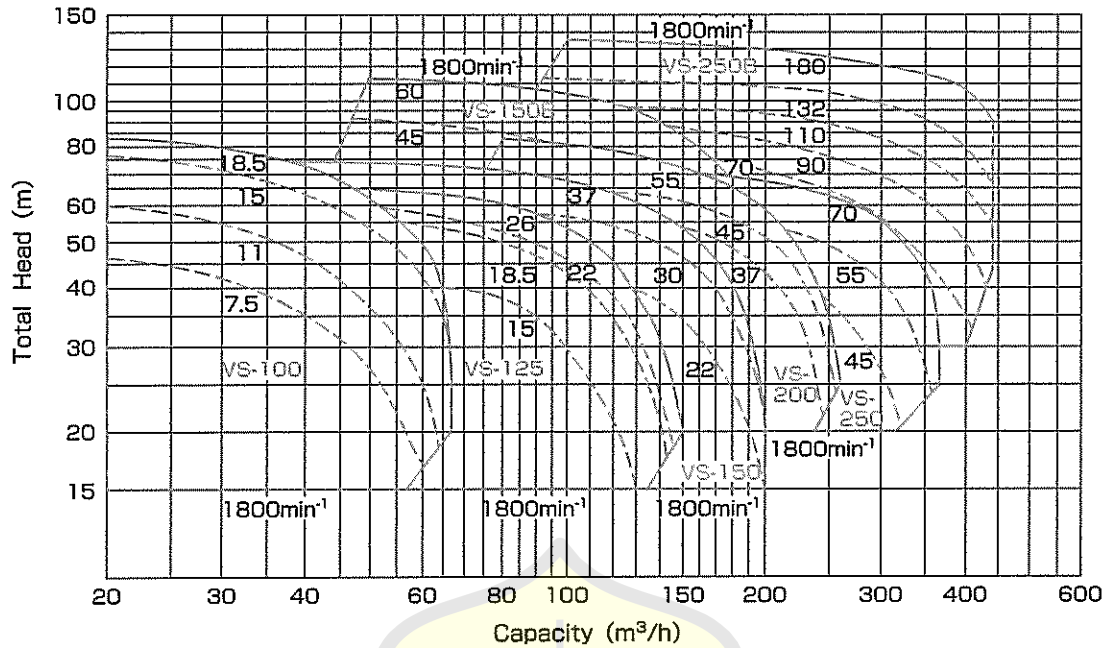
Structure & Material

2 / 2

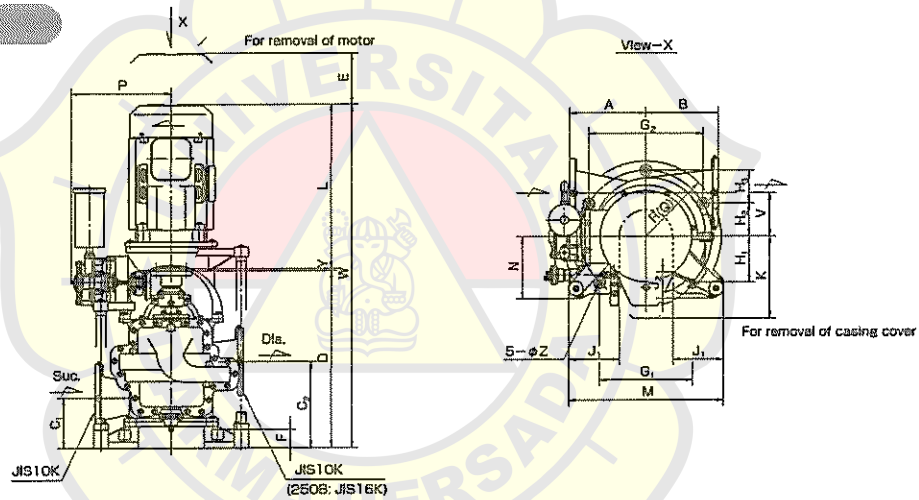
Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
001	CASING	1	BRONZE	CAC402	CAST IRON	FC200
002	CASING COVER	1	BRONZE	CAC402	CAST IRON	FC200
003	IMPELLER	1	PHOSPHOR BRONZE	CAC502A	PHOSPHOR BRONZE	CAC502A
004	IMPELLER	1	PHOSPHOR BRONZE	CAC502A	PHOSPHOR BRONZE	CAC502A
007	BOTTOM COVER	1	BRONZE	CAC402	CAST IRON	FC200
020	CASING RING	2	BRONZE	CAC402	BRONZE	CAC402
022	STAGE BUSH	1	BRONZE	CAC402	BRONZE	CAC402
101	SHAFT	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
103	KEY	2	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
104	KEY	1	CARBON STEEL	S45C	CARBON STEEL	S45C
105	SLEEVE	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
106	SLEEVE	1	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
110	O-RING	1	RUBBER	NBR	RUBBER	NBR
125	SLEEVE NUT	2	STAINLESS STEEL	SUS304	STAINLESS STEEL	SUS304
150	BEARING NUT	1	MILD STEEL	SS400	MILD STEEL	SS400
152	BEARING WASHER	1	MILD STEEL	SS400	MILD STEEL	SS400
201	BALL BEARING	1	BEARING STEEL	SUJ2	BEARING STEEL	SUJ2
203	BOTTOM METAL	1	LEAD BRONZE	-	LEAD BRONZE	-
204	BEARING SPACER	1	MILD STEEL	SS400	MILD STEEL	SS400
205	BEARING HOUSING	1	CAST IRON	FC200	CAST IRON	FC200

Part No.	Name	Req. No.	Sea Water		Fresh Water	
			Material	JIS	Material	JIS
206	HOUSING COVER	1	CAST IRON	FC200	CAST IRON	FC200
208	BEARING COVER	1	CAST IRON	FC200	CAST IRON	FC200
210	GREASE NIPPLE	1	BRASS	C3602	BRASS	C3602
211	GREASE FITTING	1	BRASS	C3602	BRASS	C3602
301	COUPLING	1	CAST IRON	FC200	CAST IRON	FC200
302	COUPLING	1	CAST IRON	FC200	CAST IRON	FC200
304	COUPLING RING	8	RUBBER	NBR	RUBBER	NBR
305	COUPLING BOLT & NUT	8	MILD STEEL	SS400	MILD STEEL	SS400
402	PUMP BED	1	CAST IRON	FC200	CAST IRON	FC200
403	MOTOR FRAME	1	CAST IRON	FC200	CAST IRON	FC200
405	SUPPORT	2	STEEL GAS PIPE	SGP	STEEL GAS PIPE	SGP
501	GLAND PACKING	5	CARBONIZED FIBER	-	CARBONIZED FIBER	-
502	NECK BUSH	1	BRONZE	CAC402	BRONZE	CAC402
503	LANTERN RING	1	BRONZE	CAC402	BRONZE	CAC402
504	GLAND	1	BRONZE	CAC402	BRONZE	CAC402
530	OIL SEAL	1	RUBBER	NBR	RUBBER	NBR
531	OIL SEAL	1	RUBBER	NBR	RUBBER	NBR
900	GASKET	1	PAPER	-	PAPER	-
905	GASKET	1	RUBBER	NBR	RUBBER	NBR

Performance



Dimension



Model No.	Motor		Bore		Dimension (mm)																								
	kW	min ⁻¹	Suc.	Dia.	A	B	C1	C2	D	E	F	G1	G2	H1	H2	H3	J1	J2	K	L	M	N	P	Q	V	W	Y	Z	
VS-100	7.5								150											480						829			
	11	1800	100	100	300	270	220	380	846		80	368	450	184	130	130	175	80	450	695	590	240	485	310	170	844	3	24	
	15								200											635						894			
	18.5																			695						1034			
VS-125	15																			635						1598			
	18.5	1800	125	125	290	320	262	442	960	200	90	353	433	177	125	125	180	105	540	695	630	255	485	300	175	1648	3	26	
	22																			725						1688	4		
	26																			695						1564	3		
VS-150	22																			695						1605			
	30	1800	150	150	370	350	245	428	876	200	80	424	520	212	150	150	215	120	630	725	750	303	485	360	210	1605	4	28	
	37																			800						1680			
	45																			800						1776			
VS-150B	60																			1050						2026			
	45	1800	150	150	350	330	262	442	972	250	90	424	520	212	150	150	215	120	630	800	750	303	485	360	200	1776	4	28	
	60																			1050						2026			
	37																			800						1680			
VS-200	45	1800	200	200	370	350	245	428	876	250	90	424	520	212	150	150	215	120	630	800	750	303	485	360	210	1680	4	28	
	55																			850						1830			
	45																			800						1758			
	55																			850						1830			
VS-250	45	1800	200	200	400	430	290	552	955	250	90	424	520	212	150	150	215	120	670	850	750	303	485	360	210	1908	4	28	
	55																			950						2008			
	70																			1050						2148			
	110																			1210						2308	4	28	
VS-250B	132	1800	250	250	430	430	290	490	1085	250	80	452	554	226	160	160	245	105	800	1210	750	303	540	365	330	2308			
	180																			1566						2665			
	132																			1280						2388			
	180																			1566						2665			

REFERENSI BAB VI



Table 18.2 Anchor, Chain Cables and Ropes

No. for Reg.	Equipment numeral Z ₁ or Z ₂	Stockless anchor			Stud link chain cables						Recommended ropes				
		Bower anchor		Stream anchor	Bower anchors			Stream wire or chain for stream anchor		Towline		Mooring ropes			
		Number ¹⁾	Mass per anchor		Total length	Diameter			Length	Br. load ²⁾	Length	Br. load ²⁾	Number	Length	Br. load ²⁾
				d ₁		d ₂	d ₃	[m]							
			[kg]	[m]	[mm]	[mm]	[mm]	[m]	[kN]	[m]	[kN]		[m]	[kN]	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
101	up to 50	2	120	40	165	12,5	12,5	12,5	80	65	180	100	3	80	35
102	50 - 70	2	180	60	220	14	12,5	12,5	80	65	180	100	3	80	35
103	70 - 90	2	240	80	220	16	14	14	55	75	150	100	3	100	40
104	90 - 110	2	300	100	247,5	17,5	16	16	85	80	180	100	3	110	40
105	110 - 130	2	360	120	247,5	19	17,5	17,5	90	90	180	100	3	110	45
106	130 - 150	2	420	140	275	20,5	17,5	17,5	90	100	180	100	3	120	50
107	150 - 175	2	480	165	275	22	19	19	90	110	180	100	3	120	55
108	175 - 205	2	570	190	302,5	24	20,5	20,5	90	120	150	110	3	120	60
109	205 - 240	2	660	240	302,5	26	22	22	90	120	150	110	4	120	65
110	240 - 280	2	780	300	330	28	24	24	180	150	180	150	4	120	70
111	280 - 320	2	900	360	357,5	30	26	24	180	175	180	175	4	140	80
112	320 - 360	2	1020	420	357,5	32	28	24	180	200	180	200	4	140	85
113	360 - 400	2	1140	480	385	34	30	26	180	225	180	225	4	140	95
114	400 - 450	2	1290	540	385	36	32	28	180	250	180	250	4	140	100
115	450 - 500	2	1440	600	412,5	38	34	30	180	275	180	275	4	140	110
116	500 - 550	2	1590	660	412,5	40	34	30	190	305	180	305	4	160	120
117	550 - 600	2	1740	720	440	42	36	32	190	340	190	340	4	160	130
118	600 - 660	2	1920	840	440	44	38	34	190	370	190	370	4	160	145
119	660 - 720	2	2100	960	440	46	40	36	190	405	190	405	4	160	160
120	720 - 780	2	2280	1080	467,5	48	42	36	190	440	190	440	4	170	170
121	780 - 840	2	2460	1200	467,5	50	44	38	190	480	190	480	4	170	185
122	840 - 910	2	2640	1320	467,5	52	46	40	190	520	190	520	4	170	200
123	910 - 980	2	2850	1440	495	54	48	42	190	560	190	560	4	170	215
124	980 - 1060	2	3060	1560	495	56	50	44	200	600	190	600	4	180	230
125	1060 - 1140	2	3300	1680	495	58	50	46	200	645	190	645	4	180	250
126	1140 - 1220	2	3540	1800	522,5	60	52	46	200	690	190	690	4	180	270
127	1220 - 1300	2	3780	1920	522,5	62	54	48	200	740	190	740	4	180	285
128	1300 - 1390	2	4050	2040	522,5	64	56	50	200	785	190	785	4	180	305
129	1390 - 1480	2	4320	2160	550	66	58	50	200	835	190	835	4	180	325
130	1480 - 1570	2	4590	2280	550	68	60	52	220	890	190	890	5	190	325
131	1570 - 1670	2	4890	2400	550	70	62	54	220	940	190	940	5	190	335
132	1670 - 1790	2	5250	2520	577,5	73	64	56	220	1025	190	1025	5	190	350
133	1790 - 1930	2	5610	2640	577,5	76	66	58	220	1110	190	1110	5	190	375
134	1930 - 2080	2	6000	2760	577,5	78	68	60	220	1170	190	1170	5	190	400
135	2080 - 2230	2	6450	2880	605	81	70	62	240	1260	190	1260	5	200	425
136	2230 - 2380	2	6900	3000	605	84	73	64	240	1355	190	1355	5	200	450
137	2380 - 2530	2	7350	3120	605	87	76	66	240	1455	190	1455	5	200	480
138	2530 - 2700	2	7800	3240	632,5	90	78	68	260	1470	190	1470	6	200	490
139	2700 - 2870	2	8300	3360	632,5	92	81	70	260	1470	190	1470	6	200	490
140	2870 - 3040	2	8760	3480	632,5	95	84	73	260	1470	190	1470	6	200	500
141	3040 - 3210	2	9300	3600	660	97	84	76	280	1470	190	1470	6	200	520
142	3210 - 3400	2	9900	3720	660	100	87	78	280	1470	190	1470	6	200	555
143	3400 - 3600	2	10500	3840	660	102	90	78	280	1470	190	1470	6	200	590
144	3600 - 3800	2	11100	3960	687,5	105	92	81	300	1470	190	1470	6	200	620
145	3800 - 4000	2	11700	4080	687,5	107	95	84	300	1470	190	1470	6	200	650
146	4000 - 4200	2	12300	4200	687,5	111	97	87	300	1470	190	1470	7	200	650
147	4200 - 4400	2	12900	4320	715	114	100	87	300	1470	190	1470	7	200	660
148	4400 - 4600	2	13500	4440	715	117	102	90	300	1470	190	1470	7	200	670
149	4600 - 4800	2	14100	4560	715	120	105	92	300	1470	190	1470	7	200	680
150	4800 - 5000	2	14700	4680	742,5	122	107	95	300	1470	190	1470	7	200	685
151	5000 - 5200	2	15400	4800	742,5	124	111	97	300	1470	190	1470	8	200	685
152	5200 - 5500	2	16100	4920	742,5	127	111	97	300	1470	190	1470	8	200	695
153	5500 - 5800	2	16900	5040	742,5	130	114	100	300	1470	190	1470	8	200	705
154	5800 - 6100	2	17800	5160	742,5	132	117	102	300	1470	190	1470	9	200	705
155	6100 - 6500	2	18900	5280	742,5	120	107	95	300	1470	190	1470	9	200	715
156	6500 - 6900	2	20000	5400	770	124	111	97	300	1470	190	1470	9	200	725
157	6900 - 7400	2	21500	5520	770	127	114	97	300	1470	190	1470	10	200	725
158	7400 - 7900	2	23000	5640	770	132	117	102	300	1470	190	1470	11	200	725
159	7900 - 8400	2	24500	5760	770	137	122	111	300	1470	190	1470	11	200	735
160	8400 - 8900	2	26000	5880	770	142	127	111	300	1470	190	1470	12	200	735
161	8900 - 9400	2	27500	6000	770	147	132	111	300	1470	190	1470	13	200	735
162	9400 - 10000	2	29000	6120	770	152	132	111	300	1470	190	1470	14	200	735
163	10000 - 10700	2	31000	6240	770	157	137	111	300	1470	190	1470	15	200	735
164	10700 - 11500	2	33000	6360	770	162	142	111	300	1470	190	1470	16	200	735
165	11500 - 12400	2	35500	6480	770	167	147	111	300	1470	190	1470	17	200	735
166	12400 - 13400	2	38500	6600	770	172	152	111	300	1470	190	1470	18	200	735
167	13400 - 14600	2	42000	6720	770	177	157	111	300	1470	190	1470	19	200	735
168	14600 - 16000	2	46000	6840	770	182	162	111	300	1470	190	1470	21	200	735

d₁ = Chain diameter Grade K 1 (Ordinary quality)
 d₂ = Chain diameter Grade K 2 (Special quality)
 d₃ = Chain diameter Grade K 3 (Extra special quality)

See also D

¹⁾ see C.1.
²⁾ see F.1.2

Pada kemudi balansir, untuk, mengurangi kemungkinan getaran, bagian luasan balansir dianjurkan $\leq 23\%$ dari seluruh luas kemudi dan lebar bagian balansir pada potongan-potongan horisontal $< 0,35$ lebar sayap kemudi.

Pada kapal-kapal yang mempunyai batas sarat air yang cukup tinggi, mempunyai ukuran yang tinggi ($\lambda = hp/bp$ cukup tinggi).

Tetapi tinggi kemudi harus diperlihatkan pula menurut bentuk buritan kapal.

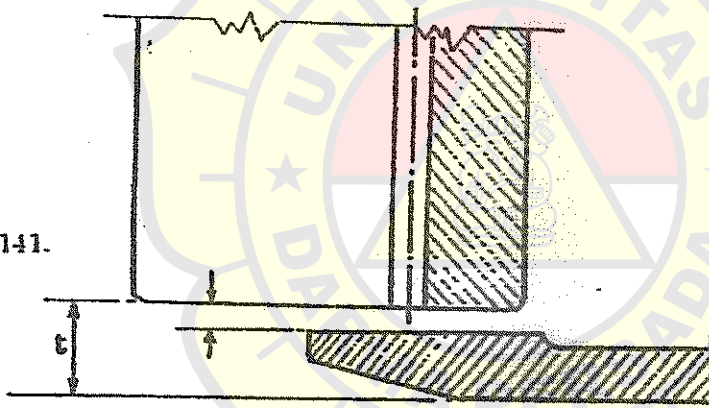
Beberapa batasan untuk harga λ :

- Kapal barang dan kapal penumpang : $\lambda = 1,8$
- Kapal coaster : $\lambda = 1,05 - 1,15$
- Kapal tunda, pandu : $\lambda = 1,8$
- Kapal ikan ukuran sedang : $\lambda = 1,55 - 2,0$

Dianjurkan tinggi tiap-tiap kemudi harus menutupi diameter baling-baling. Bagian bawah kemudi untuk menjaga kerusakan-kerusakan dari geseran dengan dasar laut harus lebih tinggi dari garis dasar kapal.

Batas-batasnya sebagai berikut :

Gambar 141.



- Untuk kemudi menggantung atau setengah menggantung
 $t = (4 - 10\%) h$
- Untuk kemudi bertumpu
 $t = (6 - 12)\% h$

- Dimana :

$h =$ tinggi kemudi

Catatan : Umumnya untuk semua bentuk diambil ketentuan :

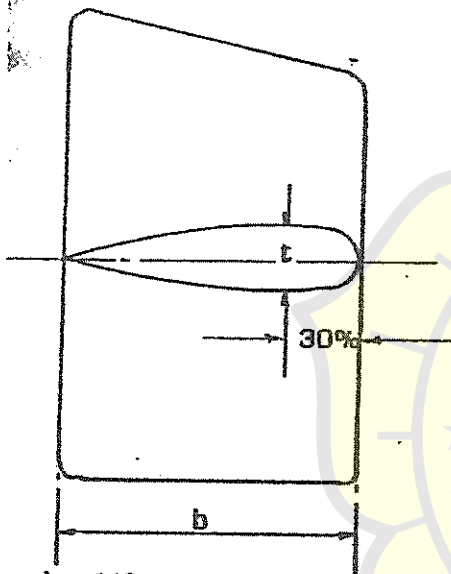
$t \geq 150 \text{ mm}$.

Oleh Van Lammeren ditetapkan batasan-batasan $\lambda = h/b$ sebagai berikut :

Type kapal dan kemudi	h/d
1. kapal barang 1 baling-baling dan kapal penumpang semuanya dengan kemudi balansir.	1,8
2. Kapal pantai 1 baling-baling dengan kemudi balansir.	1,15
3. Kapal tunda 1 baling-baling dan kapal pandu.	1,75

4. Untuk semua kapal dengan 2 baling-baling dengan kemudi biasa.	1,5
5. Untuk kapal-kapal 2 baling-baling dengan kemudi-setengah balansir.	1,1
6. Untuk kapal-kapal dengan 2 baling-baling dengan dua kemudi.	2,2

Bentuk kemudi harus dibuat sedemikian supaya dengan perubahan letak kemudi dalam sudut attack yang tidak begitu besar, kapal dapat membuat belokan besar, dengan catatan pada saat yang sama dengan perubahan letak kemudi tersebut diperhitungkan supaya tidak mempengaruhi kecepatan kapal.



gambar 142.

Berdasarkan praktek yang dilakukan, koefisien tebal plat profil kemudi :

$C_t = t/b$ terletak dalam batas-batas : 0,18 - 0,22.

Tetapi untuk kemudi setengah menggantung pada kapal besar hanya C_t mencapai 0,5.

Untuk kemudi biasa (tak balansir) untuk twin screw diambil batas-batas:

$$C_t = 0,15 - 0,18$$

Untuk setengah balansir :

$$C_t = 0,18 - 0,22$$

Kemudi kembar menggantung biasanya lebih tebal dari kemudi yang bertumpu, tetapi untuk menjaga kekuatan, kemudi tersebut mempunyai harga : $C_t = 0,2$

Untuk menghindari getaran dianjurkan supaya jarak maximum di depan kemudi yaitu 30% lebar profil, dihitung dari permukaan depan.

Koefisien kompensasi dihitung dengan rumus pendekatan yang menghasilkan perhitungan moment putar yang sangat kecil di poros, hingga memperkecil kekuatan motor penggerak kemudi serta pengurangan energi untuk merubah letak kemudi.

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Tabel II

L. B. H (m)	L. B. H (ft)	Kapasitas (lt)	Jumlah orang	berat sekoci (kg)	Berat Orang (kg)	berat perlengkapan (kg)	Total berat (kg)
9,4 x 2,74 x 1,114	30 x 9 x 3,75	607	60	2205	4500	356	7061
8,84 x 2,74 x 1,10	28 x 8,75 x 3,60	645	54	1976	4050	356	6382
8,63 x 2,59 x 1,07	28 x 8,50 x 3,50	500	50	1824	3750	330	5894
8,23 x 2,51 x 1,04	27 x 8,25 x 3,40	454	45	1646	3376	330	5351
7,92 x 2,44 x 0,99	26 x 8,00 x 3,25	405	40	473	3000	305	4778
7,62 x 2,36 x 0,96	25 x 7,75 x 3,15	366	36	1326	2700	305	4331
7,31 x 2,29 x 0,91	24 x 7,50 x 3,00	324	32	1180	2400	254	3843
7,01 x 2,20 x 0,88	23 x 7,50 x 2,90	300	30	1087	2250	254	3591
6,71 x 2,21 x 0,84	22 x 7,25 x 2,75	236	26	955	1950	229	3134
6,40 x 2,13 x 0,82	21 x 7,00 x 2,70	238	23	864	1725	229	2818
6,10 x 2,06 x 0,79	20 x 6,75 x 2,60	210	21	762	1575	203	2540
5,79 x 1,98 x 0,76	19 x 6,50 x 2,50	182	18	650	1350	178	2178
5,49 x 1,90 x 0,73	18 x 6,25 x 2,40	162	16	590	1200	152	1942
5,18 x 1,83 x 0,715	17 x 6,00 x 2,30	143	14	508	1050	152	1710
4,88 x 1,75 x 0,70	16 x 5,75 x 2,30	127	12	475	900	127	1494

TABEL ELECTRIC WINDLASS

Type	Diameter rantai		Gaya tarik kg.	kecepatan M/menit	Motor Hp.
	inch	m/m			
EAH - 1	7/8"	22	1850	11,0	9
	15/16"	24	2100	12,8	9
	1"	25	2300	13,4	12
	1 1/16"	27	2600	11,4	12
	1 1/8"	29	3175	12,0	15
EAH - 2	1 3/16"	30	3675	9,0	17
	1 3/4"	32	4250	9,0	17
	15/16"	33	4825	9,4	17
	1 3/8"	35	5400	10,0	24
	1 7/16"	37	5900	10,5	24
EAH - 3	1 1/2"	38	6475	10,1	24
	1 9/16"	40	7125	10,4	30
	1 5/8"	41	7750	10,9	30
	1 11/16"	43	8375	7,3	25
	1 3/4"	44	9525	7,5	30
EAH - 4	1 13/16"	46	9850	7,4	35
	1 7/8"	48	10675	7,3	35
	1 15/16"	49	11425	7,5	35
	2"	51	12375	7,3	40
	2 1/16"	52	13325	7,5	40
EAH - 5	2 1/8"	54	14300	7,3	50
	2 3/16"	56	15250	7,4	50
	2 1/4"	57	16200	7,6	50

REFERENSI BAB VII



an sering merupakan satu-satunya bagian beban internal yang terbesar, maka perlu kewaspadaan dalam memperhitungkannya. Pemancaran kalor dari penerangan merupakan bentuk energi radiasi, bukan beban yang diperoleh segera bagi sistem pengkondisian udara. Energi radiasi dari lampu pertama-tama diserap oleh dinding lantai, dan peralatan-peralatan di dalam ruangan hingga suhunya naik dengan laju yang ditentukan oleh massanya. Oleh karena suhu permukaan benda-benda tersebut naik di atas suhu udara, maka dari permukaan-permukaan tersebut kalor dikonveksikan sehingga akhirnya menjadi beban bagi sistem pendinginan. Jadi, disebabkan oleh massa benda-benda yang menyerap radiasi, terjadi penundaan (delay) antara penyalaan lampu dan energi dari lampu menimbulkan pengaruh pada beban. Dengan alasan yang sama, beban masih tetap bertahan setelah lampu dimatikan. Untuk menyesuaikan terhadap hal-hal ini, telah dikembangkan rumusan berikut untuk memperkirakan perolehan kalor dari lampu-lampu⁴:

$$q = (\text{daya lampu, Watt}) (F_u) (F_b) (\text{CLF})$$

- dengan F_u = faktor penggunaan atau fraksi penggunaan lampu yang terpasang
 F_b = faktor balast untuk lampu-lampu fluorescent = 1,2 untuk fluorescent biasa
 CLF = faktor beban-pendinginan dari Tabel 4-6

Tabel 4-6 memuat faktor beban pendinginan untuk dua macam pemasangan (fixture lampu-lampu yang umum, yang dioperasikan 10 dan 16 jam sehari. Tambahan keterangan an tentang variasi pemasangan, massa lantai, dan periode penyalaan lampu, tersedia.^{4, 6}

Tabel 4-6 Faktor beban-pendinginan dari penerangan⁴

Lama-jam setelah lampu dinyalakan	Pemasangan X† Lama-jam penyalaan		Pemasangan Y‡ Lama-jam penyalaan	
	10	16	10	16
0	0,08	0,19	0,01	0,05
1	0,62	0,72	0,76	0,79
2	0,66	0,75	0,81	0,83
3	0,69	0,77	0,84	0,87
4	0,73	0,80	0,88	0,89
5	0,75	0,82	0,90	0,91
6	0,78	0,84	0,92	0,93
7	0,80	0,85	0,93	0,94
8	0,82	0,87	0,95	0,95
9	0,84	0,88	0,96	0,96
10	0,85	0,89	0,97	0,97
11	0,32	0,90	0,22	0,98
12	0,29	0,91	0,18	0,98
13	0,26	0,92	0,14	0,98
14	0,23	0,93	0,12	0,99
15	0,21	0,94	0,09	0,99
16	0,19	0,94	0,08	0,99
17	0,17	0,40	0,06	0,24
18	0,15	0,36	0,05	0,20

†Penjelasan pemasangan X, lampu terbenam tanpa lubang angin. Pengatur (register) udara suplai & udara balik berada di bawah langit-langit atau di runag langit-langit dan grill. Y, lampu yang dit lubang angin atau tergantung bebas. Pengatur udara suplai berada di bawah atau di dalam langit-lan dengan pengatur udara balik di sekitar pemasangan dan melalul ruang langit-langit.

Tabel 4-11 Koefisien peneduhan (shading coefficients)⁴

Jenis kaca	Ketebalan mm	Tanpa peneduh dalam	Koefisien peneduhan			
			Kisi Pelindung		Tanpa Guna	
			Sedang	Terang	Gelap	Silang
Kaca tunggal						
Lembaran biasa	3	1,00				
Pelat (tebal)	6-12	0,95	0,64	0,55	0,59	0,25
Penyerap panas	6	0,70	0,64	0,55	0,59	0,25
	10	0,50	0,57	0,53	0,40	0,30
			0,54	0,52	0,40	0,28
Kaca rangkap						
Lembaran biasa	3	0,90	0,57	0,51	0,60	0,25
Pelat (tebal)	6	0,83	0,57	0,51	0,60	0,25
Reflektif	6	0,2-0,4	0,2-0,33			

Energi matahari yang menembus suatu jendela dapat dirumuskan sebagai berikut:

$$q_{sg} = (SHGF_{maks}) (SC)A$$

dengan q_{sg} = energi matahari yang menembus jendela.

Ada satu faktor lagi yang harus diperhitungkan, bahwa energi matahari memasuki ruangan tidak segera menjadi beban pendinginan. Energi radiasi ini pertama-tama diserap oleh permukaan-permukaan di dalam ruangan, selama waktu ini suhu permukaan-permukaan tersebut naik dengan laju yang ditentukan oleh sifat-sifat termal dinamisnya. Jadi energi matahari yang diserap ditunda sebelum dilepaskan lagi ke udara di ruangan secara konveksi. Oleh karena proses ini dapat menimbulkan perbedaan waktu yang berarti maka hal ini juga dimasukkan menjadi suatu faktor beban pendinginan (CLF) dalam menghitung beban radiasi melalui kaca. Harga CLF yang diturunkan dari suatu analisis komputer ekstensif dimuat dalam Tabel 4-12.

Dalam menentukan kalor yang diterima dari radiasi matahari melalui permukaan-permukaan tembus cahaya, peneduhan dari luar juga harus diperhitungkan. Peneduhan oleh overhang atau peneduh-peneduh lain, seperti ditunjukkan dalam Gambar 4-5,

Tabel 4-12 Faktor-faktor beban pendinginan untuk kaca yang dilengkapi dengan peneduh dalam, di lintang utara⁴.

Waktu matahari (jam)	Arah jendela								
	E	EL	T	Tenz	S	-BD	B	BL	Hor
6	0,73	0,56	0,47	0,30	0,09	0,07	0,06	0,07	0,12
7	0,66	0,76	0,72	0,57	0,16	0,11	0,09	0,11	0,27
8	0,65	0,74	0,80	0,74	0,23	0,14	0,11	0,14	0,44
9	0,73	0,58	0,76	0,81	0,38	0,16	0,13	0,17	0,59
10	0,80	0,37	0,62	0,79	0,58	0,19	0,15	0,19	0,72
11	0,86	0,29	0,41	0,68	0,75	0,22	0,16	0,20	0,81
12	0,89	0,27	0,27	0,49	0,83	0,38	0,17	0,21	0,85
13	0,89	0,26	0,24	0,33	0,80	0,59	0,31	0,22	0,85
14	0,86	0,24	0,22	0,28	0,68	0,75	0,53	0,30	0,81
15	0,82	0,22	0,20	0,25	0,50	0,83	0,72	0,52	0,71
16	0,75	0,20	0,17	0,22	0,35	0,81	0,82	0,73	0,58
17	0,78	0,16	0,14	0,18	0,27	0,69	0,81	0,82	0,42
18	0,91	0,12	0,11	0,13	0,19	0,45	0,61	0,69	0,25

TABLE 9.4.1 Properties of Commonly Used Refrigerants 40°F Evaporating and 100°F Condensing

	Chemical Formula	Molecular Mass	Ozone Depletion Potential (ODP)	Global Warming Potential (HGWP)	Evaporating Pressure, psia	Condensing Pressure, psia	Compression Ratio	Refrigeration Effect, Btu/lb
Hydrofluorocarbons HFCs								
R-32	CH ₂ F ₂	52.02	0.0	0.14	135.6	340.2	2.51	
R-125	CHF ₃ CF ₃	120.03	0.0	0.84	111.9	276.2	2.47	37.1
R-134a	CF ₃ CH ₂ F	102.03	0.0	0.26	49.7	138.8	2.79	65.2
R-143a	CH ₃ CF ₃	84.0	0.0					
R-152a	CH ₃ CHF ₂	66.05	0.0		44.8	124.3	2.77	
R-245ca	CF ₃ CF ₂ CH ₃	134.1	0.0					
HFC's azeotropics								
R-507	R-125/R-143 (45/55)		0.0	0.98				
HFC's near azeotropic								
R-404A	R-125/R-143a (44/52/4)		0.0	0.94				
R-407A	R-32/R-125/R-134a (20/40/40)		0.0	0.49				
R-407C	R-32/R-125/R-134a (23/25/52)		0.0	0.70				
Hydrochlorofluorocarbons HCFCs and their azeotropics								
R-22	CHClF ₂	86.48	0.05	0.40	82.09	201.5	2.46	69.0
R-123	Di-chlorotrifluoroethane	152.93	0.02	0.02	5.8	20.8	3.59	62.9
R-124	Chlorotetrafluoroethane	136.47	0.02		27.9	80.92	2.90	5.21
HCFC's near azeotropics								
R-402A	R-22/R-125/R-290 (38/60/2)		0.02	0.63				
HCFC's azeotropics								
R-401A	R-22/R-124/R-152a (53/34/13)		0.37	0.22				
R-401B	R-22/R-124/R-152a (61/28/11)		0.04	0.24				

**SECTION 14
PRODUCT LOAD**

The product load is composed of any heat gain occurring due to the product in the refrigerated space. The load may arise from a product placed in the refrigerator at a temperature higher than the storage temperature, from a chilling or freezing process, or from the heat of respiration of perishable products. The total product load is the sum of the various types of product load which may apply to the particular application.

TABLES OF SPECIFIC PRODUCT DATA

The following tables list data on specific products that is essential in calculating the refrigeration product load. Table 10 covers food products, Table 11 solids, and Table 12 liquids.

HEAT OF RESPIRATION

Fruits and vegetables, even though they have been removed from the vine or tree on which they grew, are still living organisms. Their life processes continue for some time after being harvested, and as a result they give off heat. Certain other food products also undergo continuing chemical reactions which produce heat. Meats and fish have no further life processes and do not generate any heat.

The amount of heat given off is dependent on the specific product and its storage temperature. Table 10 lists various food products with pertinent storage data. Note that the heat of respiration varies with the storage temperature.

(continued on p. 14-7)

**Table 10
FOOD PRODUCTS DATA**

Product	Average Freezing Point F	Percent Water	SP H, Btu/ (lb) (F deg)		Latent Heat of Fusion Btu/ lb	Heat of Respiration Btu per (24 hr) (ton) at Temp. Indicated	
			Above Freezing	Below Freezing		°F	BTU
VEGETABLES							
Artichokes	29.1	83.7	0.87	0.45	120	40	10,140
Asparagus	29.8	93	0.94	0.48	134	40	11,700-23,100
Beans, string	29.7	88.9	0.91	0.47	128	40	9700-11400
Beans, Lima	30.1	66.5	0.73	0.40	94	40	4300-6100
Beans, dried		12.5	0.30	0.24	18		
Beets	31.1	87.6	0.90	0.46	126	32	2700
						40	4100
Broccoli	29.2	89.9	0.92	0.47	130	40	11,000-17,000
Brussels sprouts	31	84.9	0.88	0.46	122	40	6600-11,000
Cabbage	31.2	92.4	0.94	0.47	132	40	1700
Carrots	29.6	88.2	0.90	0.46	126	32	2100
						40	3500
Cauliflower	30.1	91.7	0.93	0.47	132	40	4500
Celery	29.7	93.7	0.95	0.48	135	32	1600
						40	2400
Corn (green)	28.9	75.5	0.79	0.42	106	32	7200-11,300
						40	10,600-13,200
Corn (dried)		10.5	0.28	0.23	15		
Cucumbers	30.5	96.1	0.97	0.49	137		
Eggplant	30.4	92.7	0.94	0.48	132		
Endive (escarole)	30.9	93.3	0.94	0.48	132		
Horseradish	26.4	73.4	0.78	0.42	104		
Kale	30.7	86.6	0.89	0.46	124		
Kohlrabi	30	90	0.92	0.47	128		
Lettuce	31.2	94.8	0.96	0.48	136	32	2300
						40	2700
Mushrooms	30.2	91.1	0.93	0.47	130	32	6200
						50	22,000
Olives	28.5	75.2	0.80	0.42	108		
Onions	30.1	87.5	0.90	0.46	124	32	700-1100
						40	1800

Table 10 (cont.)
FOOD PRODUCTS DATA

Product	Average Freezing Point F	Percent Water	SP ht, Btu/(lb) (F deg)		Latent Heat of Fusion Btu/lb	Heat of Respiration Btu per (24 hr) (ton) at Temp. Indicated	
			Above Freezing	Below Freezing		°F	BTU
Parsnips	28.9	78.6	0.84	0.46	112		
Peas (green)	30	74.3	0.79	0.42	106	40	13,200-14,000
Peas (dried)		9.5	0.28	0.22	14		
Peppers (sweet)	30.1	92.4	0.94	0.47	132	40	4700
Potatoes (white)	28.9	77.8	0.82	0.43	111	40	1300-1800
Potatoes (sweet)	28.5	68.5	0.75	0.40	97	40	1710
Pumpkin	30.1	90.5	0.92	0.47	130		
Radishes	30.1	93.6	0.95	0.48	134		
Rhubarb	28.4	94.9	0.96	0.48	134		
Sauerkraut	26	89	0.92	0.47	129		
Spinach	30.3	92.7	0.94	0.48	132	40	8000
Squash	30.1	90.5	0.92	0.47	130		
Tomatoes (green)	30.4	94.7	0.95	0.48	134	60	6230
Tomatoes (ripening)	30.4	94.1	0.95	0.48	134	40	1260
Turnips	30.5	90.9	0.93	0.47	130	32	1900
						40	2200
Vegetables (mixed)	30	90	0.90	0.45	130		
MEATS AND FISH							
Bacon		20	0.30	0.30	29		
Beef (dried)		5-15	0.22-0.34	0.19-0.26	7-22		
Beef (fresh-lean)	29	68	0.77	0.40	100		
Beef (fresh-fat)	28		0.60	0.35	79		
Brined meats			0.75				
Cod fish (fresh)	28		0.90	0.49	119		
Cut meats	29	65	0.72	0.40	95		
Fish (frozen)	28	70	0.76	0.41	101		
Fish (iced)		70	0.76	0.41	101		
Fish (dried)			0.56	0.34	65		
Hams and loins	27	60	0.68	0.38	86.5		
Lamb	29	58	0.67	0.30	83.5		
Livers	29	65.5	0.72	0.40	93.3		
Oyster (shell)	27	80.4	0.83	0.44	116		
Oysters (tub)	27	87	0.90	0.46	125		
Pork (fresh)	28	60	0.68	0.38	86.5		
Pork (smoked)		57	0.60	0.32			
Poultry (fresh)	27	74	0.79	0.37	106		
Poultry (frozen)	27	74	0.79	0.37	106		
Sausage (casings)			0.60				
Sausage (drying)	26	65.5	0.89	0.56	93		
Sausage (franks)	29	60	0.86	0.56	86		
Sausage (fresh)	26	65	0.89	0.56	93		
Sausage (smoked)	25	60	0.86	0.56	86		
Scallops	28	80.3	0.89	0.48	116		
Shrimp	28	70.8	0.83	0.45	119		
Veal	29	63	0.71	0.39	91		
MISCELLANEOUS							
Beer	28	92	1.0				
Bread		32-37	0.70	0.34	46-53		
Bread (dough)		58	0.75				
Butter	30-0	15	0.64	0.34	15		
Candy			0.93				
Caviar (tub)	20	55				40	3820
Cheese (American)	17	60	0.64	0.36	79	40	4680
Cheese (Camembert)	18	60	0.70	0.40	86	40	4920
Cheese (Limburger)	19	55	0.70	0.40	86	40	4920
Cheese (Roquefort)	3	55	0.65	0.32	79	45	4000
Cheese (Swiss)	15	55	0.64	0.36	79	40	4660
Chocolate (coating)	95-85	55	0.30	0.55	40		
Cream (40%)	28	73	0.85	0.40	90		
Eggs (waxed)	27		0.76	0.40	100		
Eggs (frozen)	27			0.41	100		
Flour		13.5	0.36	0.28			
Flowers (cut)	32						
Furs—Woolens				0.40			
						480/sq. ft. Floor Area	

Table 10 (cont.)
FOOD PRODUCTS DATA

Product	Average Freezing Point F	Percent Water	SP ht, Btu/(lb) (F deg)		Latent Heat of Fusion Btu/lb	Heat of Respiration Btu per (24 hr) (ton) at Temp. Indicated	
			Above Freezing	Below Freezing		°F	BTU
Honey		18	0.35	0.26	26	40	1420
Hops						35	1500
Ice cream	27-3	58-66	0.78	0.45	96		
Lard			0.52				
Malt						50	1500
Maple sugar		5	0.24	0.21	7	45	1420
Maple syrup		36	0.49	0.31	52	45	1420
Milk	31	87.5	0.93	0.49	124		
Nuts (dried)		3-10	0.21-0.29	0.19-0.24	4.3-14	35	1000
Oleomargarine		15.5	0.32	0.25	22		
Tobacco and cigars	25						
Yeast		70.9	0.77	0.41	102		
FRUITS							
Apples	28.4	84.1	0.86	0.45	121	32	830
						40	1435
Apricots	28.1	85.4	0.88	0.46	122		
Avocados	27.2	94	0.91	0.49	136	60	13,200-39,700
Bananas	28	74.8	0.80	0.42	108	68	8400-9200
Blackberries	28.9	85.3	0.88	0.46	122		
Blueberries	28.6	82.3	0.86	0.45	118	32	1300-2200
Cantaloupes	29	92.7	0.94	0.48	132	40	2000
						60	8500
Cherries	26	83	0.87	0.45	120		
Cranberries	27.3	87.4	0.90	0.46	124		
Currants	30.2	84.7	0.88	0.45	120		
Dates (dry)	-4.1	20	0.36	0.26	29		
Dates (fresh)	27.1	78	0.82	0.43	112		
Figs (fresh)	27.1	78	0.82	0.43	112		
Figs (dried)		24	0.39	0.27	34		
Gooseberries	28.9	88.3	0.90	0.46	126		
Grapefruit	28.4	88.8	0.91	0.46	126	32	460
						40	1070
Grapes	26.3	81.7	0.86	0.44	116	35	830
Honey Dew Melon	20	92.6	0.94	0.48	132	40	1000
Lemons	28.1	89.3	0.92	0.46	127	40	810
						60	2970
Limes	29	86	0.89	0.46	122	40	810
						60	2970
Mangoes	32	93	0.90	0.46	134		
Nectarines	29	82.9	0.90	0.49	119		
Oranges	28	87.2	0.90	0.46	124	32	795
						40	1400
Peaches	29.4	86.9	0.90	0.46	124	32	1110
						40	1735
						32	770
Pears	28.5	83.5	0.86	0.45	118		
Persimmons	28.3	78.2	0.84	0.43	112		
Pineapples	29.4	85.3	0.88	0.45	123		
Plums	28	85.7	0.88	0.45	122		
Pomegranates	28	77	0.87	0.48	112		
Prunes (fresh)	28	85.7	0.88	0.45	123		
Quinces	28.1	85.3	0.88	0.45	122		
Raspberries	30.1	82	0.85	0.45	122	40	6800-8500
						60	18,100-22,300
Strawberries	29.9	90	0.92	0.47	129		
Tangerines	28.0	87.3	0.93	0.51	126	32	3265
						40	5865
Watermelons	29.2	92.1	0.97	0.48	132		

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Technische Daten
Technical data
Caractéristiques techniques

Verdichter Typ	Motor Version	Förder- volumen bei 87 Hz	Anzahl der Zylinder	Öl- füllung	Gewicht	Rohranschlüsse				FU Anschluss	Elektrische Daten ①	
						DL Druckleitung		SL Saugleitung			Max. Betriebs- strom bei 380V/3/50Hz	Max. Leistungs- aufnahme Verdichter
Compressor type	Motor version	Displace- ment at 87 Hz	Number of cylinders	Oil charge	Weight	Pipe connections				FI connection		
						DL Discharge line		SL Suction line			Max. operating current for 380V/3/50Hz	Max. power con- sumption compressor
Type de compresseur	Version moteur	Volume balayé à 87 Hz	Nombre de cylindres	Charge d'huile	Poids	Raccords				Raccorde- ment de CF		
						DL Conduite de refoulement		SL Conduite d'aspiration			Volt	Courant de service max. à 380V/3/50Hz
		m ³ /h		dm ³	kg ①	mm	pouce	mm	pouce			
2DC-3.F1Y	1	23,7	2	1,5	88	16	5/8	22	7/8	380...480 V/3/50 Hz 380...480 V/3/60 Hz	15	9
4FC-5.F1Y	1	32,0	4	2,0	105	16	5/8	28	1 1/8		20	11
4EC-6.F1Y	1	40,1	4	2,0	105	16	5/8	28	1 1/8		22	12
4DC-7.F1Y	1	47,3	4	2,0	105	22	7/8	35	1 3/8		22	12
4DC-7.F3Y	1	47,3	4	2,0	106	22	7/8	35	1 3/8		28	17
4CC-8.F1Y	2	57,4	4	2,0	106	22	7/8	35	1 3/8		22	12
4CC-9.F3Y	1	57,4	4	2,0	106	22	7/8	35	1 3/8		34	21
4VES-6.F3Y	2	61,3	4	2,6	153	28	1 1/8	42	1 5/8		17	11
4VCS-10.F4Y	1	61,3	4	2,6	163	28	1 1/8	42	1 5/8		35	22
4TES-8.F3Y	2	73,0	4	2,6	158	28	1 1/8	42	1 5/8		20	12
4TCS-12.F4Y	1	73,0	4	2,6	165	28	1 1/8	42	1 5/8		42	26
4PES-10.F3Y	2	85,6	4	2,6	163	28	1 1/8	42	1 5/8		23	14
4PCS-15.F4Y	1	85,6	4	2,6	171	28	1 1/8	42	1 5/8		48	30
4NES-12.F3Y	2	99,2	4	2,6	165	28	1 1/8	42	1 5/8		27	17
4NCS-20.F4Y	1	99,2	4	2,6	174	28	1 1/8	42	1 5/8		55	36

Frequenzbereich

2DC-3.F1Y: 30...87 Hz
 4FC-5.F1Y...4NCS-20.F4Y: 25...87 Hz
 4VES-6.F3Y...4NES-12.F3Y: 25...87 Hz

Frequency range

2DC-3.F1Y: 30...87 Hz
 4FC-5.F1Y...4NCS-20.F4Y: 25...87 Hz
 4VES-6.F3Y...4NES-12.F3Y: 25...87 Hz

Plage de fréquences

2DC-3.F1Y: 30...87 Hz
 4FC-5.F1Y...4NCS-20.F4Y: 25...87 Hz
 4VES-6.F3Y...4NES-12.F3Y: 25...87 Hz

Ölsumpfheizung

- 230 V
 PTC-Heizung selbst-regulierend
 2DC-3.F1Y...4CC-9.F3Y: 0...120 W
 4VES-6.F3Y...4NES-12.F3Y: 0...140 W
 4VCS-10.F4Y...4NCS-20.F4Y: 0...140 W

- obligatorisch bei
- Außenaufstellung des Verdichters
 - langen Stillstandszeiten
 - großer Kältemittel-Füllmenge
 - Gefahr von Kältemittel-Kondensation in dem Verdichter

Crankcase heater

- 230 V
 self-regulating PTC heater
 2DC-3.F1Y...4CC-9.F3Y: 0...120 W
 4VES-6.F3Y...4NES-12.F3Y: 0...140 W
 4VCS-10.F4Y...4NCS-20.F4Y: 0...140 W

- mandatory in case of
- outdoor installation of the compressor
 - long shut-off periods
 - high refrigerant charge
 - danger of refrigerant condensation into the compressor

Résistance de carter

- 230 V
 résistance CTP autorégulante
 2DC-3.F1Y...4CC-9.F3Y: 0...120 W
 4VES-6.F3Y...4NES-12.F3Y: 0...140 W
 4VCS-10.F4Y...4NCS-20.F4Y: 0...140 W

- obligatoire pour
- installation extérieure du compresseur
 - longues périodes d'immobilisation
 - haute charge de fluide frigorigène
 - risque de condensation de fluide frigorigène dans le compresseur

Erläuterungen

- ① Inkl. Frequenzumrichter
 ② Eingang Frequenzumrichter

Explanations

- ① Including frequency inverter
 ② Input frequency inverter

Explications

- ① Compris convertisseur de fréquences
 ② Entrée convertisseur de fréquences

Refrigerant Pressure Temperature Table

F Temp	R717 psig	R22 psig	R134a psig	R404a psig	R507 psig	Vacuum Inches of Hg
-60	18.6	11.9	21.6	-	-	
-55	16.7	9.2	20.2	-	-	
-50	14.4	6.4	18.6	0.64	1.1	
-45	11.8	2.7	16.7	2.77	3.3	
-40	8.8	0.6	14.7	5.12	5.7	
-35	5.5	2.6	12.3	7.72	8.4	
-30	1.7	4.9	9.7	10.57	11.3	
-25	1.2	7.5	6.8	14.39	14.6	
-20	3.5	10.2	3.6	17.08	23.8	
-18	4.5	11.4	2.2	18.52	19.5	
-16	5.6	12.6	0.7	19.47	21.0	
-14	6.7	13.9	0.4	21.55	22.6	
-12	7.8	15.2	1.2	23.15	24.3	
-10	9.0	16.5	2.0	24.79	26.0	
-8	10.2	17.9	2.8	26.50	27.7	
-6	11.5	19.4	3.7	28.25	29.6	
-4	12.8	20.9	4.6	30.07	31.4	
-2	14.2	22.4	5.5	31.94	33.4	
0	15.6	24.0	6.5	33.87	35.3	
1	16.4	24.8	7.0	34.86	36.4	
2	17.1	25.7	7.5	35.87	37.4	
3	17.9	26.5	8.0	36.89	38.5	
4	18.7	27.4	8.6	37.92	39.5	
5	19.5	28.3	9.1	38.97	40.6	
6	20.3	29.1	9.7	40.04	41.7	
7	21.1	30.0	10.2	41.12	42.8	
8	22.0	31.0	10.8	42.22	44.0	
9	22.8	31.9	11.4	43.34	45.1	
10	23.7	32.8	12.0	44.47	46.3	
11	24.6	33.8	12.6	45.62	47.5	
12	25.5	34.8	13.2	46.78	48.7	
13	26.4	35.8	13.8	48.97	49.9	
14	27.4	36.8	14.4	49.17	51.1	
15	28.3	37.8	15.1	50.39	52.4	
16	29.3	38.8	15.7	51.63	53.6	
17	30.3	39.9	16.4	52.88	54.9	
18	31.3	40.9	17.1	54.35	56.2	
19	32.4	42.0	17.7	55.44	57.6	
20	33.4	43.1	18.4	56.75	58.9	
21	34.5	44.2	19.2	58.08	60.3	
22	35.5	45.3	19.9	59.42	61.7	
23	36.6	46.5	20.6	60.79	63.1	
24	37.7	47.6	21.4	61.17	64.5	
25	38.8	48.8	22.1	63.57	65.9	
26	40.0	50.0	22.9	64.99	67.4	
27	41.2	51.2	23.7	66.44	68.9	
28	42.4	52.4	24.5	67.90	70.4	
29	43.7	53.7	25.3	69.38	71.9	
30	44.9	54.9	26.1	70.88	73.4	
31	46.1	56.2	26.9	72.40	75.0	
32	47.4	57.5	27.8	73.84	76.6	
33	48.7	58.8	28.6	75.50	78.2	
34	50.0	60.2	29.5	77.09	79.8	
35	51.4	61.5	30.4	81.68	81.4	
36	52.7	62.9	31.3	80.31	83.1	
37	54.1	64.3	32.2	81.95	85.5	
38	55.5	65.7	33.1	83.62	86.3	
39	57.0	67.1	34.1	85.31	88.3	
40	58.4	68.6	35.0	87.02	90.3	
41	59.2	70.0	36.0	88.72	91.3	
42	61.4	71.5	37.0	90.50	93.3	
43	62.9	73.0	38.0	92.98	95.3	
44	64.5	74.5	39.0	94.08	97.3	
45	66.1	76.1	40.0	95.90	99.3	
46	67.6	77.0	41.1	97.75	101.3	
47	69.3	79.2	42.2	99.61	103.3	
48	70.9	80.8	43.2	101.5	105.3	
49	72.6	82.4	44.3	103.42	106.3	
50	74.3	84.1	45.4	105.36	108.3	
55	83.2	92.6	51.2	115.41	119.3	
60	92.6	101.6	57.4	126.08	130.3	
65	102.8	111.3	64.0	137.39	141.3	
70	113.8	121.5	71.1	149.38	154.3	
75	125.5	132.2	78.7	162.05	166.3	
80	138.0	143.7	86.7	175.45	180.3	
85	151.4	155.7	95.2	189.54	195.3	
90	165.5	168.4	104.3	204.51	210.3	
95	180.6	181.9	113.9	220.22	226.3	
100	196.7	196.0	124.1	236.76	243.3	
105	213.9	210.8	134.9	254.15	260.3	
110	231.8	226.4	146.4	272.43	279.3	
115	251.0	242.8	158.4	291.62	299.3	
120	271.1	260.0	171.1	347.75	319.3	
125	292.5	278.1	184.5	332.85	341.3	
130	314.9	297.0	198.7	354.96	364.3	
135	338.8	316.8	213.5	377.96	388.3	
140	363.5	337.5	229.2	377.30	413.3	
145	390.2	359.1	245.6	402.30	439.3	
150	417.4	381.7	262.8	427.30	467.3	
155	447.0	405.4	281.0	454.02	-	

C Temp	R717 bar	R22 bar	R134a bar	R404a bar	R507 bar
-60	0.218	0.375	0.169	0.522	0.522
-58	0.249	0.420	0.180	0.544	0.592
-56	0.283	0.469	0.205	0.608	0.648
-54	0.320	0.522	0.232	0.674	0.719
-52	0.362	0.580	0.261	0.747	0.796
-50	0.408	0.644	0.294	0.827	0.880
-48	0.459	0.713	0.330	0.913	0.970
-46	0.515	0.787	0.370	1.006	1.068
-44	0.576	0.868	0.413	1.106	1.173
-42	0.644	0.955	0.460	1.214	1.286
-40	0.717	1.049	0.516	1.330	1.408
-38	0.797	1.151	0.572	1.454	1.523
-36	0.885	1.264	0.633	1.587	1.663
-34	0.98	1.259	0.699	1.730	1.813
-32	1.083	1.376	0.770	1.882	1.973
-30	1.195	1.501	0.847	2.045	2.144
-28	1.315	1.635	0.930	2.218	2.325
-26	1.446	1.830	1.020	2.402	2.518
-24	1.587	2.092	1.116	2.598	2.723
-22	1.738	2.265	1.219	2.806	2.940
-20	1.801	2.448	1.330	3.027	3.170
-18	2.076	2.643	1.448	3.260	3.414
-16	2.263	2.849	1.575	3.507	3.671
-14	2.464	3.068	1.710	3.767	3.942
-12	2.679	3.299	1.854	4.043	4.228
-10	2.908	3.543	2.007	4.333	4.529
-8	3.152	3.801	2.170	4.639	4.846
-6	3.412	4.072	2.344	4.951	5.179
-4	3.688	4.358	2.527	5.299	5.529
-2	3.982	4.659	2.722	5.655	5.966
0	4.294	4.976	2.928	6.023	6.282
2	4.625	5.308	3.146	6.420	6.686
4	4.975	5.657	3.376	6.830	7.108
6	5.345	6.023	3.619	7.260	7.551
8	5.737	6.406	3.876	7.710	8.014
10	6.150	6.807	4.145	8.180	8.498
12	6.586	7.226	4.429	8.672	9.004
14	7.046	7.665	4.728	9.188	9.532
16	7.530	8.123	5.042	9.722	10.084
18	8.039	8.601	5.371	10.281	10.659
20	8.574	9.099	5.716	10.864	11.258
22	9.136	9.619	6.078	11.472	11.883
24	9.725	10.160	6.457	12.104	12.534
26	10.343	10.723	6.853	12.763	13.212
28	10.991	11.309	7.267	13.448	13.919
30	11.669	11.919	7.701	14.160	14.653
32	12.379	12.552	8.153	14.900	15.416
34	13.121	12.210	8.626	15.669	16.213
36	13.896	13.892	9.117	16.468	17.041
38	14.705	14.601	9.630	17.297	17.901
40	15.549	15.335	10.164	18.157	18.795
42	16.429	16.097	10.720	19.049	19.724
44	17.347	16.885	11.299	19.974	20.689
46	18.302	17.702	11.901	20.932	21.692
48	19.297	18.548	12.526	21.925	22.734
50	20.331	19.423	13.176	22.953	23.816
52	21.407	20.328	13.851	24.018	24.94
54	22.525	21.265	14.552	25.120	26.107
56	23.686	22.232	15.278	26.260	27.319
58	24.892	23.232	16.032	27.440	28.578
60	26.143	24.266	16.813	28.660	29.884
62	27.440	25.333	17.623	29.921	31.241
64	28.785	26.435	18.462	31.225	32.649
66	30.179	27.573	19.331	32.572	34.112
68	31.622	28.747	20.231	33.964	35.63
70	33.117	29.959	21.162	35.402	37.207
72	34.664	31.210	22.126	36.887	-
74	36.264	32.500	23.123	-	-
76	37.918	33.932	24.154	-	-
78	39.629	35.205	25.221	-	-
80	41.397	36.623	26.324	-	-

CONVERSIONS

- $\Delta T^{\circ}C = \Delta T^{\circ}F \text{ or } \Delta T^{\circ}F = \Delta T^{\circ}C$
- Temperature in $^{\circ}F = 1.8^{\circ}C + 32$
- Temperature in $^{\circ}C = \frac{1}{1.8}(^{\circ}F - 32)$
- 1 psi = 0.06895 bar = 6.895 kPa or 1 bar = 14.5 psi = 100 kPa
- Cv (U.S. GPM) = Kv multiplied by 1.156 or Kv = Cv multiplied by 0.865
- 1 American Standard Commercial Ton of Refrigeration = 12000 Btu/hr = 3024 kcal/hr = 3.517 kW
- 1 kW = 0.284 American Standard Commercial Ton of Refrigeration
- 1" (inch) = 25.4 mm or 1 mm = 0.03937"
- 1 ft = 0.3048 m or 1 m = 3.2808 ft
- 1 lb = 0.4536 kg or 1 kg = 2.2046 lbs

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HANSEN TECHNOLOGIES CORPORATION



SPLIT TYPE MARINE AIR CONDITIONER

INSTALLATION, OPERATION AND MAINTENANCE MANUAL

Brand Name: COOLMAR

MODEL NO

MAS 008

MAS 010

MAS 012

MAS 015

MAS 018

MAS 020

MAS 022

MAS 024



are made of chrome. The fan body can turn between 0 – 90 for the convenience during the air duct installation.

3. TECHNICAL SPECIFICATIONS TABLE

SPECIFICATIONS		Model / Unit	MAS 008	MAS 010	MAS 012	MAS 015	MAS 018	MAS 020	MAS 022	MAS 024
Cooling Capacity		Btu/h	7.500	9.500	12.200	15.000	18.200	20.000	22.100	24.600
Heating Capacity		Btu/h	7.600	9.700	12.600	15.800	18.700	20.300	22.600	25.000
Power Consumption		W	680	900	1.270	1.600	2.000	2.200	2.400	2.630
Current	Indoor Unit	A	0,3	0,4	0,5	0,6	0,6	0,7	0,7	0,7
	Outdoor Unit	A	3,0	3,7	5,3	6,6	8,7	10,1	10,5	11,3
Indoor Unit	Length	mm	290	290	320	450	450	450	450	450
	Width	mm	270	270	270	320	320	320	320	320
	Height	mm	320	320	320	350	350	350	350	350
	Net Weight	kg	12	12	14	18	19	19	20	22
	Air Flow	m ³ /h	275	320	520	650	780	950	1.100	1.250
	Fan Motor Power	W	60	70	100	110	110	115	120	120
Outdoor Unit	Length	mm	330	330	330	330	330	330	330	330
	Width	mm	270	270	270	320	320	320	320	320
	Height	mm	320	320	340	370	370	370	400	400
	Net Weight	kg	17	18	19	25	27	27	29	32
Suction Pipe		Inch	3/8"	3/8"	3/8"	1/2"	1/2"	1/2"	1/2"	1/2"
Discharge Pipe		Inch	1/4"	1/4"	1/4"	3/8"	3/8"	3/8"	3/8"	3/8"
Condenser Pipe		Inch	3/4"	3/4"	3/4"	3/4"	3/4"	3/4"	3/4"	3/4"
Drain Pipe		Inch	5/8"	5/8"	5/8"	5/8"	5/8"	5/8"	5/8"	5/8"
Duct Diameter		mm	100	100	125	125	2x125	150	150	150
Proposed Fuse for the System		A	C 16	C 16	C 16	C 20	C 20	C 25	C 25	C 25
Max Pump Current That can be Connected to the Unit Electrical Box		A	4	4	4	4	4	4	4	4
Condenser water flow		l/m	9	11	13	13	16	19	19	20
Voltage		V	230							
Frequency		Hz	50							
IP Class			IP 22							
Feeding Cable Cross Section /Type			3 x 2,5 / Tin Coated							

Lampiran A

Faktor Pengubahan

Untuk ringkasnya, satuan-satuan untuk tiap besaran di bawah ini dihubungkan dengan sebuah satuan dasar atau satuan SI turunan. Pengubahan antara pasangan satuan yang lain untuk sebuah besaran dibuat dengan menggunakan aturan biasa untuk manipulasi satuan.

CONTOH Ubahlah ft³ menjadi gal.

Dari bagian volume kita dapatkan $1 \text{ m}^3 = 35.3147 \text{ ft}^3 = 264.172 \text{ gal}$, dari situ diperoleh

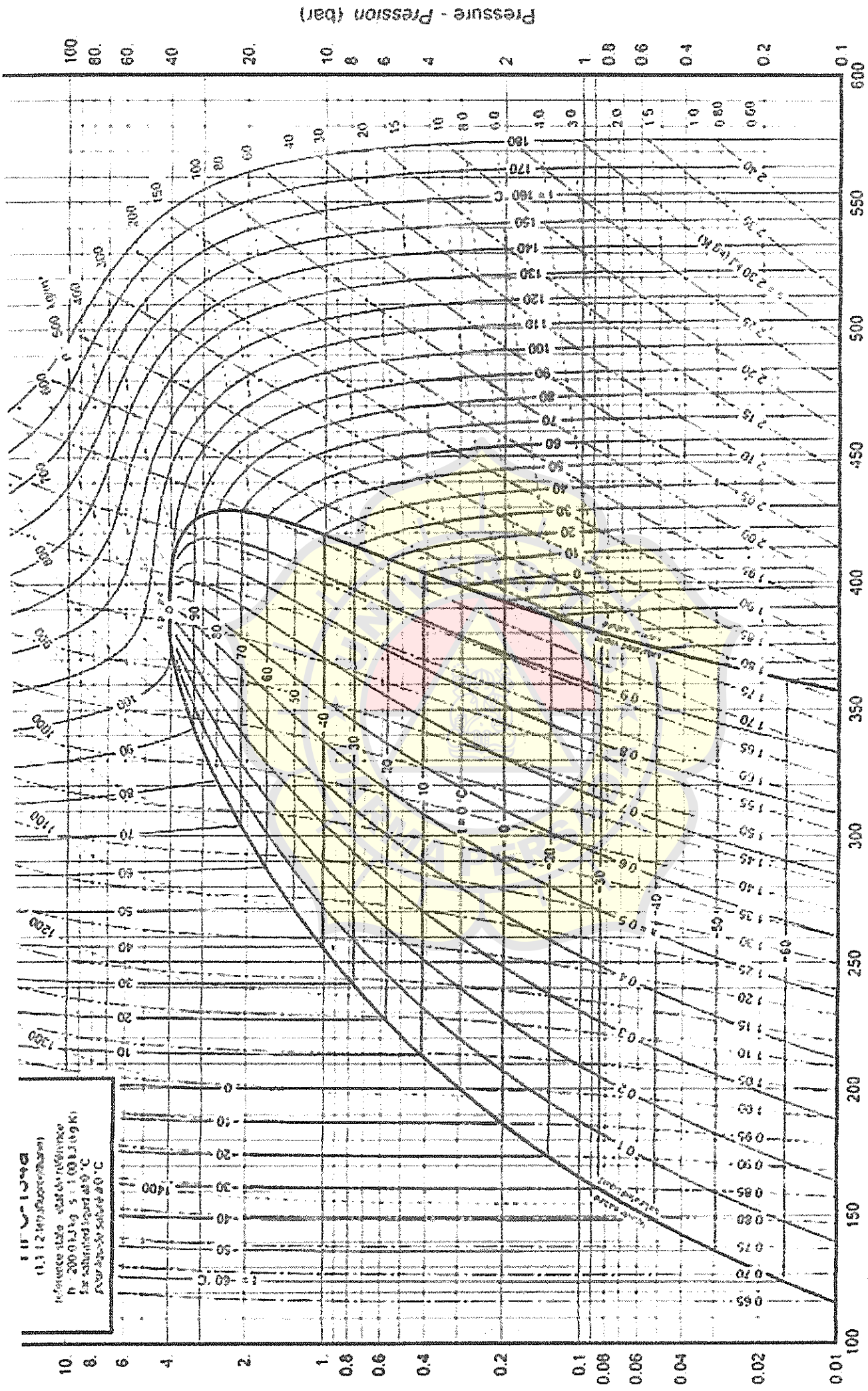
Besaran	Pengubahan	Besaran	Pengubahan
Panjang	1 m = 100 cm	Energi	1 kJ = $10^3 \text{ kg} \cdot \text{m}^2 \cdot \text{s}^{-2}$
	1 m = 3.28084 ft		= $10^3 \text{ N} \cdot \text{m}$
Massa	1 kg = 10 ³ g		= $10^3 \text{ V} \cdot \text{s}$
	1 kg = 2.20462 lb _m		= 10^{10} erg
Gaya	1 N = 1 kg · m · s ⁻²		= $10^4 \text{ cm}^2 \cdot \text{bar}$
	= 10 ⁷ dyne		= 239,006 kal
Tekanan	1 bar = $10^5 \text{ kg} \cdot \text{m}^{-1} \cdot \text{s}^{-2}$		= 9869,23 cm ³ · atm
	= $10^5 \text{ N} \cdot \text{m}^{-2}$		= 5.12197 psia · ft ³
	= 100 kPa		= 737,562 ft · lb _f
	= 10 ⁶ dyne · cm ⁻²		= 0.947831 Btu
	= 0.986923 atm		
Volume	1 m ³ = 10 ⁶ cm ³	Daya	1 kW = $10^3 \text{ kg} \cdot \text{m}^2 \cdot \text{s}^{-3}$
	= 10 ³ L		= 10^3 W
	= 35.3147 ft ³		= $10^3 \text{ J} \cdot \text{s}^{-1}$
Kerapatan	1 kg · m ⁻³ = 10 ³ g · cm ⁻³		= 10 ³ V · A
	= 1 g · L ⁻¹		= 239,006 kal · s ⁻¹
	= 0.0624278 lb _m · ft ⁻³		= 737,562 ft · lb _f · s ⁻¹
	= 0.00034540 lb _m · gal ⁻¹		= 56,8699 Btu · min ⁻¹
			= 1.34102 hp

Catatan: atm = atmosfer baku
 kal = kalori termokimia
 Btu = Btu Tabel Uap Air Internasional
 L = liter

46. Konstanta kesetimbangan kimia *K* bertambah dengan naiknya *T*, asalkan perubahan entalpi reaksi baku ΔH° positif.
 47. Ada dua derajat kebebasan di dalam sebuah sistem reaktif kimia yang mengandung spesies-spesies gas N₂, H₂, dan NH₃.
 48. Pada suhu konstan, kenaikan tekanan akan menyebabkan kenaikan hasil metanol (CH₃OH) dari reaksi gas ideal
- $$\text{CO}(g) + 2\text{H}_2(g) \rightarrow \text{CH}_3\text{OH}(g)$$
49. W sama untuk semua proses aliran tunak yang menghasilkan perubahan keadaan yang sama, asalkan suhu lingkungannya sama.
 50. Kerja yang hilang merupakan sebuah besaran yang dibuat untuk menerangkan pengesualian terhadap hukum termodinamika pertama.

JAWAB:

- 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
S S B B S B S B S S S S S B S B
- 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30
B S B S B S S B B B B B S S B
- 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45
S B S S B B B S S B S S B B S
- 46 47 48 49 50
B S B B S



SI Units
 Reference state: saturated liquid
 $h = 2000 \text{ kJ/kg}$ $s = 1000 \text{ kJ/kg}$
 For saturated liquid at 0°C
 $h_{\text{ref}} = 0$ $s_{\text{ref}} = 0$

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 Gaithersburg, MD 20899-8550

Enthalpy - Enthalpie (kJ/kg)

International Organization of Standards, 2 rue des Saussaies, 75008 Paris, France



Table A.E.1 Saturation Properties of Refrigerant R-134a: Temperature Increments

Temp., F	Press., P _{sat} , psia	Specific Volume, ft ³ /lbm			Internal Energy, Btu/lbm			Enthalpy, Btu/lbm			Entropy, Btu/lbm · R		
		Sat. Liquid, v _f	Sat. Vapor, v _g		Sat. Liquid, u _f	Sat. Vapor, u _g		Sat. Liquid, h _f	Evap., h _{fg}	Sat. Vapor, h _g	Sat. Liquid, s _f	Sat. Vapor, s _g	
40	7.4272	0.01299	5.7839		63.718	152.95		63.733	97.167	160.90	0.19016	0.42169	
50	9.8624	0.01429	4.4330		66.725	154.32		66.746	95.664	162.41	0.19724	0.41989	
60	12.898	0.01565	3.4449		69.756	155.69		69.784	94.136	163.92	0.20421	0.41851	
70	14.671	0.01635	3.0514		71.281	156.38		71.313	93.357	164.67	0.20766	0.41760	
80	16.632	0.01706	2.7109		72.812	157.06		72.848	92.562	165.41	0.21109	0.41693	
90	18.794	0.01779	2.4154		74.350	157.75		74.391	91.759	166.15	0.21449	0.41631	
100	21.171	0.01853	2.1579		75.894	158.43		75.940	90.950	166.89	0.21786	0.41572	
110	23.777	0.01929	1.9330		77.445	159.11		77.497	90.123	167.62	0.22122	0.41518	
120	26.628	0.02007	1.7357		79.002	159.79		79.062	89.288	168.35	0.22456	0.41467	
130	29.739	0.02086	1.5623		80.567	160.47		80.634	88.436	169.07	0.22787	0.41419	
140	33.124	0.02168	1.4094		82.140	161.14		82.214	87.576	169.79	0.23117	0.41374	
150	36.800	0.02251	1.2742		83.720	161.82		83.803	86.697	170.50	0.23445	0.41332	
160	40.784	0.02337	1.1543		85.307	162.49		85.401	85.799	171.20	0.23771	0.41293	
170	45.092	0.02425	1.0478		86.903	163.15		87.007	84.893	171.90	0.24095	0.41257	
180	49.741	0.02515	0.95280		88.507	163.81		88.623	83.967	172.59	0.24418	0.41222	
190	54.749	0.02608	0.86796		90.120	164.47		90.248	83.022	173.27	0.24739	0.41190	
200	60.134	0.02703	0.79198		91.742	165.12		91.883	82.057	173.94	0.25059	0.41159	
210	65.913	0.02802	0.72380		93.372	165.77		93.529	81.071	174.60	0.25378	0.41131	
220	72.105	0.02903	0.66246		95.013	166.41		95.185	80.075	175.26	0.25695	0.41103	
230	78.729	0.03008	0.60718		96.663	167.05		96.853	79.047	175.90	0.26011	0.41077	
240	85.805	0.03116	0.55724		98.324	167.67		98.532	77.998	176.53	0.26327	0.41052	
250	93.351	0.03229	0.51204		99.995	168.30		100.22	76.930	177.15	0.26641	0.41028	
260	101.39	0.03345	0.47104		101.68	168.91		101.93	75.820	177.75	0.26955	0.41005	
270	109.93	0.03465	0.43379		103.37	169.51		103.65	74.690	178.34	0.27268	0.40982	
280	119.01	0.03590	0.39988		105.08	170.11		105.38	73.540	178.92	0.27580	0.40959	
290	128.65	0.03720	0.36896		106.80	170.69		107.13	72.350	179.48	0.27892	0.40937	
300	138.85	0.03856	0.34079		108.53	171.26		108.89	71.130	180.02	0.28204	0.40914	
310	149.65	0.03998	0.31483		110.28	171.82		110.67	69.880	180.55	0.28515	0.40891	
320	161.07	0.04146	0.29111		112.04	172.37		112.46	68.590	181.08	0.28827	0.40867	
330	173.14	0.04301	0.26933		113.82	172.90		114.28	67.280	181.53	0.29139	0.40842	
340	185.86	0.04464	0.24928		115.62	173.41		116.12	65.970	181.99	0.29451	0.40815	
350	203.92	0.04632	0.18332		123.00	173.92		123.69	59.850	183.54	0.30708	0.40889	
360	314.73	0.04691	0.13428		130.79	176.64		131.74	52.720	184.46	0.31995	0.40803	
380	400.34	0.047888	0.096375		139.24	177.19		140.54	43.790	184.33	0.33350	0.40396	
400	503.89	0.048996	0.064663		149.07	175.80		150.95	30.880	181.83	0.34896	0.39577	
420	563.35	0.047695	0.047695		155.85	172.80		158.26	19.220	177.48	0.35960	0.38830	

Tahap 4: Perhitungan faktor Penggunaan

Faktor penggunaan didefinisikan sebagai persen dari lumen lampu kosong yang mengeluarkan cahaya dan mencapai bidang kerja. Faktor ini bertanggungjawab langsung terhadap cahaya dari lumener dan cahaya yang dipantulkan permukaan ruangan. Fihak pabrik akan memasok setiap lumener dengan tabel CU nya sendiri yang berasal dari laporan pengujian fotometrik. Dengan menggunakan tabel yang tersedia dari pabrik, ditentukan faktor penggunaan untuk pemasangan berbagai cahaya jika pantulan dari dinding dan langit-langit diketahui, indeks ruangan telah ditentukan dan jenis lumener diketahui. Untuk peralatan tabung kembar, faktor penggunaannya adalah 0,66, sesuai untuk indeks ruangan 2,5.

Tahap 5: Perhitungan jumlah fitting yang diperlukan dengan penerapan rumus sebagai berikut:

$$N = \frac{E \times A}{F \times UF \times LLF}$$

Dimana:

N = Jumlah fitting

E = Tingkat lux yang diperlukan pada bidang kerja

A = Luas ruangan (L x W)

F = Flux total (Lumens) dari seluruh lampu dalam satu fitting

UF = Faktor penggunaan dari tabel untuk peralatan yang digunakan

LLF = Faktor kehilangan cahaya. Kehilangan ini disebabkan oleh penurunan keluaran lampu yang sudah lama dan penumpukan kotoran pada peralatan dan dinding bangunan.

LLF = Lumen lampu MF x Lumener MF x Permukaan ruangan MF

Nilai LLF

Kantor ber AC	0,8
Industri bersih	0,7
Industri kotor	0,6

$$N = \frac{200 \times 100}{2 \times 3050 \times 0,66 \times 0,8}$$

= 6,2; Sehingga, lampu tabung kembar nomor 6 diperlukan. Jumlah total lampu 36-Watt adalah 12.

Tahap 6: Ruang lumener untuk mencapai keseragaman yang dikehendaki

Setiap lumener akan memiliki ruang yang direkomendasikan terhadap perbandingan tinggi. Pada metodologi perancangan sebelumnya, perbandingan keseragaman, yakni perbandingan terang minimum terhadap terang rata-rata dijaga pada 0,8 dan ruang yang cocok untuk perbandingan tinggi ditentukan untuk mencapai keseragaman. Dalam perancangan modern memadukan efisiensi energi dengan tugas pencahayaan, konsep yang muncul adalah memberi keseragaman 1/3 hingga 1/10 tergantung pada tugasnya. Nilai lumener diatas yang direkomendasikan adalah

Tabel 2. Karakteristik Kinerja Pencahayaan (*Luminous*) dari Luminer yang Umum Digunakan

Jenis Lampu	Lum / Watt		Indeks Perubahan Warna	Penerapan	Umur (Jam)
	Kisaran	Rata-rata			
Lampu pijar	8-18	14	Baik sekali	Rumah, restoran, penerangan umum, penerangan darurat	1000
Lampu Neon	46-60	50	Lapisan w.r.t yang baik	Kantor, pertokoan, rumah sakit, rumah	5000
Lampu Neon Kompak (CFL)	40-70	60	Sangat Baik	Hotel, pertokoan, rumah, kantor	8000-10000
Merkuri tekanan tinggi (HPMV)	44-57	50	Cukup	Penerangan umum di pabrik, garasi, tempat parkir mobil, penerangan berlebihan/ sangat terang	5000
Lampu halogen	18-24	20	Baik Sekali	Peraga, penerangan berlebihan, arena pameran, area konstruksi	2000-4000
Sodium tekanan tinggi (HPSV) SON	67-121	90	Cukup	Penerangan umum di pabrik, gudang, penerangan jalan	6000-12000
Sodium tekanan rendah (LPSV) SOX	101-175	150	Buruk	Jalan raya, terowongan, kanal, penerangan jalan	6000-12000

3. PENGKAJIAN SISTIM PENCAHAYAAN

Bagian ini meliputi perancangan sistim penerangan untuk interior dan juga metodologi studi efisiensi energi sistim pencahayaan. Bagian ini juga memberi rekomendasi nilai penerangan yang diperlukan oleh berbagai jenis pekerjaan sesuai dengan standar India.

3.1 Merancang Sistim Pencahayaan

3.1.1 Berapa banyak cahaya yang diperlukan?

Setiap pekerjaan memerlukan tingkat pencahayaan pada permukaannya. Pencahayaan yang baik menjadi penting untuk menampilkan tugas yang bersifat visual. Pencahayaan yang lebih baik akan membuat orang bekerja lebih produktif. Membaca buku dapat dilakukan dengan 100 to 200 lux. Hal ini merupakan pertanyaan awal perancang sebelum memilih tingkat pencahayaan yang benar. CIE (Commission International de l'Eclairage) dan IES (Illuminating Engineers Society) telah menerbitkan tingkat pencahayaan yang direkomendasikan untuk berbagai pekerjaan. Nilai-nilai yang direkomendasikan tersebut telah dipakai sebagai standar nasional dan internasional bagi perancangan pencahayaan (Tabel diberikan dibawah). Pertanyaan kedua adalah mengenai kualitas cahaya. Dalam kebanyakan konteks, kualitas dibaca sebagai perubahan warna.

Table (cont'd)

(4) Operating area

Space	Illumination lx	Method of measurement	Remark
Main passage, stair and entrance in eng. room, boiler room and aux. machine room	100	Fig. 3, Fig. 5, Fig. 6	
Operation area in engine room, boiler room and aux. machine room	150	-	At a height of 850 mm above floor of operation area and monitoring station
Access to the rear of tanks in eng. room, boiler room and aux. machine room	20	Fig. 6	
Engine control room	200	Fig. 1	
on gauge	300	Fig. 12	Not applicable to photoelectric digital instrument board, display surface of CRT etc.
on operating table	300	Fig. 12	Not applicable to photoelectric digital instrument board, display surface of CRT etc.
Work shop	100	Fig. 1	
on work bench	300	-	Centre of work bench surface
at work face of machine and tool	500	-	
Engine room store	50	Fig. 1	
Shaft tunnel	20	Fig. 6	
Cargo control room	200	Fig. 1	
on gauge	300	Fig. 12	Not applicable to photoelectric digital instrument board, display surface of CRT, etc.
on operating table	300	Fig. 12	Not applicable to photoelectric digital instrument board, display surface of CRT, etc.
Emergency generator room	100	Fig. 1	
on gauge	200	Fig. 12	
Battery room	50	Fig. 1	
Boatswain's store	50	Fig. 1	
Paint store	50	Fig. 1	
Cargo oil pump room	50	Fig. 5, Fig. 6	Near passageway, stairway, and pump
Steering gear room, aircond. room etc.	50	Fig. 1	
Refrigerated cargo hold	30	Fig. 7	
General cargo hold (fixed light)	20	Fig. 8	
Under deck passage	20	Fig. 2	Container ship, dredger
Cargo handling space	20	-	Horizontal plane near operating handle
Mooring area	20	-	Mean value of measurements at several suitable points in a horizontal plane at a height of 850 mm above deck

(1) Living area

Space	Illumination lx	Method of measurement	Remark
Captain class day room	150	Fig. 1	
Captain class bed room	100	Fig. 1	
Cabin	100	Fig. 1	
State room, passenger room	100	Fig. 1	
On desk	250	Fig. 11	Local lighting in captain class room, captain class bed room, cabin, and state room
Berth at pillow	200	Fig. 9	Local lighting in captain class room, captain class bed room, cabin, and state room
Mirror front	200	Fig. 10	Local lighting in captain class room, captain class bed room, cabin, and state room
Bath room	50	Fig. 1	
Lavatory, toilet	50	Fig. 1	
Mirror front	200	Fig. 10	
Barber shop and beauty parlor	200	Fig. 1	
Dining saloon, mess room	200	Fig. 1	
on dining table	250	Fig. 11	
on table (writing, game)	250	Fig. 11	
Smoking room	200	Fig. 1	
Recreation room	200	Fig. 1	For a Japanese-style room, illumination at a height of 400 mm above floor
on dining table	250	Fig. 11	
on table (writing, game)	250	Fig. 11	
Sports room, gymnasium	200	Fig. 1	
Library	200	Fig. 1	
on table	250	Fig. 11	
Lounge	200	Fig. 1	
Cocktail lounge	-	-	Mood lighting; suitable illumination
Hospital	100	Fig. 1	
Dispensary	200	Fig. 1	
on dispensary table	500	-	Table face right under lamp or bulb
Shopping area	200	Fig. 1	For ferry boat, passenger ship, etc.
Passage, alley way, corridor passage	50	Fig. 2	
Staircase	50	Fig. 3	Including companion way

Table (cont'd)

Space	Illumination lx	Method of measurement	Remark
Entrance for passenger	100	—	Mean value of several suitable points near entrance
Outer passage	10	Fig. 4	
Swimming pool	50	—	Measuring point shall be on water surface at pool centre

(2) Navigation area

Space	Illumination lx	Method of measurement	Remark
Wheelhouse	50	Fig. 1	
Chart room	50	Fig. 1	
on chart table	250	—	Table face right under lamp or bulb
Radio office	200	Fig. 1	
Operating table	250	Fig. 11	
Electric room, such as gyro room, radar room, etc.	100	Fig. 1	
Pilot house	100	Fig. 1	Crane barge, rig
Navigation room	200	Fig. 1	Crane barge, rig
Operating room	200	Fig. 1	Crane barge, rig
Rig management room	200	Fig. 1	Crane barge, rig

(3) Service area

Space	Illumination lx	Method of measurement	Remark
Office	100	Fig. 1	
on desk	250	Fig. 11	
Galley	100	Fig. 1	
on cooking table	150	—	Centre of cooking table surface
Pantry, butcher shop, bakery etc.	100	Fig. 1	
Provision store (dry)	50	Fig. 1	
Refrigerated provision chamber	30	Fig. 1	
Laundry	100	Fig. 1	
Drying room	50	Fig. 1	
Locker and store	50	Fig. 1	

Table 1 Lamps for General Illumination

Type	Rated wattage W	Rated voltage V	Classification	Glass bulb		Length mm	Base	Standard direction of lamp	Consumption W	Illumination characteristics		Endurance time for vibration under over voltage h	Static life h	Shape
				Type	Dia. mm					Light flux lm	Efficiency lm/W			
KG 24 V 10 W	10	24	Gas-filled	A55	55 ± 1	98 ± 3	E26/25 or E22D/26 × 26	Down	10.0 ± 0.7	88 ± 13	8.5 ± 1.0	25	1000	
KG 110 V 10 W	10	110	Vacuum	A55	55 ± 1	98 ± 3	E26/25 or E22D/26 × 26	Down	10.0 ± 0.7	60 ± 7	6.0 ± 0.6	15	2000	
KG 110 V 115 V	10	115	Vacuum	A55	55 ± 1	98 ± 3	E26/25 or E22D/26 × 26	Down	20.0 ± 1.4	220 ± 33	11.0 ± 1.3	45	1000	
KG 24 V 20 W	20	24	Gas-filled	A55	55 ± 1	98 ± 3	E26/25 or E22D/26 × 26	Down	20.0 ± 1.4	142 ± 17	7.1 ± 0.7	40	2000	
KG 110 V 20 W	20	110	Vacuum	A55	55 ± 1	98 ± 3	E26/25 or E22D/26 × 26	Down	20.0 ± 1.4	112 ± 17	5.6 ± 0.7	15	2000	
KG 110 V 115 V	20	115	Vacuum	A55	55 ± 1	98 ± 3	E26/25 or E22D/26 × 26	Down	40.0 ± 2.8	540 ± 81	13.5 ± 1.6	50	1000	
KG 24 V 40 W	40	24	Gas-filled	A55	55 ± 1	105 ± 3	E26/25 or E22D/26 × 26	Down	40.0 ± 2.8	335 ± 41	8.4 ± 0.9	40	1500	
KG 110 V 40 W	40	110	Gas-filled	A55	55 ± 1	105 ± 3	E26/25 or E22D/26 × 26	Down	40.0 ± 2.8	260 ± 39	6.5 ± 0.8	30	2000	
KG 110 V 115 V	40	115	Vacuum	A60	60 ± 1	110 ± 4	E26/25 or E22D/26 × 26	Down	60.0 ± 4.2	870 ± 130	14.5 ± 1.7	50	1000	
KG 24 V 60 W	60	24	Gas-filled	A60	60 ± 1	110 ± 4	E26/25 or E22D/26 × 26	Down	60.0 ± 4.2	590 ± 71	9.8 ± 1.0	50	1500	Fig. (1)
KG 110 V 60 W	60	110	Gas-filled	A60	60 ± 1	110 ± 4	E26/25 or E22D/26 × 26	Down	60.0 ± 4.2	440 ± 66	7.4 ± 0.9	40	1500	
KG 110 V 115 V	60	115	Vacuum	A60	60 ± 1	110 ± 4	E26/25 or E22D/26 × 26	Down	100 ± 7	1550 ± 230	15.5 ± 1.9	50	1000	
KG 24 V 100 W	100	24	Gas-filled	A70	70 ± 1	136 ± 4	E26/25 or E22D/26 × 26	Down	100 ± 7	1150 ± 140	11.5 ± 1.2	50	1500	
KG 110 V 100 W	100	110	Gas-filled	A70	70 ± 1	136 ± 4	E26/25 or E22D/26 × 26	Down	100 ± 7	920 ± 140	9.2 ± 1.1	40	1500	
KG 110 V 115 V	100	115	Vacuum	A70	70 ± 1	136 ± 4	E26/25 or E22D/26 × 26	Down	200 ± 14	2740 ± 320	13.7 ± 1.4	50	1500	
KG 24 V 200 W	200	24	Gas-filled	PS 80	80 ± 1	175 ± 5	E26/30 × 28 or E22D/26 × 26	Down	200 ± 14	2280 ± 350	11.4 ± 1.1	50	1500	
KG 110 V 200 W	200	110	Gas-filled	PS 80	80 ± 1	175 ± 5	E26/30 × 28 or E22D/26 × 26	Down	300 ± 21	4500 ± 540	15.0 ± 1.5	50	1500	
KG 110 V 115 V	200	115	Vacuum	PS 80	80 ± 1	175 ± 5	E26/30 × 28 or E22D/26 × 26	Down	300 ± 21	3810 ± 570	12.7 ± 1.5	50	1500	
KG 24 V 300 W	300	24	Gas-filled	PS 95	95 ± 1	213 ± 7	E39/41	Down	500 ± 35	8200 ± 980	16.5 ± 1.6	50	1500	
KG 110 V 300 W	300	110	Gas-filled	PS 95	95 ± 1	213 ± 7	E39/41	Down	500 ± 35	7100 ± 1100	14.2 ± 1.7	50	1500	
KG 110 V 115 V	300	115	Vacuum	PS 95	95 ± 1	213 ± 7	E39/41	Down						
KG 24 V 500 W	500	24	Gas-filled	PS 110	110 ± 1	232 ± 8	E39/41	Down						
KG 110 V 500 W	500	110	Gas-filled	PS 110	110 ± 1	232 ± 8	E39/41	Down						
KG 110 V 115 V	500	115	Vacuum	PS 110	110 ± 1	232 ± 8	E39/41	Down						

Remarks: 1. The letters and figures for types shall mean as follows:

K: Marine lamps

G: Lamps for general use

Figures following G: Rated voltage

Figures following V: Rated wattage

2. The glass bulbs shall be of transparent or frosted (300 W. or less).

Table 2 Lamps for Indicating Light

Type	Rated voltage W	Rated voltage V	Classifi- cation	Glass bulb		Length mm	Base	Standard direction of lamp	Initial characteristics		Endurance time for vibration under cover- voltage h	Static life h	Shape
				Type	Dia. mm				Consumption W	Light flux lm (Reference value)			
KP 12 V 2 W	2	12	Vacuum	T13	13 ± 1	33 ± 2	E12/15	Horizontal	2.0 ± 0.3	--	20	1500	
KP 24 V 2 W	2	24	Vacuum	T10	10 ± 1	28 ± 2	BA9S/13	Horizontal	2.0 ± 0.3	--	20	1500	
KP 24 V 3 WC	3	24	Vacuum	T19	19 ± 1	45 ± 3	E12/15 or BA15D/19	Horizontal	3.0 ± 0.5	(15)	20	1500	Fig. (2)
KP 24 V 3 WE	3	24	Vacuum	T19	19 ± 1	50 ± 3	E14/22	Horizontal	3.0 ± 0.5	(15)	20	1500	Fig. (2)
KP 24 V 5 WB	5	24	Vacuum	T19	19 ± 1	65 ± 3	E12/15 or BA15D/19	Horizontal	5.0 ± 0.8	(32)	20	1500	
KP 24 V 5 WC	5	24	Vacuum	T19	19 ± 1	45 ± 3	E12/15 or BA15D/19	Horizontal	5.0 ± 0.8	(32)	20	1500	
KP 24 V 5 WE	5	24	Vacuum	T19	19 ± 1	50 ± 3	E14/22	Horizontal	5.0 ± 0.8	(32)	20	1500	Fig. (2)
KP 24 V 5 WD	5	24	Vacuum	G19	19 ± 1	35 ± 2	E12/15 or BA15D/19	Horizontal	5.0 ± 0.8	(30)	20	1500	Fig. (2)
KP 115 V 5 WC	5	115	Vacuum	T19	19 ± 1	45 ± 3	E12/15 or BA15D/19	Horizontal	8 max	(20)	15	1500	
KP 115 V 5 WE	5	115	Vacuum	T19	19 ± 1	50 ± 3	E14/22	Horizontal	8 max	(20)	15	1500	Fig. (2)
KP 115 V 10 WA	10	115	Vacuum	T26	26 ± 1	75 ± 3	E26/25 or B22D/26 × 26	Horizontal	10.0 ± 1.5	(50)	15	1500	Fig. (2)
KP 115 V 10 WC	10	115	Vacuum	T19	19 ± 1	45 ± 3	E12/15 or BA15D/19	Horizontal	10.0 ± 1.5	(50)	15	1500	
KP 115 V 10 WE	10	115	Vacuum	T19	19 ± 1	50 ± 3	E14/22	Horizontal	10.0 ± 1.5	(50)	15	1500	
KP 230 V 10 W	10	230	Vacuum	T19	19 ± 1	50 ± 3	E14/22	Horizontal	15 max	(55)	15	1500	

Remarks: 1. The letters for types shall mean as follows:

- W: Lamps for indicating light
- A, B, C, D: Length

2. The glass bulbs shall be of transparent.

1407-177

Appendix table 1. Dimension, cap and characteristics (Continued)

Types	Classification of size	Rated lamp wattage W	Rated input voltage V	Start test voltage V	Lamp wattage W	Lamp current A	(Reference) Lamp voltage V	Initial characteristics										Lumen maintenance factor %	(Reference) Rated life h
								Total luminous flux lm											
								D	N	W, WW, L	EX-D	EX-N	EX-W, WW-L						
FL4	4	4	100	94	4.6	0.162±0.020	30	(90)	(95)	(100)	-	-	-	-	-	-	2400 or more		
FL6	6	6	-	-	5.9	0.147±0.020	44	(155)	(170)	(180)	-	-	-	-	-	-	-		
FL8	8	8	-	-	7.9	0.170±0.020	56	(260)	(280)	(290)	-	-	-	-	-	-	-		
FL10	10	10	-	-	9.5	0.230±0.030	46	410	440	460	490	530	540	540	75 or more	4000 or more			
FL15	15	15	-	-	14.7	0.300±0.030	55	710	780	820	860	920	940	940	-	-			
FL20SS/18	20	18	-	-	18.0	0.340±0.040	59	1010	1100	1160	1320	1400	1430	1430	85 or more	6000 or more			
FL20S		20	-	-	19.0	0.360±0.040	58	-	-	-	-	-	-	-	-	-			
FL30S	30	30	-	-	30.0	0.610±0.050	55	1480	1620	1700	1790	1900	1940	1940	75 or more	-			
FL40SS/37	40	37	200	180	37.0	0.410±0.040	108	2610	2850	3000	3180	3380	3450	3450	85 or more	8000 or more			
(FL40SS/38)		38	-	-	38.0	0.410±0.040	109	-	-	-	-	-	-	-	-	-			
FL40S		40	-	-	39.5	0.420±0.040	106	-	-	-	-	-	-	-	-	-			

- Remarks**
1. The value attaching () to the value of total luminous flux shall be the reference value.
 2. Total luminous flux of -DL, -SDL and -EDL in color rendering property classification shall be 75% or more, 65% or more and 60% or more of this table's value respectively.
 3. Total luminous flux of shatterproof types shall be 97% or more of this table's value.
 4. Lumen maintenance factor of -DL, -SDL and -EDL in color rendering property classification shall be more than the value deducting 5 from this table's value.

Series 40

2NM Single Color Index Models (for Aqua Signal series 40, 41, 42, 55 etc.; Perko 200 (Fig. 0375), Hella 2984, 2986, 2988, etc.)



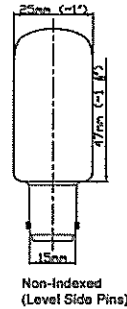
Part #	8001757	8001764	8001771	8000043
Description	For anchor, steaming, & stern nav. lights	For port nav. lights.	For starboard nav. lights.	For amber/yellow nav. lights
LED Color	White	Red	Green	Amber / Yellow
Voltage	12/24 VDC	12/24 VDC	12/24 VDC	12/24 VDC
Bulb Type	Indexed	Indexed	Indexed	Indexed

2NM Single Color Non-Index Models

(for Perko series 1127, 1130, etc.; Perko Bulb Fig. 0374)



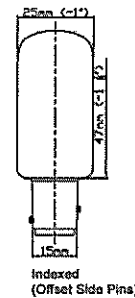
Part #	8001078	8001382	8001405
Description	For anchor, steaming, & stern nav. lights	For port nav. lights.	For starboard nav. lights.
LED Color	White	Red	Green
Voltage	12 VDC	12 VDC	12 VDC
Bulb Type	Non-Index	Non-Index	Non-Index



Bi-Color



Part #	8001085	8001092
Description	Bi-Color PS40	Bi-Color PS41
Bulb Type	Aqua Signal series 40 Base Mount	Aqua Signal series 41 Top Mount
LED Color	Red / Green	Red / Green
Voltage	12 VDC	12 VDC
Remark	Indexed	Indexed

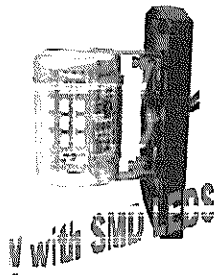


Tri-Color



Part #	8001450	8001436
Description	Tri-Color MKII	24 Tri-Color
Replacement	For aqua signal, Hella, & Perko tri-color nav lights	For 24V aqua signal series 40 tri-color stack
LED Color	White / Red / Green	White / Red / Green
Voltage	12 VDC	24 VDC
Remark	Indexed	Indexed

Series 25



Part #	8001122	9000241
Description	Bi-Color (Dimpled Festoon)	2NM 39-44mm White Festoon
Bulb Type	Port, starboard, and bi-color nav. lights	
LED Color	Red / Green	White
Voltage	12 VDC	12 VDC

navigation

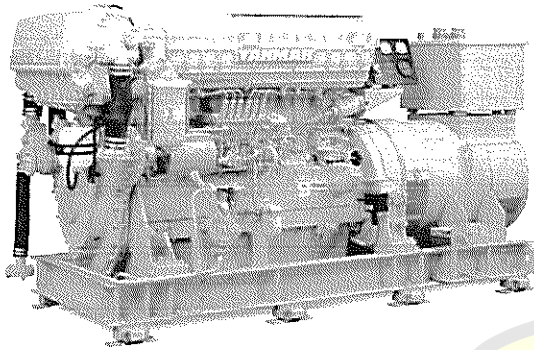
REFERENSI BAB VIII



6HAL2 series

MARINE
AUXILIARY
DIESEL ENGINE

122~414hp / 1200~1800rpm
100~350kVA (80~280kW)



- 6-cylinder, direct injection.
- Natural aspirated or turbocharged. (with intercooler)
- 6HAL2-WT, 6HAL2-WHT and 6HAL2-WDT conform to IMO Tier II emissions regulations.
- Type approved by NK, BV, GL, KR.

Specifications

Model	6HAL2-N	6HAL2-TN	6HAL2-WT	6HAL2-WHT	6HAL2-WDT
Number of cylinders	In-line 6				
Bore X stroke	mm 130 X 165				
Displacement	lit. 13.14				
Continuous rated engine speed	1200 1500	1200	1500 1800	1200 1500 1800	1200 1500 1800
Continuous rated output	122 156	163	204 244	217 289 360	271 346 414
Applicable generator capacity	100 (80) 125 (100) 130 (104)	170 (136) 200 (160)	180 (144) 250 (200) 300 (240)	225 (180) 290 (232) 350 (280)	
Frequency	60 50	60	50 60	60 50 60	60 50 60
Combustion system	Direct injection				
Aspiration	Natural aspiration	Exhaust Turbocharger	Exhaust Turbocharger with intercooler		
Dry weight (Engine only)	1380	1422	1437	1447	
Dry weight (Gen. set)	2350	2410	2750	2850	

Accessories

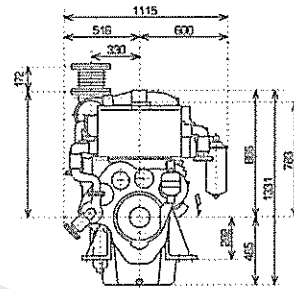
- Instrumental panel (attached to engine)
- Cooling system : Sea water pump / Centrifugal type fresh water pump / Heat exchanger / Fresh water reservoir / Thermostat for fresh water / Emergency use sea water inlet
- Lubrication system : Lubrication oil pump / Lubrication oil cooler / Lubrication oil filter (Tandem switch type) / Manual priming pump
- Fuel system : Paper filter type fuel strainer / Drain separator to be mounted on vessel
- Turbocharging system : Exhaust gas outlet expansion joint from engine
- Electrical equipment : Starter motor (DC24V) 6.0kW / Alternator (DC24V600W) / Battery switch / 2 pole wiring
- Thermometer : Exhaust gas at outlet of each cylinder / Cooling water outlet / Lubrication oil at cooler inlet

[44]

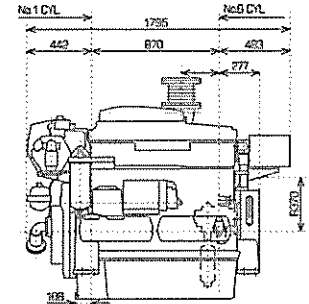
Dimensions Unit:mm

Engine only (6HAL2-TN, -WT, -WHT, -WDT)

Front view



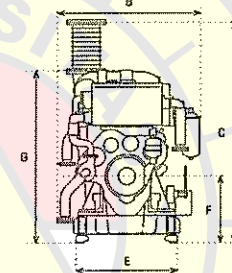
Left side view



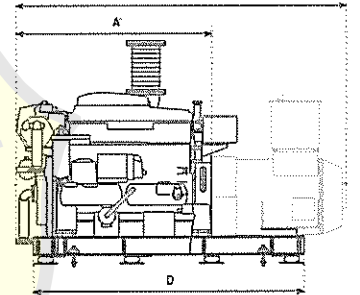
Generator set dimensions for your reference Unit:mm

Generator set dimensions shown below depend on generator model

Front view



Left side view



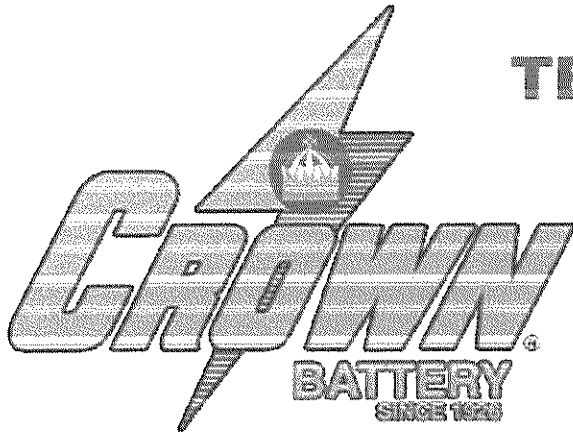
G : Minimum Height for Removing Piston (Not included the dimension for bolt facing to piston remove.)

Model	A	A'	B	C	D	E	F	G
6HAL2-N	2499	1589	1164	1654	2100	820	544	1327
6HAL2-TN	2499	1589	1164	1774	2100	820	544	1327
6HAL2-WT	2499	1589	1164	1774	2100	820	544	1327
6HAL2-WHT	2574	1589	1164	1804	2200	820	544	1327
6HAL2-WDT	2684	1589	1164	1804	2200	820	544	1327

- Generator

- Cooling system : Kingston cock
- Lubrication system : Inlet and outlet joint for semi dry sump
- Fuel system : Primary fuel strainer to be mounted on vessel
- Generator (and common bed) : Taiyo or Stamford
- Thermometer : Exhaust gas at inlet of turbocharger (WT, TN, WHT, WDT) / Lubrication oil at cooler outlet
- Electrical governor for parallel operation
- Exhaust piping : Expansion joint for piping / Silencer
- Compressed air starting device
- Remote control device : Trip panel / Stop solenoid / LO pressure switch / FW temperature switch / Speed relay / Junction box & wiring

[45]



TECHNICAL DATA SHEET

Crown Battery Mfg. Co. • Fremont, Ohio USA
419-334-7181 • FAX 419-334-7124

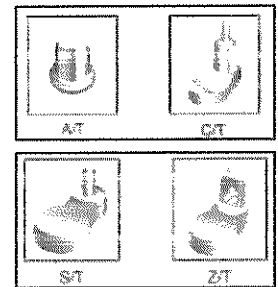
CR-395

Commercial Deep Cycle Battery

Crown Battery Manufacturing Company offers a complete lineup of high-performing and low-maintenance commercial deep cycle batteries produced in standard BCI industry profiles for voltage, electrical capacity and physical dimension. Crown Battery's innovative and proven deep cycle product design makes it the battery of choice for many tough commercial battery applications, including commercial floor care and aerial access equipment, electric motorcars, personnel carriers, material handling equipment and photovoltaic systems.



Available Terminals



SPECIFICATIONS

Nominal Voltage	6 Volts		
Amp Hour Capacity	395 (C20)	320 (C5)	
Reserve Capacity Minutes	225 @ 75 Amperes		
Physical Characteristics	Length	12.19"	310 mm
	Width	7.19"	183 mm
	Height	16.50"	419 mm
	Wet Weight	121 Lbs	55.0 Kgs
Terminal Options	A/T, C/T, S/T, Z/T		

Cover Style:	Exposed Vent Opening
Cover Vent Style:	Quarter-Turn Bayonet Style
Container and Cover Material:	Black Polypropylene
Case to Cover Seal Method:	Heat Seal
Inner-Cell Connector Type:	Through Partition Weld
Plate Lug to Collector Bar Fusion Method:	Inverted Automatic Cast-On
Number of Plates per Battery:	51 Plates
Positive Grid Material:	Antimony Lead Alloy
Positive Grid Design:	Z³ Horizontal Pellet
Positive Plate Dimension:	5.750" x 11.500" x 0.140"
	146mm x 292mm x 3.6mm
Negative Grid Material:	Antimony Lead Alloy
Negative Grid Design:	Z³ Horizontal Pellet
Negative Plate Dimension:	5.750" x 11.500" x 0.105"
	146mm x 292mm x 2.7mm
Separator Type:	Microporous Polyethylene Envelope with Glass

ELECTRICAL SPECIFICATIONS

Amp Hour Capacity	20 Hour Rate	19.75 A	395 Ah
	10 Hour Rate	33.20 A	332 Ah
	5 Hour Rate	57.00 A	285 Ah
	2 Hour Rate	108.0 A	216 Ah
Internal Resistance	80 F	27 C	8.1 mOhm
Capacity affected by Temperature (20 Ah Rate)	104 F	40 C	102%
	80 F	27 C	100%
	32 F	0 C	65%

Created with



Visit our website at
www.crownbattery.com

download the free trial version at nitropdf.com/professionals

II.2.1 Estimasi Tenaga Penggerak

Metode *Admiralty*

$$BHP = \frac{\frac{2}{\Delta^3} x V^3}{\Delta c}$$

Kapal pembanding :

$$\begin{aligned}\Delta c &= \frac{\frac{2}{\Delta^3} x V^3}{BHP} \\ &= \frac{1601,5^{2/3} x 12,97^3}{1800} \\ &= 165,9199921\end{aligned}$$

Kapal rancangan :

$$\begin{aligned}BHP &= \frac{2962,917^{2/3} x 15^3}{165,9199921} \\ &= 4193,951 \text{ HP}\end{aligned}$$

Maka untuk 1 M/E :

$$\begin{aligned}BHP &= \frac{4193,951}{2} \\ &= 2096,975\end{aligned}$$

Daya mesin awal yang dipesan oleh owner adalah 2 x 2100 HP namun space mesin yang digunakan yang mendekati 2330 HP maka digunakan daya mesin untuk supply vessel ini adalah 2 x 2330 HP